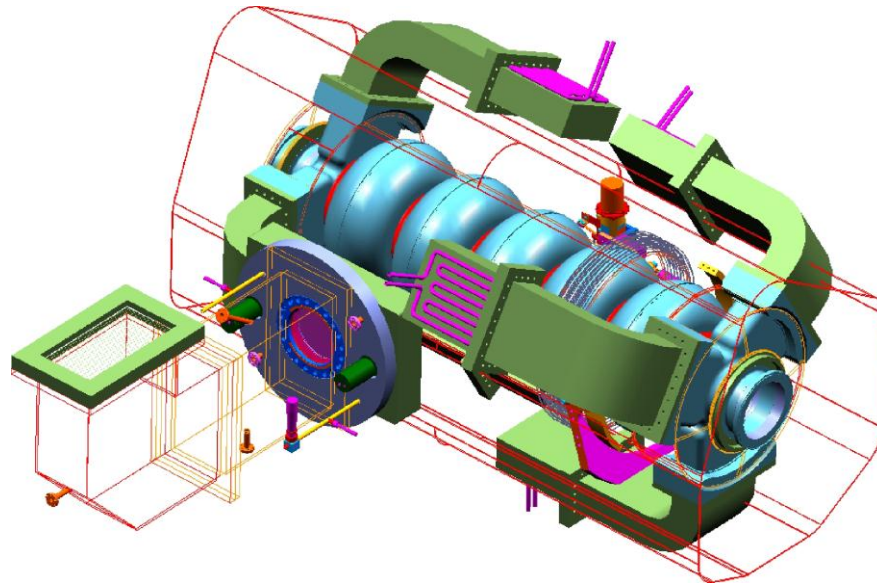


# Waveguide HOM damping studies at JLab



R. Rimmer et. al. HOM10, Cornell

# Outline

- Motivation
- Solution(s)
- 748.5 MHz version
- 1497 MHz version
- Future applications
- SPX crab cavity
  - HOM, LOM and SOM damping
  - On-cell alternative design
- Conclusions

# Motivation

- 100 mA to “Ampere class” ERL for the Navy
- Compact design for shipboard FEL
  - High gradient, high packing factor
- Proven technology wherever possible
- R&D path consistent with Jlab capabilities and experience
- Eye to future light source projects for DOE

## Requirements:

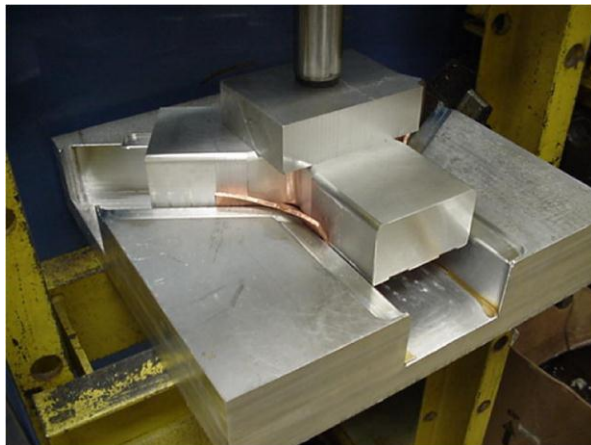
JLab Ampere-class module specifications.

Voltage	100-120 MV
Length	~10m
Frequency	748.5 MHz
Beam Aperture	>3" (76.2mm)
BBU Threshold	>1A
HOM Q's	<10 <sup>4</sup>
Beam power	0-1MW

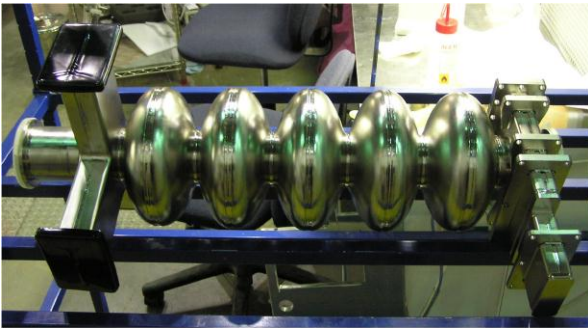
Plus: reasonable cryogenic cost, maintainability,  
flexibility

# Why consider waveguides?

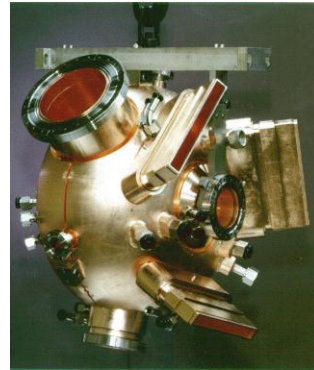
- Waveguide is a natural high-pass filter
- High power-handling capability
- Small beamline length required
- Loads can be at higher temperature
- Static loss is tolerable
- Good experience at PEP-II and CEBAF
- Easy to fabricate



# Concepts



+



=



Take the best from Jlab experience and high-current storage ring technology.

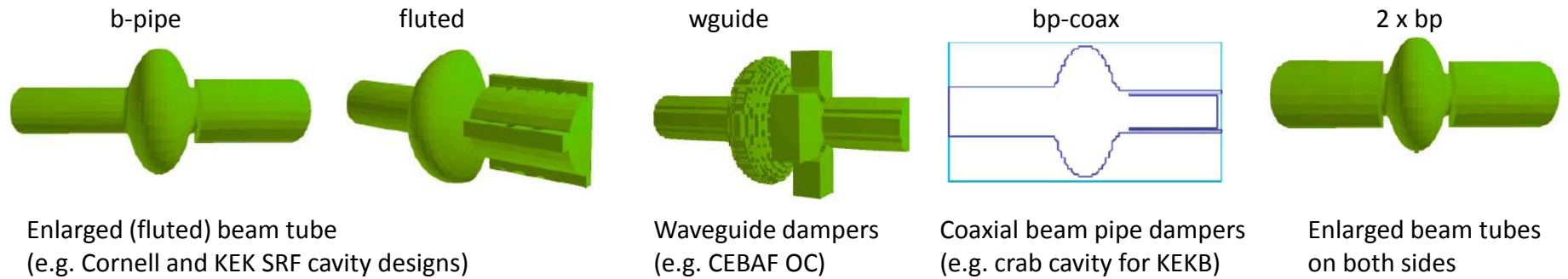
General layout:

- Symmetrical waveguide-damped 5-cell cavities.
- Six cavities per cryomodule at 16.7 MV/m - 20 MV/m.
- Good packing factor with real-estate gradient  $\sim 10\text{-}12$  MV/m.
- HOM power dissipated at room temperature.
- Cell with a good HOM frequency spectrum.
- High-current optimized cell shape gives good efficiency

# JLAB HC Cryomodule Development

## Cavity Cell Shape and Number of Cells

- Wide range of cell shapes existing (e.g. High Gradient (HG), Low Loss (LL), Original Cornell, ILC)
- Storage ring light sources and colliders routinely operate with strongly damped single-cell cavities
- Various HOM damping schemes have been investigated for models at 1.5 GHz (MAFIA T3)



- Damping of monopole ( $TM_{011}$ ) and dipole modes ( $TE_{111}$ ,  $TM_{110}$ ) can be efficient
- Comparably low Qs obtained for all concepts for most parasitic modes (monopole  $< 8 \times 10^2$ , dipole  $< 1.6 \times 10^3$ )
- All damping schemes principally suited for next generation ERL's

Table 1.  $TM_{011}$  mode for various damping methods

	freq MHz	Q	$R^*$ ( $\Omega$ )	$R/Q$ ( $\Omega$ )
b-pipe	2803	252	3001	11.9
flutes	2803	137	1010	7.3
wguide	2800	353	5040	14.3
bp-coax	2783	725	11879	16.4
2xbp	2822	121	1481	12.2

\* $R=V^2/2P$

Table 2. Dipole modes for various damping methods

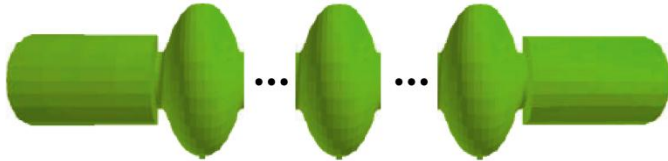
	$TE_{111}$ f, MHz	$TE_{111}$ Q	$TE_{111}$ $R^*$ , ( $\Omega$ )	$TM_{110}$ f, MHz	$TM_{110}$ Q	$TM_{110}$ $R^*$ ( $\Omega$ )
b-pipe	1853	83	246	2028	130	1567
flutes	1857	79	239	2029	130	1479
w-guide	1867	553	1594	2027	1131	14419
coax	1924	341	1496	2065	502	5150
2xbp	1830	37	192	2018	53	735

\*R calculated at 25mm offset in the cavity

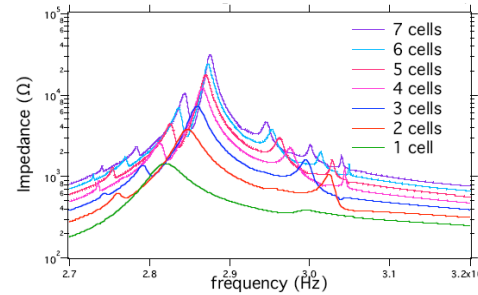
# JLAB HC Cryomodule Development

## Cavity Cell Shape and Number of Cells

- Study damping efficiency by adding cells (beam pipe loaded structure)



Enlarged beam tubes  
(Original Cornell (OC) shape cavity cells)



TM<sub>011</sub> passband mod vs. # cells

- Damping efficiency better in shorter structures

Table 3. Strongest TM<sub>011</sub> passband mode vs # cells

#cells	freq MHz	Q	R* (Ω)	R/Q (Ω)
1	2822	121	1481	12.2
2	2848	167	3856	23.0
3	2860	219	7369	33.7
4	2866	295	12140	41.1
5	2870	362	17795	49.1
6	2873	455	24360	53.5
7	2876	527	31463	59.7

\*R=V<sup>2</sup>/2P

Table 4. Strongest TE<sub>111</sub>/TM<sub>110</sub> passband modes vs # cells

#cells	TE <sub>111</sub> f, MHz	TE <sub>111</sub> Q	TE <sub>111</sub> R*, (Ω)	TM <sub>110</sub> f, MHz	TM <sub>110</sub> Q	TM <sub>110</sub> R* (Ω)
1	1830	37	192	2018	53	735
2	1907	46	569	2101	2641	10103
3	1940	45	1193	2093	2023	14362
4	1867	94	1844	2101	4058	29270
5	1892	121	3232	2097	3233	40923
6	1910	139	4859	2102	5029	46740
7	1922	135	6088	2099	4177	72101

\*R calculated at 25mm offset in the cavity

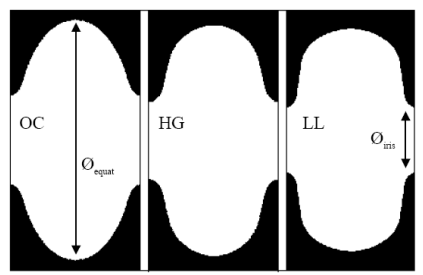
- However: Overhead length of HOM load(s) may reduce the real estate gradient of cryomodule (may want to share HOM loads with adjacent cavities)



# JLAB HC Cryomodule Development

## Cavity Cell Shape and Number of Cells

### Study effect of cell shape on coupling strength



Parameter		OC	HG	LL
$O_{equator}$	[mm]	187.0	180.5	174.0
$O_{ins}$	[mm]	70.0	61.4	53.0
$k_{cc}$	[%]	3.29	1.72	1.49
$E_{peak}/E_{acc}$	[-]	2.56	1.89	2.17
$B_{peak}/E_{acc}$	[mT/(MV/m)]	4.56	4.26	3.74
R/Q	[ $\Omega$ ]	96.5	111.9	128.8
G	[ $\Omega$ ]	273.8	265.5	280.3
R/Q-G	[ $\Omega \cdot \Omega$ ]	26422	29709	36103

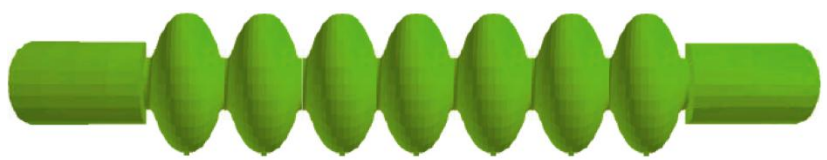
Figure 1: Geometry of three inner cells.

Proceedings of the 2003 Particle Accelerator Conference

### CAVITIES FOR JLAB'S 12 GEV UPGRADE

J. Sekutowicz, G. Ciovati, P. Kneisel, G. Wu, TJNAF, Newport News, 23606 VA, USA  
 A. Brinkmann, DESY, 22603 Hamburg, FRG  
 W. Hartung, MSU, East Lansing, Michigan, USA  
 R. Parodi, INFN Genoa, 16146 Genoa, Italy  
 S. Zheng, Tsinghua University, 100084 Beijing, China

### 7-cell cavities with open beam tubes



7-cell OC, HG and LL cavity

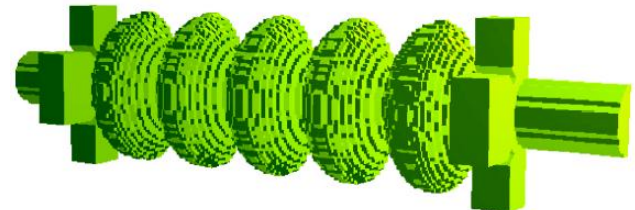
Table 5.  $TM_{011}$  mode data for multi-cell cavities.

	#cells	Freq.MHz	Q	$R^{\dagger}$ ( $\Omega$ )	R/Q ( $\Omega$ )
OC	7	2876	527	31463	59.7
HG	7	2876	1348	90380	67.0
LL	7	2629	985	53556	54.4
OC	5	2870	362	17795	49.1

OC*	5	2871	707	35453	50.1
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\*waveguide damped

$$^{\dagger}R = V^2/2P$$



5-cell OC with waveguide damping endgroups

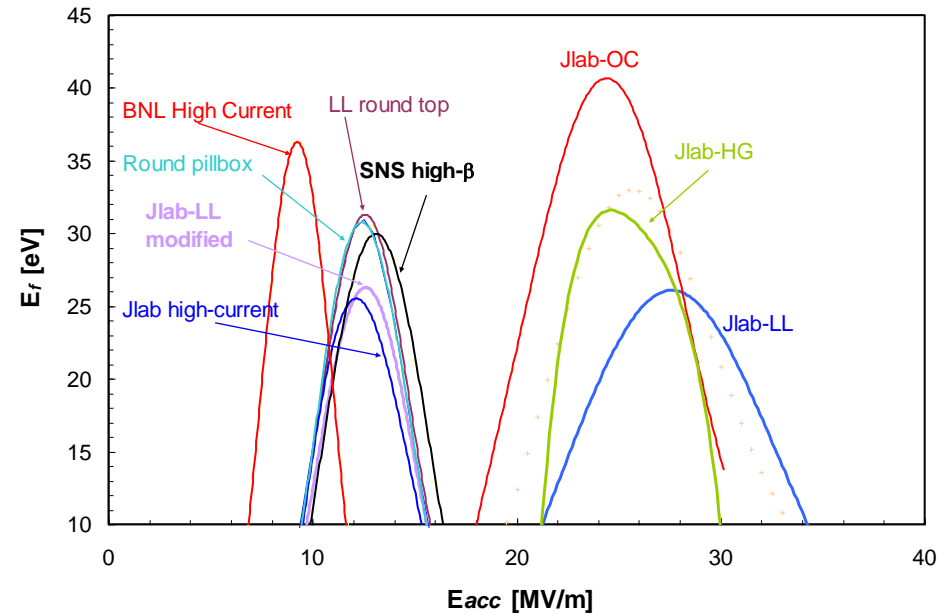
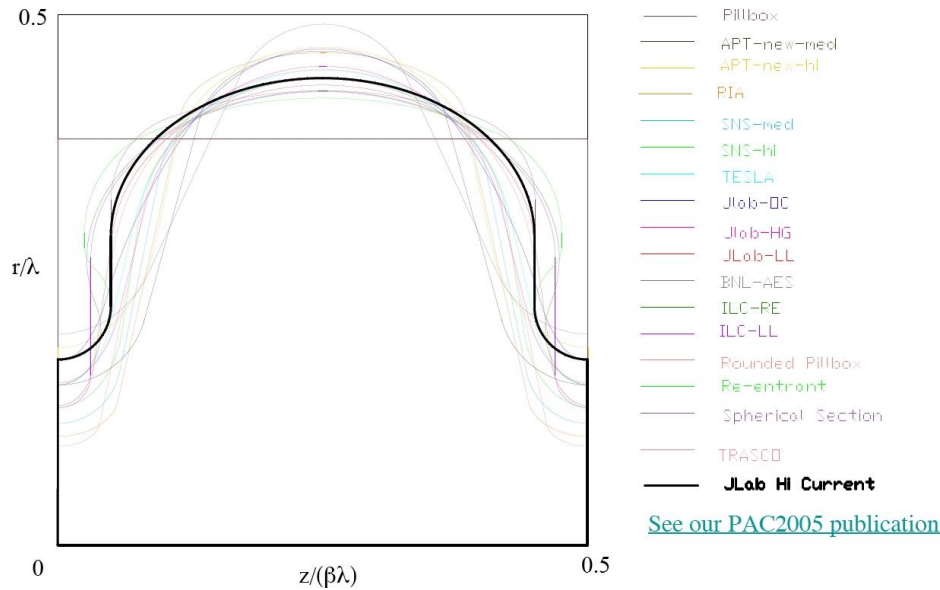
Table 6.  $TE_{111}/TM_{110}$  mode data for multi-cell cavities.

	# cells	$TE_{111}$ f,MHz	$TE_{111}$ Q	$TE_{111}$ $R^{\dagger}$ ( $\Omega$ )	$TM_{110}$ f, MHz	$TM_{110}$ Q	$TM_{110}$ $R^{\dagger}$ ( $\Omega$ )
OC	7	1922	135	6088	2099	4177	72101
HG	7	2014	185	11359	2156	5694	146409
LL	7	2021	490	14107	2209	2071	39510
OC	5	1892	121	3232	2097	3233	40923

OC*	5	1894	956	22949	2103	3274	47064
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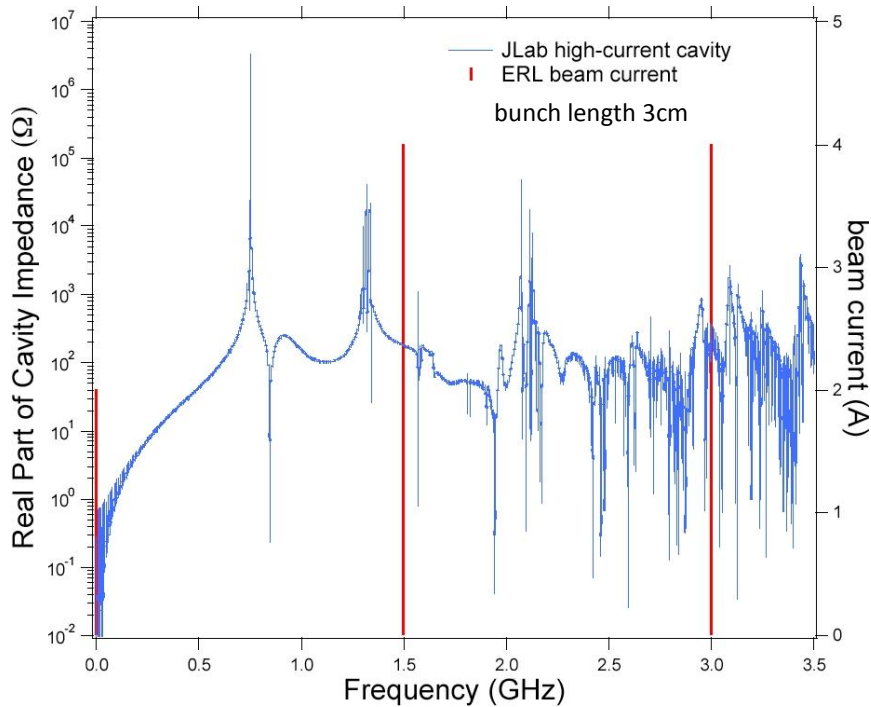
\*waveguide damped  $^{\dagger}R$  calculated at 25mm offset in cavity

# Cavity cell shape optimization concept for High Current

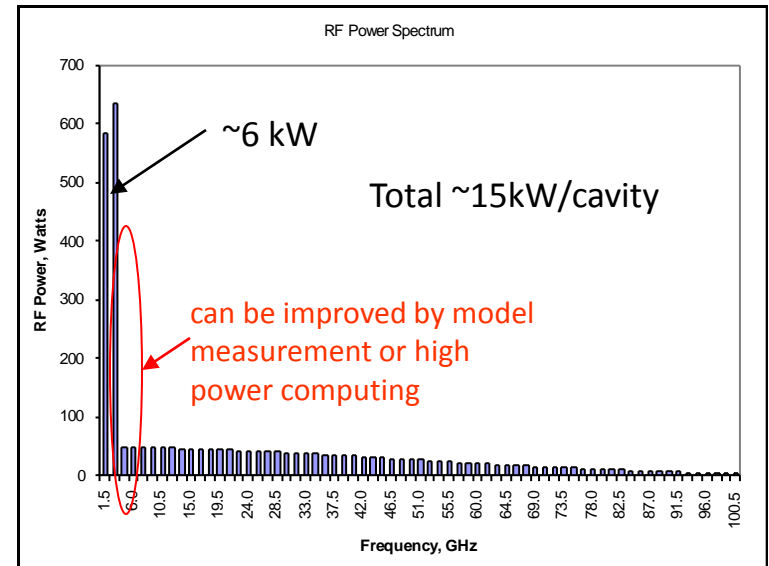


- Optimize shape to keep trapped HOMs (below beam pipe cut-off frequency) away from beam resonance to avoid huge HOM power.
- Preserve reasonable fundamental mode efficiency but maintain the iris size to give good HOM damping.
- Optimized shape also has to avoid multipacting barriers.

# Estimation of total HOM power extracted from the beam



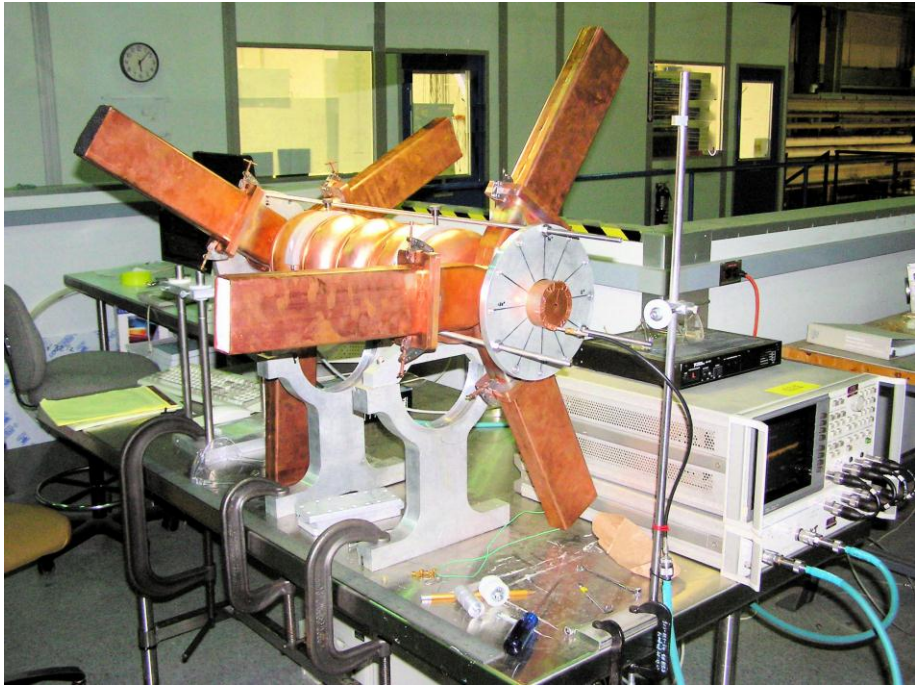
Monopole modes excited by on-axis beam



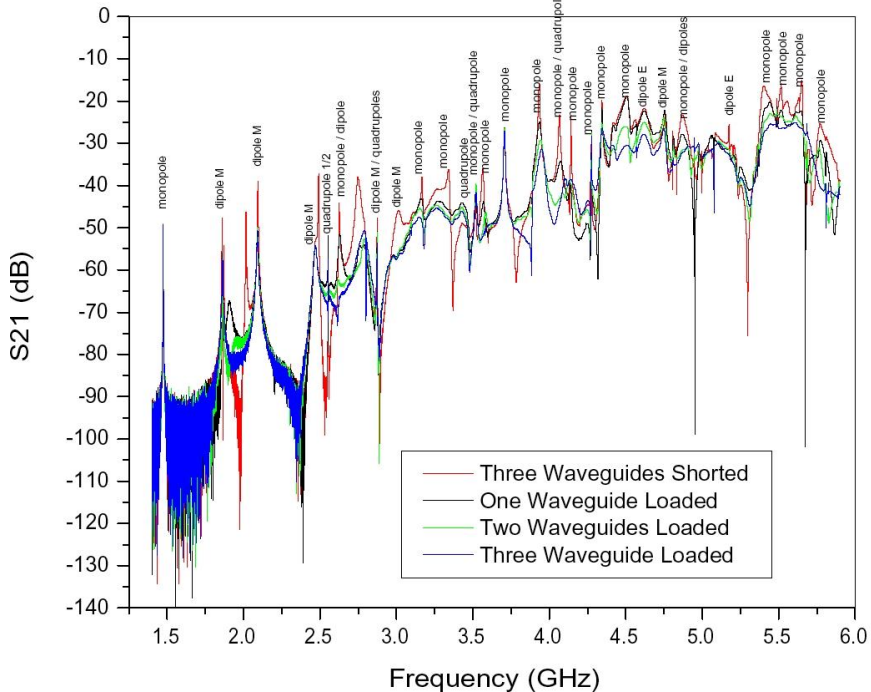
High-frequency tail estimated from broad-band impedance (loss parameter). Below cut-off from impedance spectrum. In between is uncertain so round up to ~20 kW.

beam excitation Frequency (GHz)	monopole modes only impedance (Ω)	dipole modes only impedance (Ω) at 1cm off-axis	beam peak current (A)	Monopole HOM power (W)	Dipole HOM power (W)	beam power (W)
1.497	180.713	2.326	4.000	2891	37	2929
2.994	196.794	1.578	4.000	3149	25	3174

# Copper 5-cell model measurement and data fitting techniques



1500MHz High Current Aluminum Cavity Model with One "Y" Waveguide Group



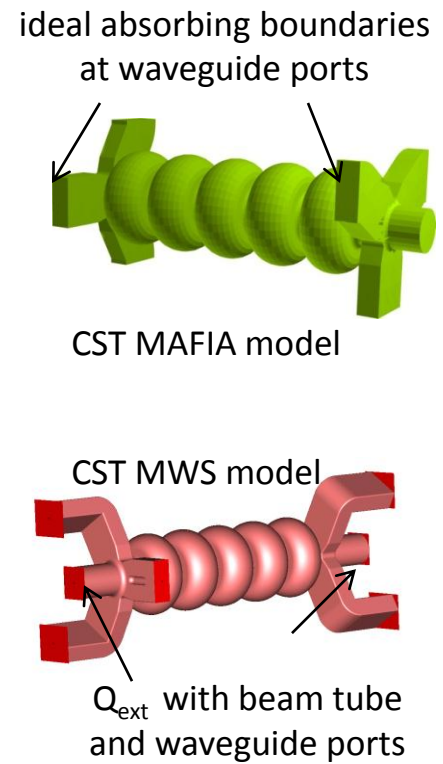
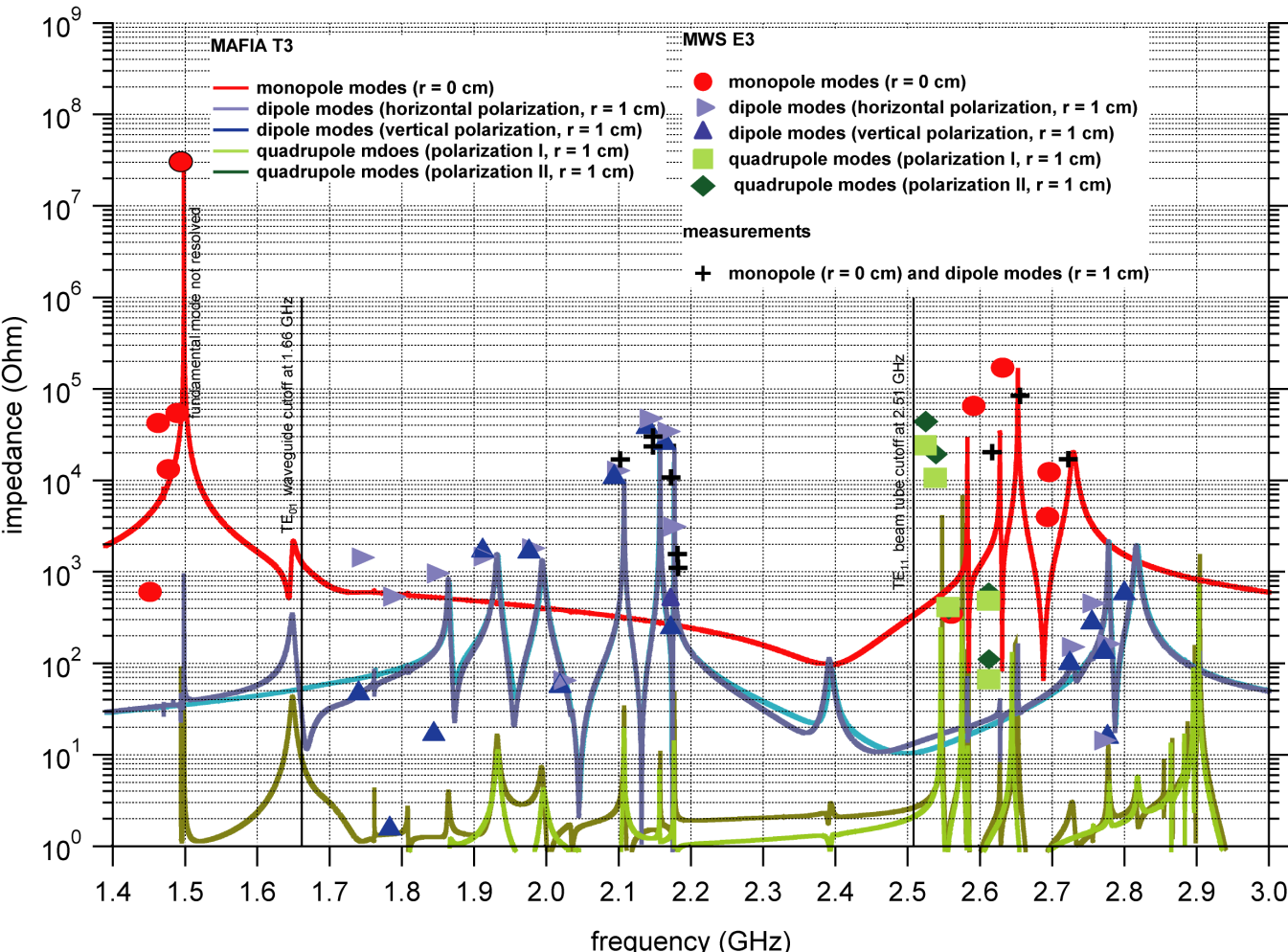
- S21 from beam pipe to beam pipe.
- Labview automation.
- Ceramic bead-pull on-axis or off-axis.
- End groups staggered 30° or 60°.
- 5, 6, 7-cell assembly.
- Data sets with dummy loads or shorts.
- Rotatable coupling antennas.

- Data set can be fitted by the 5-peak fitting algorithm first developed at LBNL to get freqs and Qs and amplitudes.
- Data analysis for mode successful
- BBU threshold needs to be verified in compact lattice.

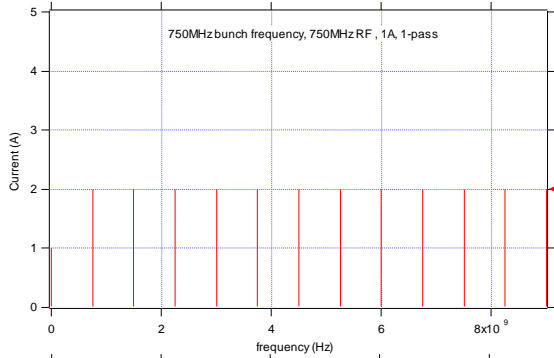
# JLAB HC Cryomodule Development

## Broadband HOM Damping Efficiency

- ❑ Most parasitic HOMs measured on warm model (“2 bead-pull measurement method”)
- ❑ Simulation also performed with Eigenmode solver of CST Microwave Studio (MWS)
- ❑ Conclusion: HOM damping requirements can be met to support Ampere-level of current
- ❑ Simulation and measurement in good agreement

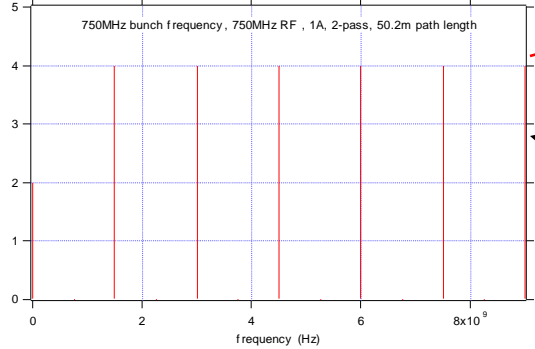


# Beam excitation spectrum depends on operation modes



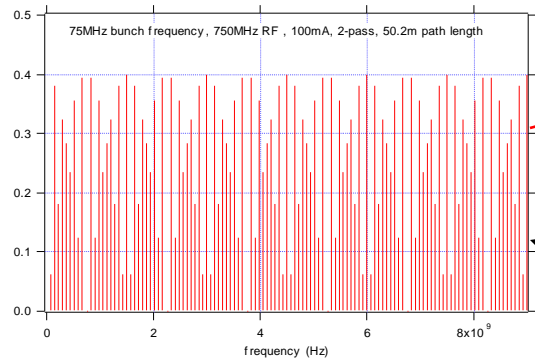
750MHz laser, 750MHz RF  
1A, 1-pass.

Single pass beam  
(every bucket filled)



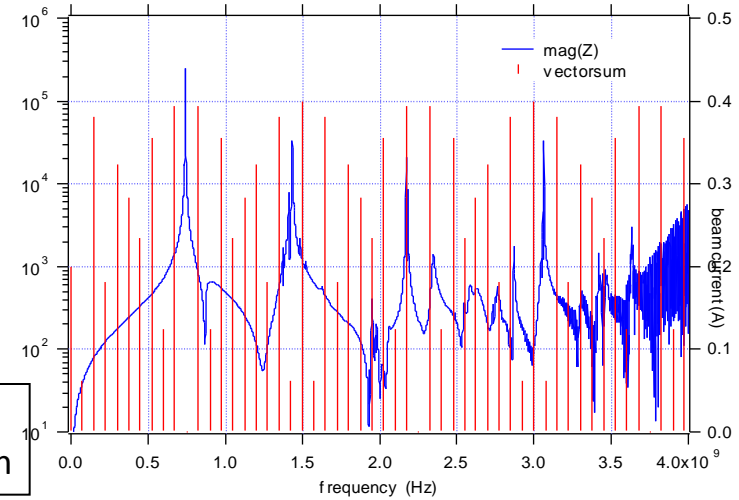
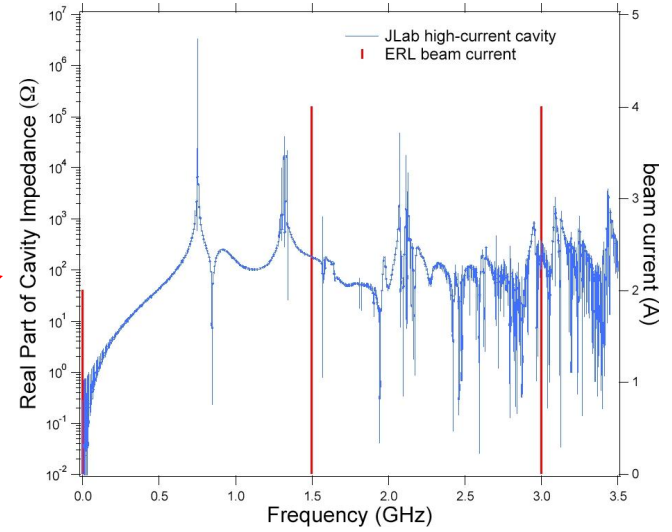
ERL (every bucket filled)

750MHz laser, 750MHz RF  
1A, 2-pass, 50.2m path length



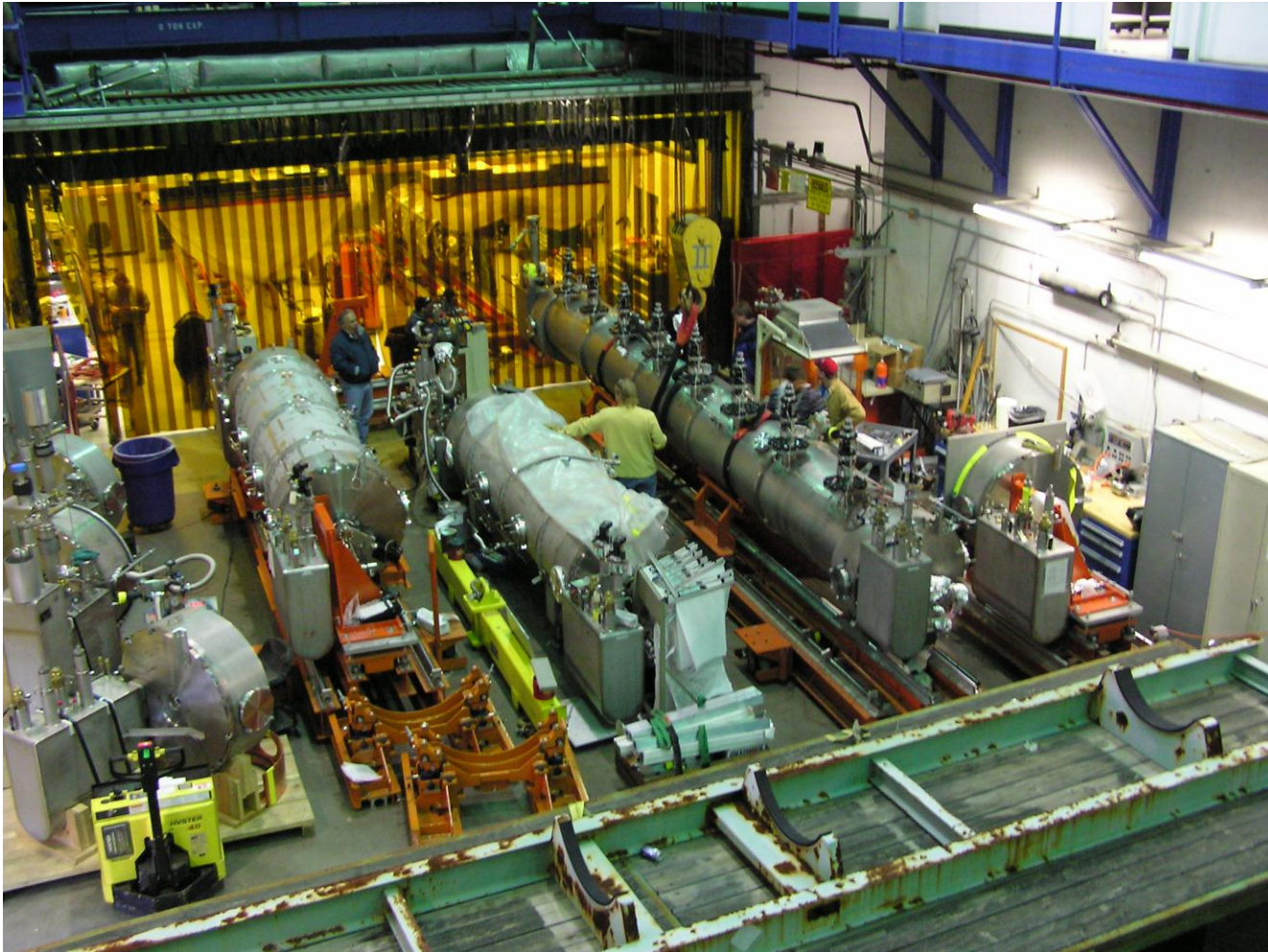
ERL (sparse fill)

75MHz laser, 750MHz RF  
100mA, 2-pass, 50.2m path length



[See JLAB TN-05-047](#)

# JLab Cryomodule experience



JLab has built ~74 Cryomodules of ~6 different types and built or processed >500 Multi-cell cavities.

# CEBAF Cryomodules

## 6 GeV CEBAF

- 50 MV(after rework)
- 12.5 MV/m CW average
- 1497 MHz
- 5-cell cavities
- Waveguide HOMs
- ~25 mA capable\*
- 6 kW FPC's
- Modular construction
- Waveguide FPCs
- Dog-leg cold waveguides



\*in Jlab ERL/FEL

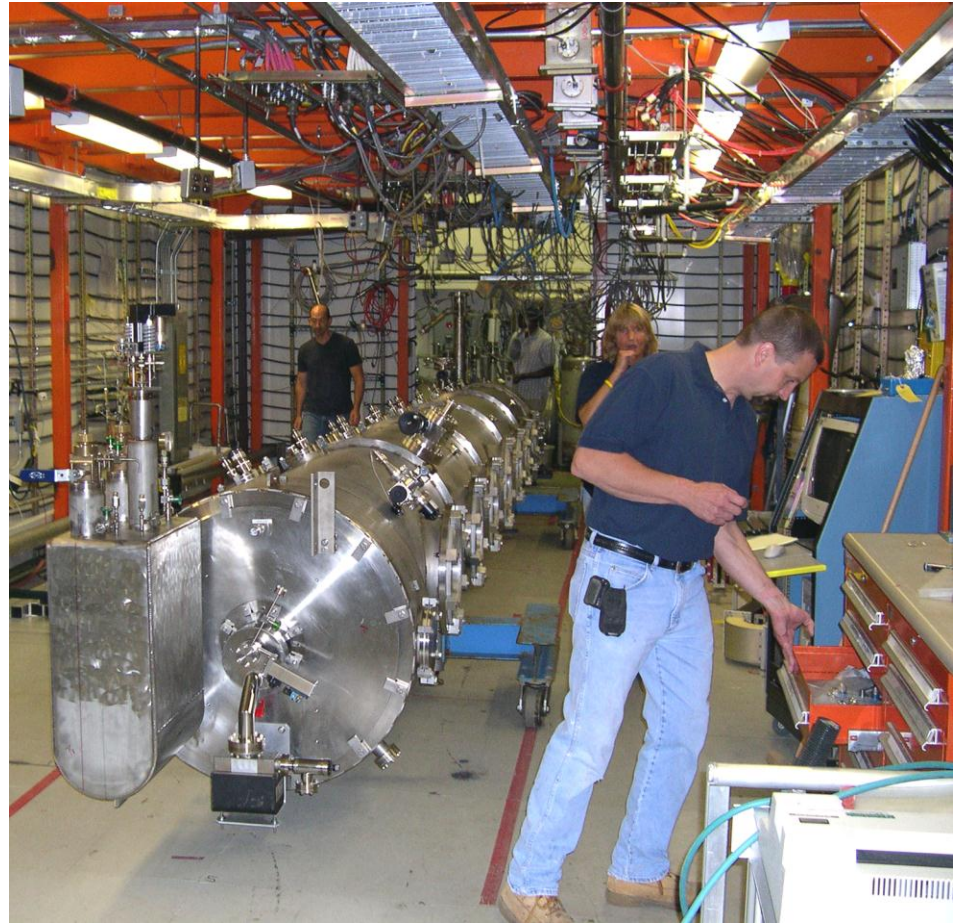




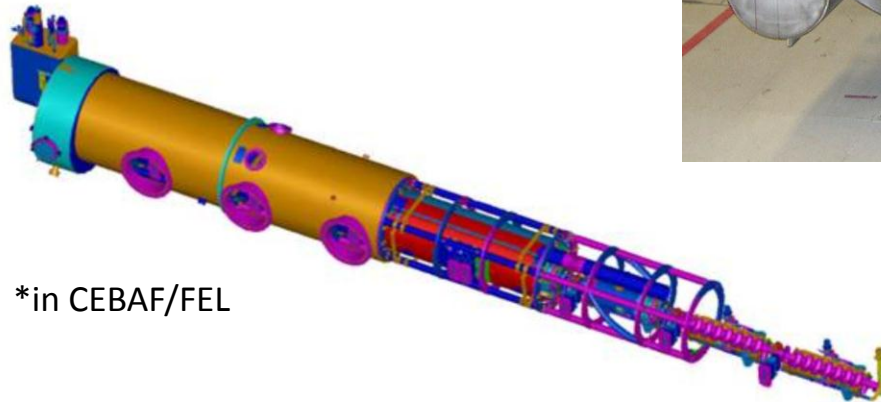
# CEBAF cryomodules

12 GeV upgrade

- 100 MV
- 20 MV/m CW
- 1497 MHz
- 7-cell low-loss cavities
- TESLA type HOMs
- ~1-10 mA capable\*
- 13 kW FPC's



“Renaissance” in test cave

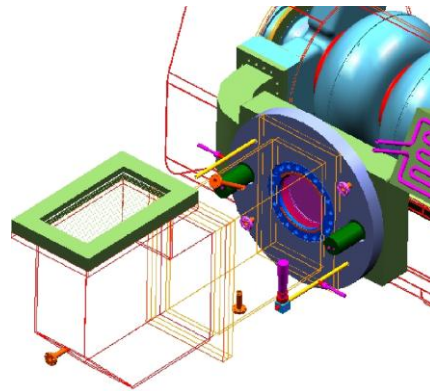
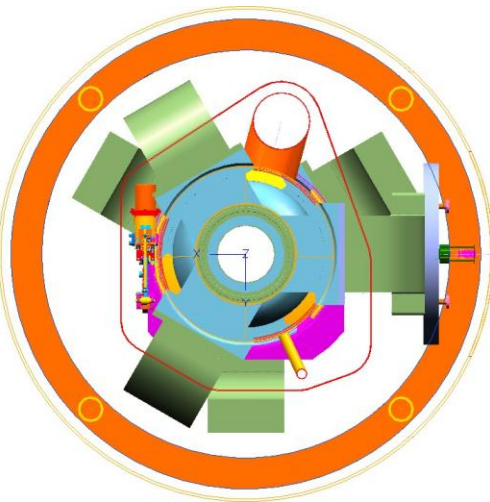
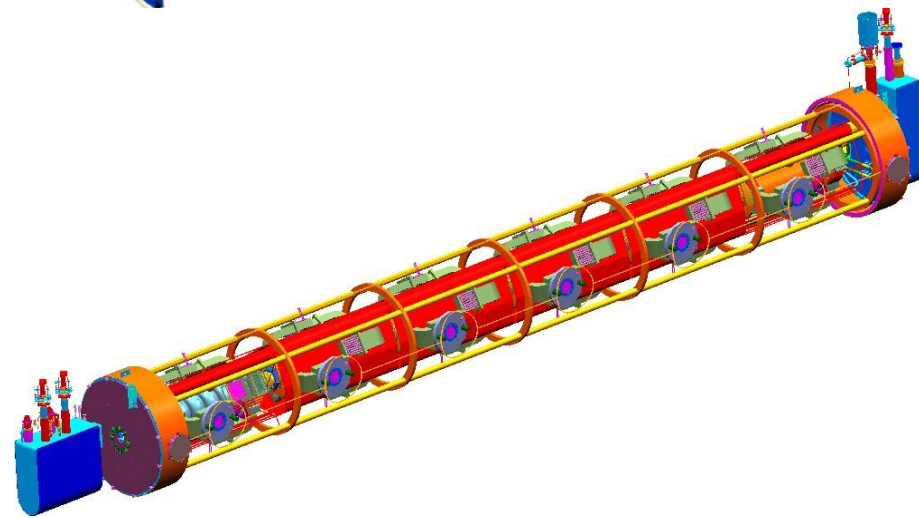
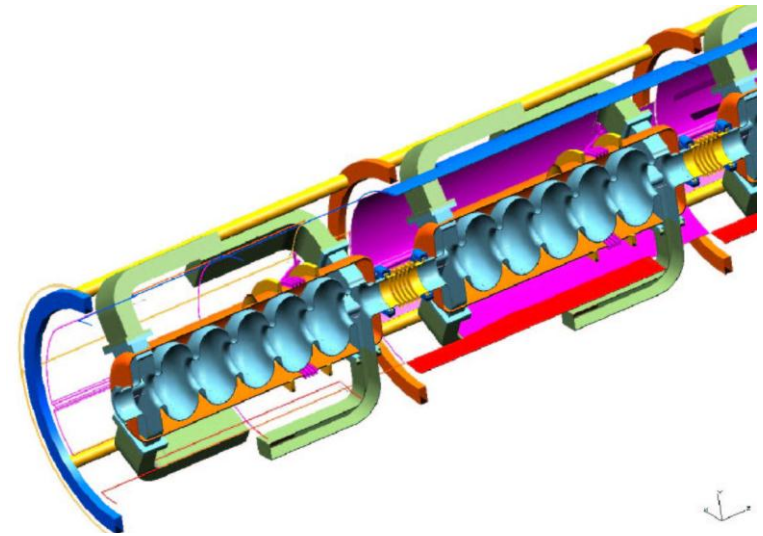


\*in CEBAF/FEL

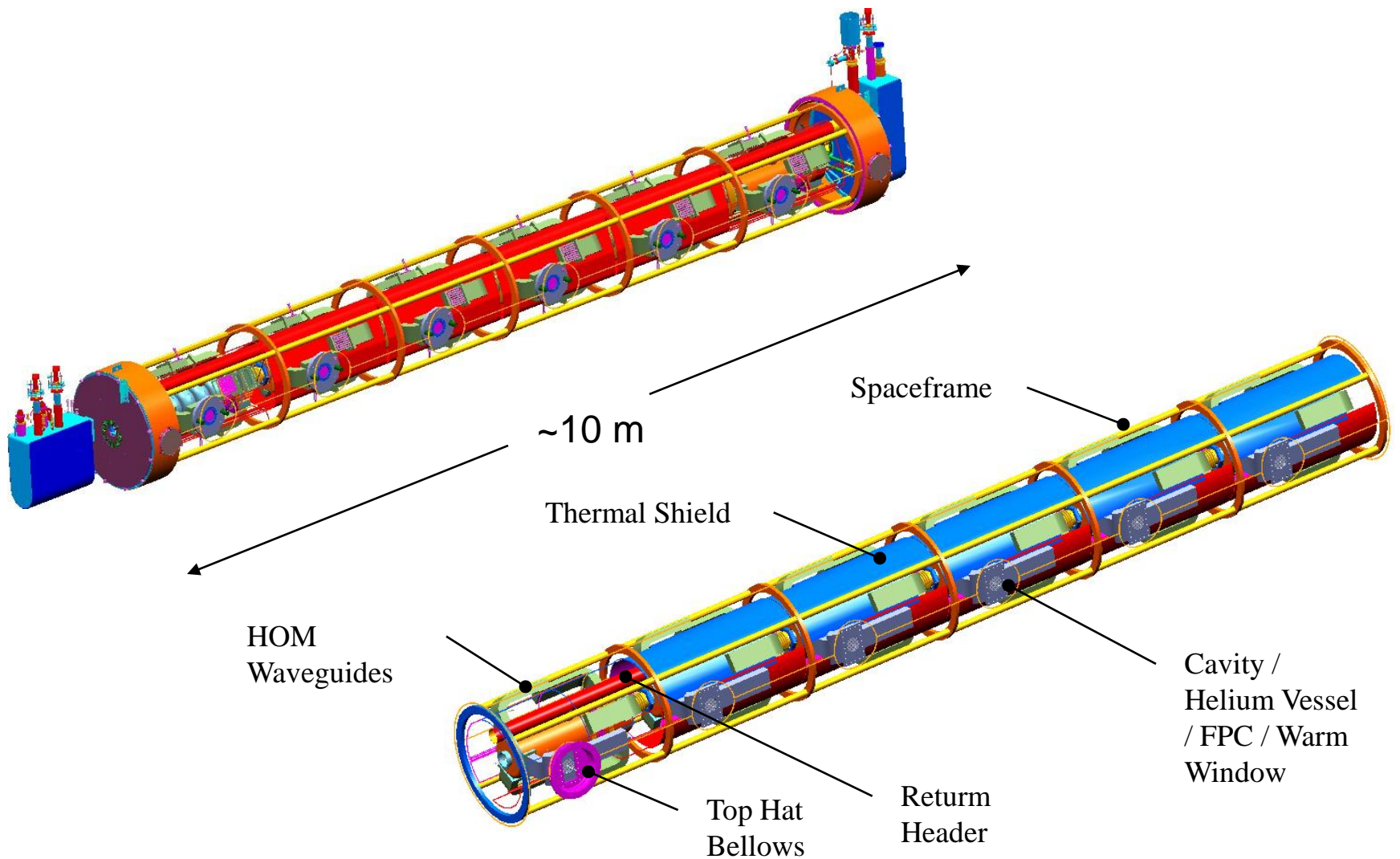
# General layout

750 MHz cryomodule with six five-cell cavities with waveguide damping

Frequency	750 MHz
# cells	5
Damping Type	Waveguide
Cavity Length	1.4m
Iris Diameter	14 cm (5.5")
# Cavities	6
Min. Module Length	10.4m
Nominal Module Voltage	100 MV (120 MV peak)
Cavity Gradient (Eacc)	16.7 MV/m (20 MV/m max)
Real Estate Gradient	~10 MV/m
TE <sub>111</sub> freq, Q <sub>ext</sub>	947 MHz, 9.5e2
TM <sub>110</sub> freq, Q <sub>ext</sub>	1052 MHz, 3.3e3
TM <sub>011</sub> freq, Q <sub>ext</sub>	1436 MHz, 7.1e2
HOM Power/Cavity	~20 kW(est)
BBU Threshold	>1A



# Jlab Ampere-class Cryomodule Concept



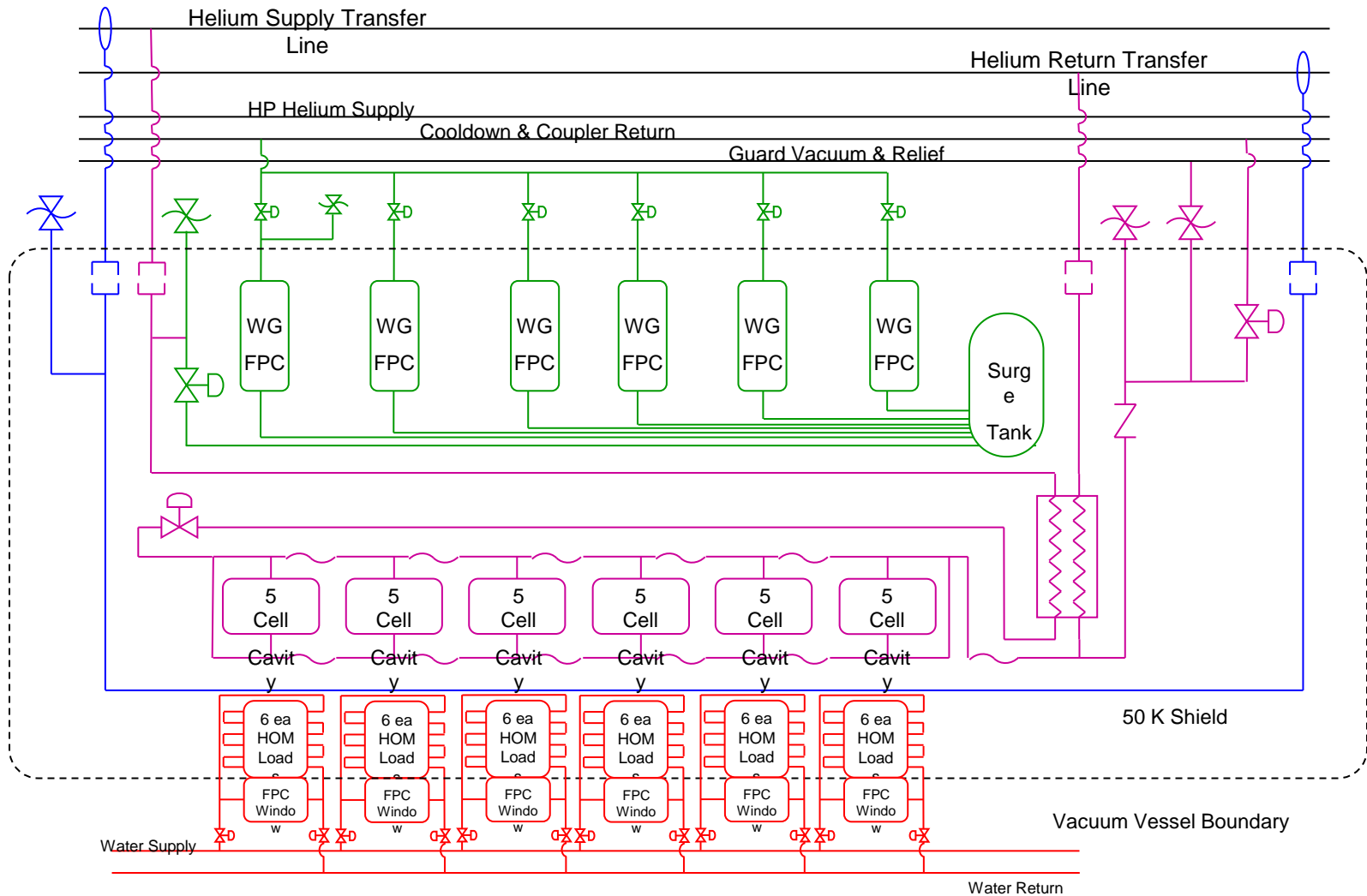
# Preliminary Heat Load Estimates (748.5 MHz)

	<u>2 K</u>	<u>50 K</u>
Static	73 W	362 W
(mainly FPC and HOMs)		
Includes u-tubes (10 W @ 2K, 30 W @ 50 K)		
May be improved?		

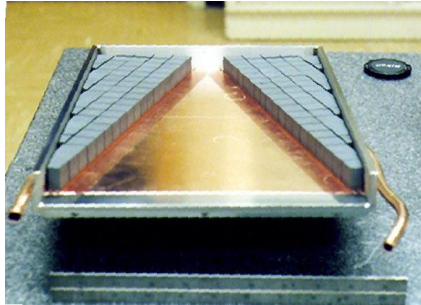
<u>Dynamic</u>	<u>382 W</u>	<u>188 W</u>
(cavity FPC and HOM RF losses)		
Total	455 W	550 W

Coupler Cooling ~ 1 gram/sec cool outer conductors

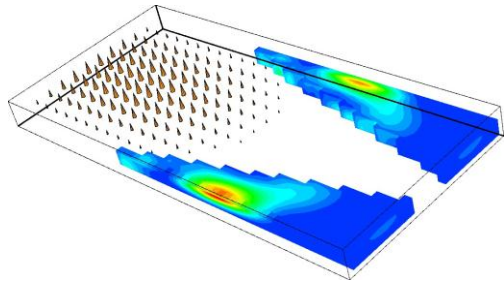
# Cryomodule Flow Schematic



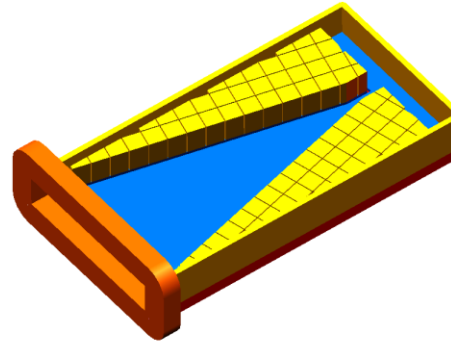
# HOM load and window based on existing designs



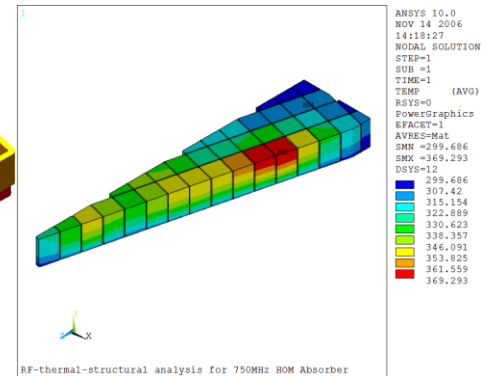
PEP-II HOM load



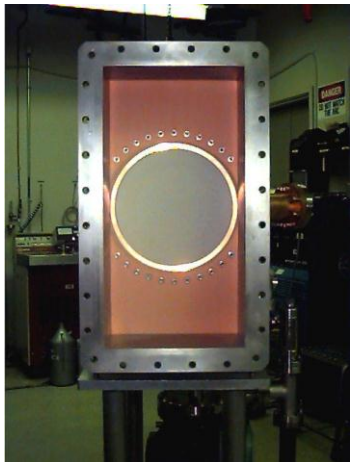
MAFIA model



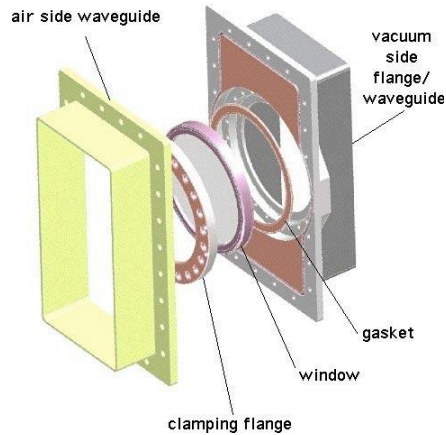
748.5 MHz version



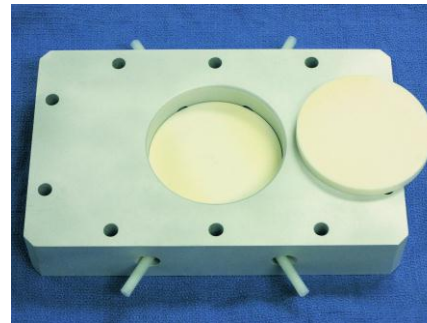
ANSYS multiphysics analysis



PEP-II window 476 MHz (WR2100)



LEDA 700 MHz, 1 MW (WR1150)



Cold model 1.3-1.5 GHz (WR650)

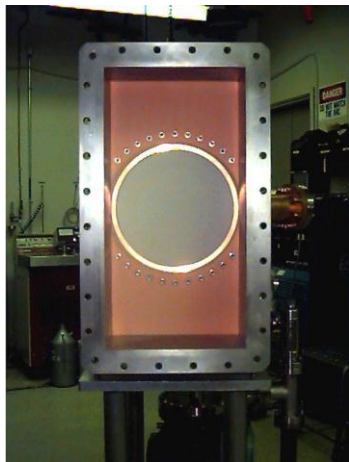


First Jlab built pre-stressed window

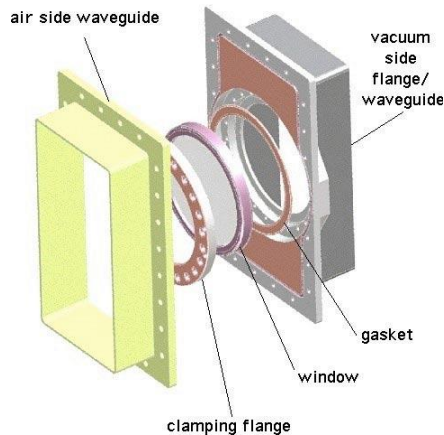
# Fundamental power coupler for 1 A CM

- Operating frequency: **748.5 MHz**
- Max FWD RF power **200 kW CW\***
- Sustain local peak RF power of **800 kW**
- No line of sight from the beam to the ceramic window
- Adopt proven pre-stressed waveguide window design
- Coupling set by distance from beam center line to waveguide step

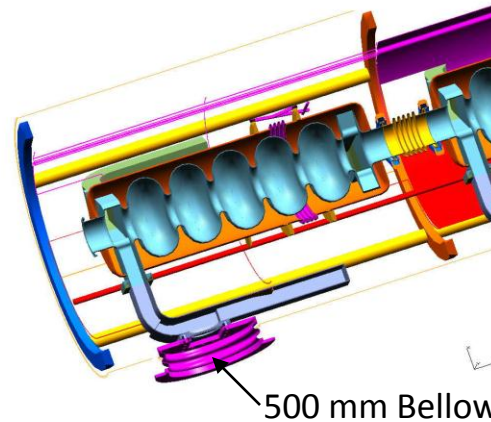
\* could go higher because of transient demands



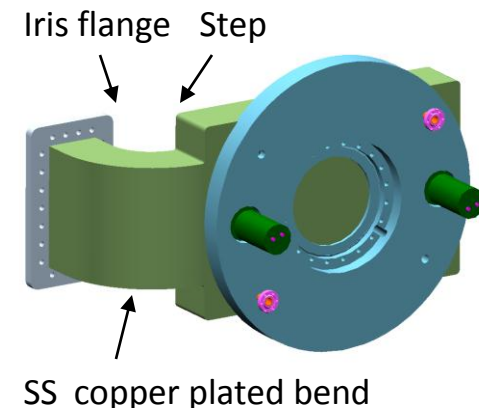
PEP-II window 476 MHz  
600 kW, (WR2100)



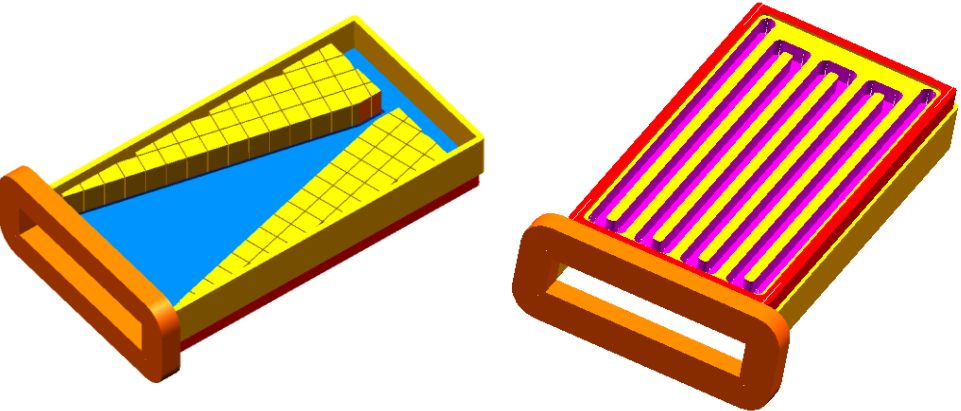
LEDA 700 MHz, 1 MW  
(WR1150)



1ACM 748.5MHz concept



# HOM load



High-power HOM load concept

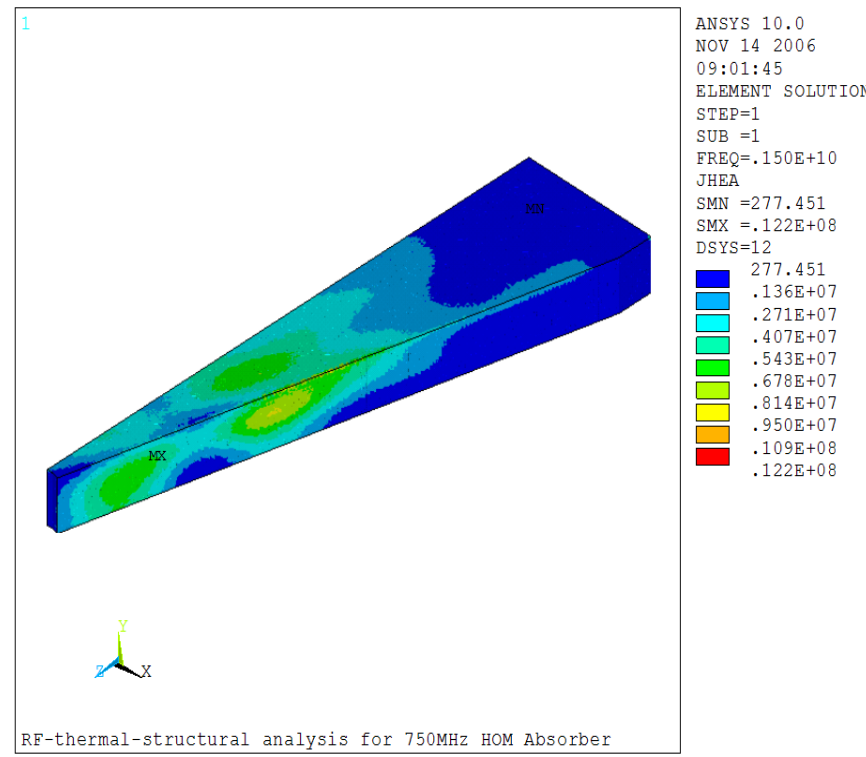
- RF heat summary

Freq. GHz	Input Power, W	Dielectric Loss, W	Surface loss, W	Total power loss, W
1.497	1775.200	1764.876	7.7799	1772.6557
2.994	1923.921	1909.972	8.6038	1918.5754
4.5	150.700	149.195	0.8314	150.0267
6	150.179	148.113	1.0018	149.1147
Sum	<b>4000</b>	3972.156	18.217	<b>3990.372</b>

99.5% of the RF heat is absorbed in tiles. Only ~0.5% surface heat loss.

- Joule heat densities

Joule heat densities at the interested four frequencies are calculated and superimposed for thermal analysis.



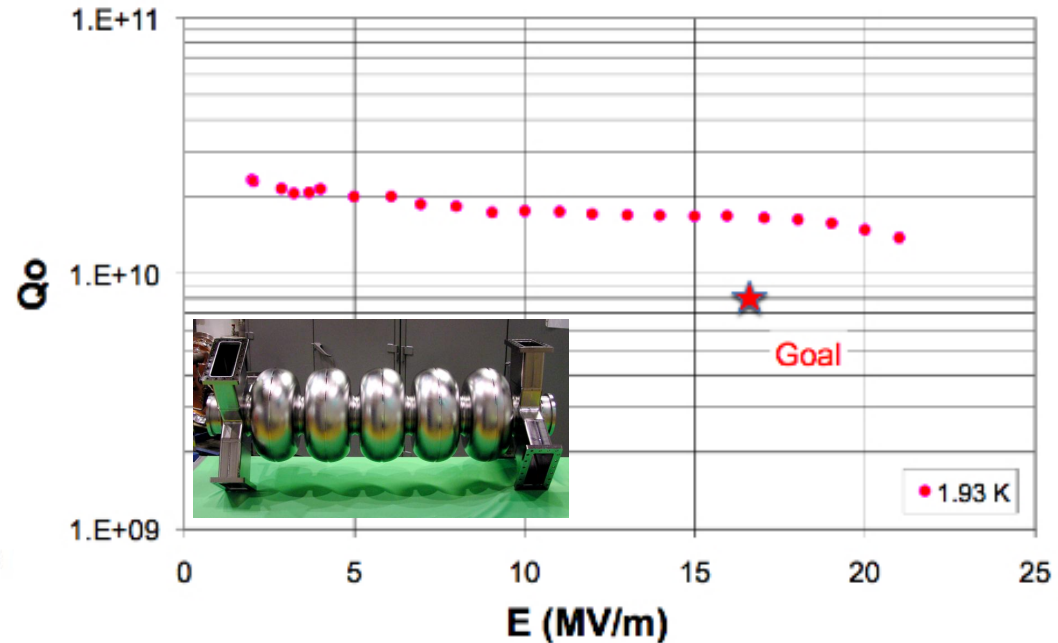
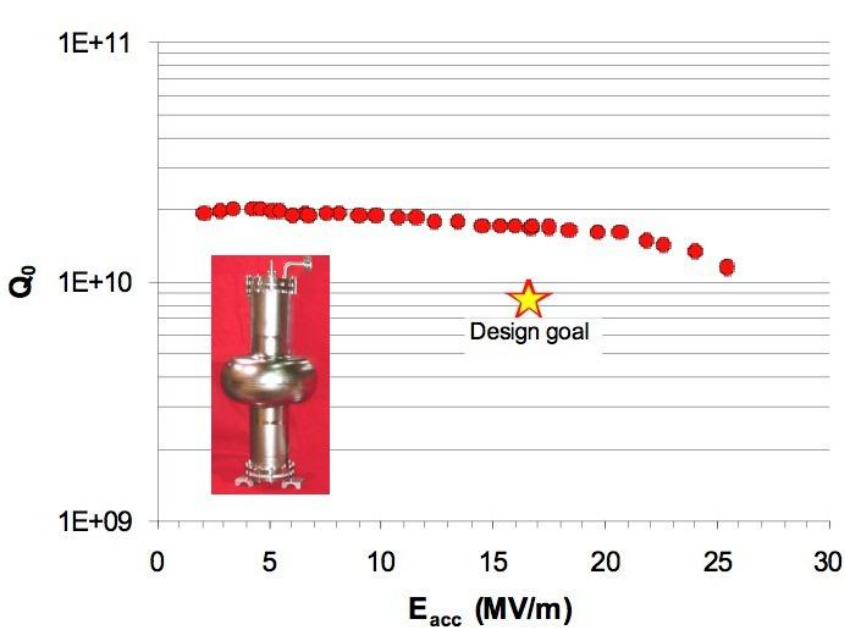


# Thanks to the JLAB “High Current” Team



From left to right:  
H. Wang  
P. Kneisel  
F. Marhauser  
R. Rimmer  
T. Elliot  
K. Smith  
E. Daly  
G. Cheng  
B. Manus  
L. Turlington  
S. Manning  
B. Clemens  
M. Stirbet

# 748.5 MHz HC first tests

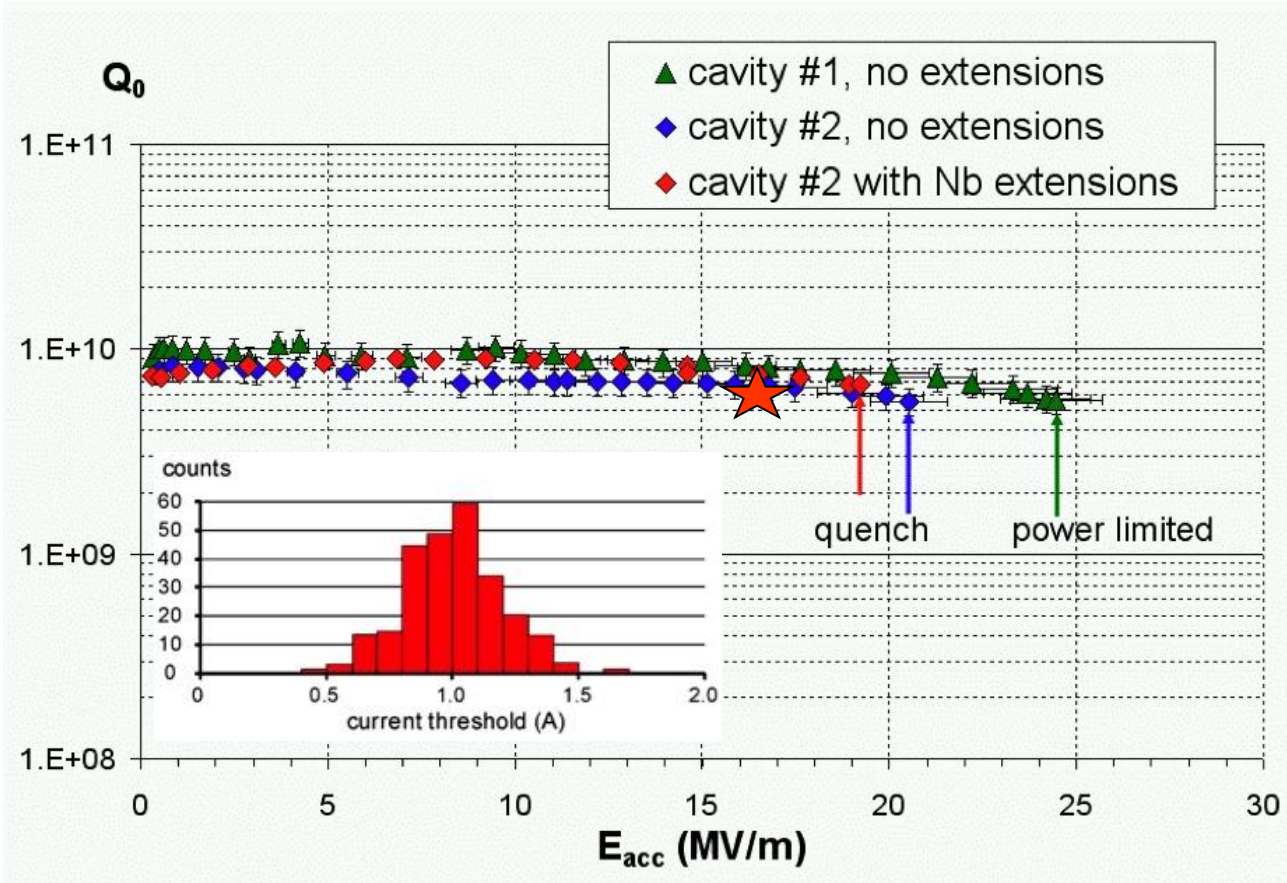
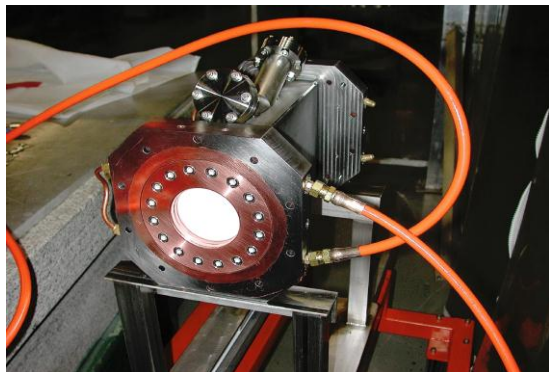


No Multipacting, RF power limited  
*Bulk BCP + 600C furnace outgass*  
*+ light BCP*

Multipacting seen from 3 MV/m  
but processed away in a few  
hours. FE/RF power limited.  
*Bulk BCP only, no furnace outgas*

# JLab 1497 MHz high-current cryomodules

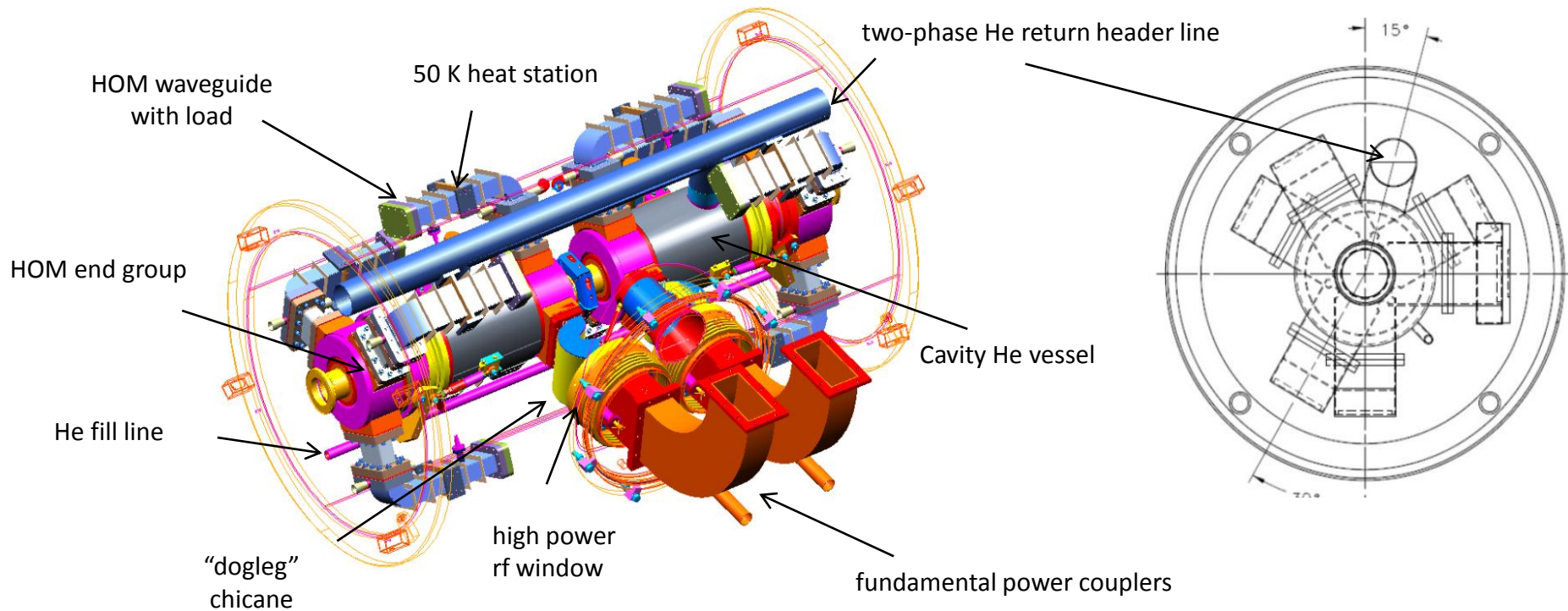
- Two half-scale prototypes of FEL high current cavity built and tested
  - Results exceed requirements for 4<sup>th</sup> gen. light source
  - Planned to build demo cryounit for beam test in FEL.



# JLAB 1497 MHz HC Cryomodule Development

HC optimized cell shape, 5 cells, WG FPC, WG HOMs

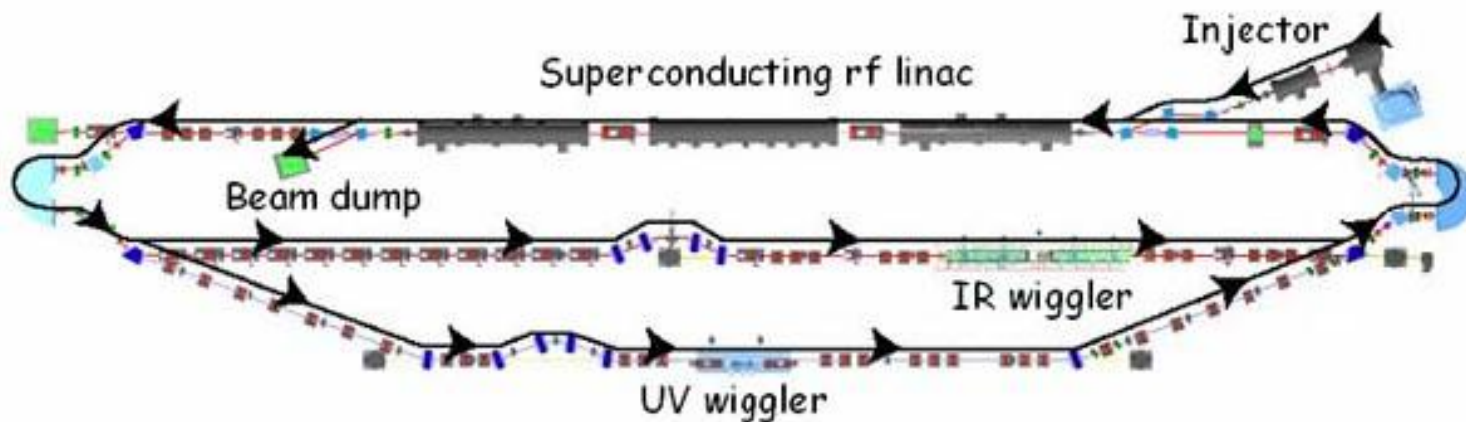
Planned for beam test in JLab FEL in 2010 (funding lost)



Conceptual design of a cavity-pair injector cryomodule (L=2.6m)

# JLab 10 kW FEL

- Fourth-generation light source with energy recovery
- The IR branch is operational (14 kW world record), while the UV branch is now under commissioning.

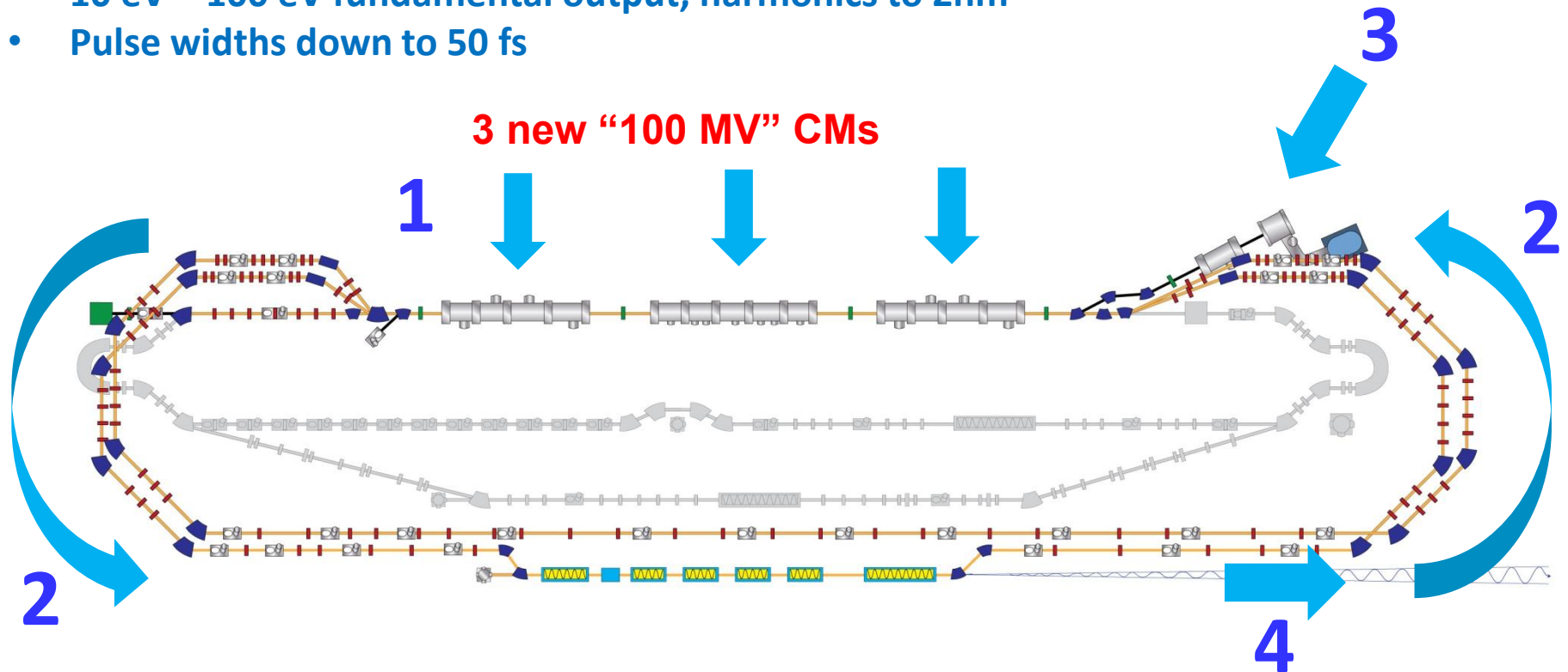


	IR Branch	UV Branch (under construction)
Wavelength range (microns)	1.5 – 14	0.25 - 1
Bunch Length (FWHM psec)	0.2 - 2	0.2 - 2
Laser power (kW)	> 10	> 1
Repetition Rate ( cw operation, MHz)	4.7 – 75	4.7 - 75



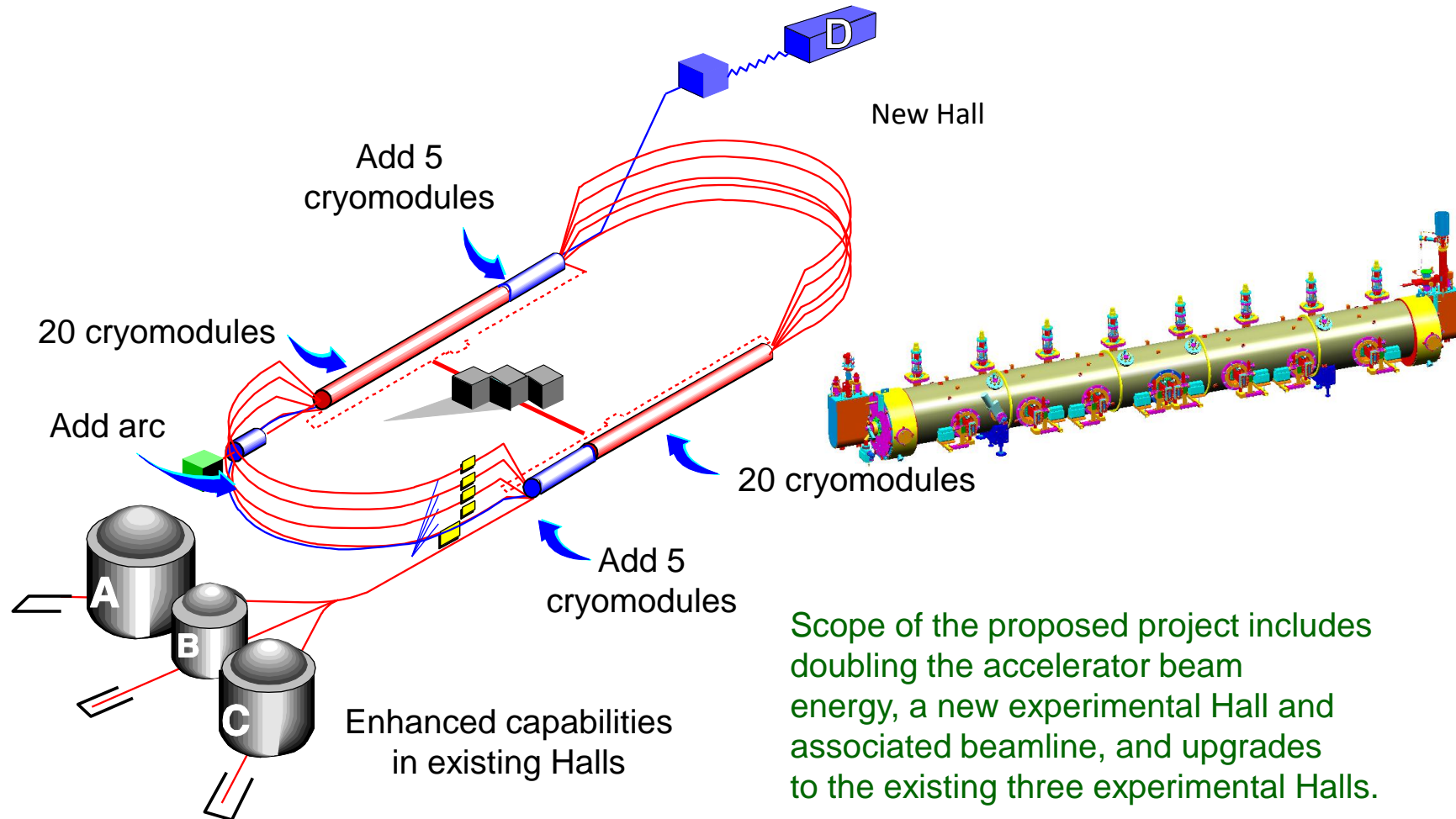
# Proposed: JLab FEL Conversion to JLAMP

- 4 steps
- 600 MeV, 2 pass acceleration
- 200 pC, 1 mm mrad injector
- Up to 4.68 MHz CW repetition rate
- Recirculation and energy recovery
- 10 eV – 100 eV fundamental output, harmonics to 2nm
- Pulse widths down to 50 fs



# SCOPE OF 12 GeV UPGRADE

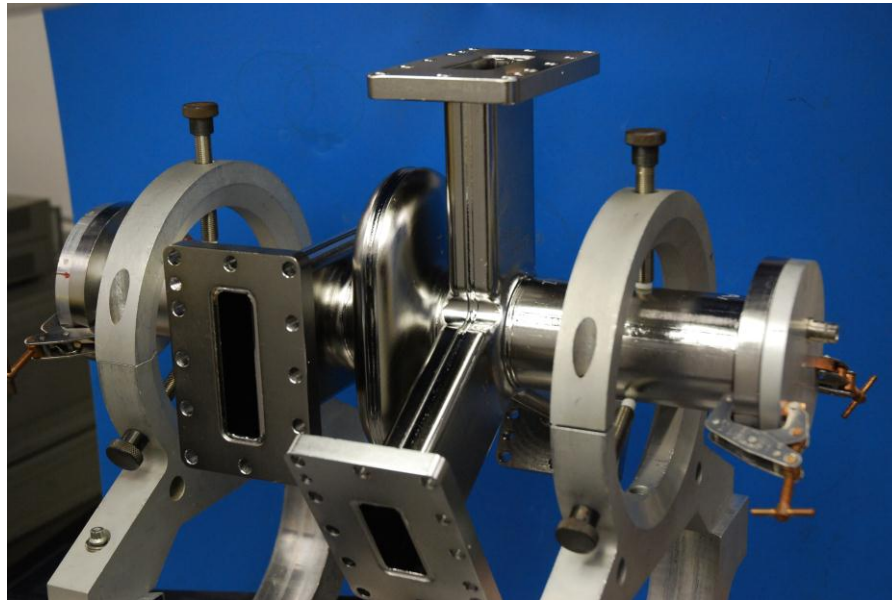
Upgrade is designed to build on existing facility:  
vast majority of accelerator and experimental equipment have continued use



Scope of the proposed project includes doubling the accelerator beam energy, a new experimental Hall and associated beamline, and upgrades to the existing three experimental Halls.

# New applications

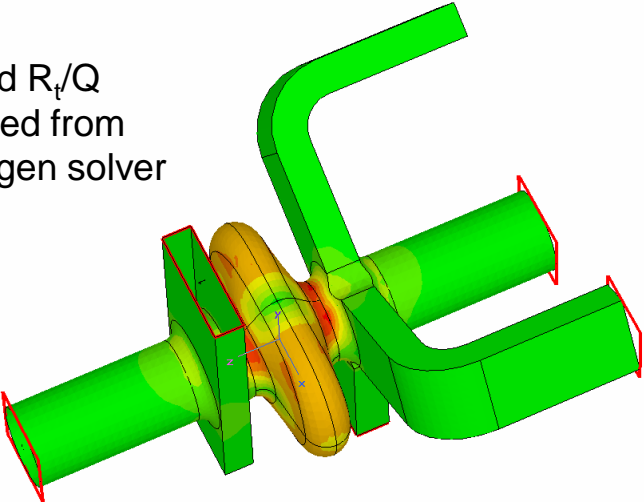
- ANL SPX baseline cavity
  - Up to 200 mA, 2x 8-cavity CM required
  - Strong HOM/LOM/SOM damping required
  - Possibility of moderate HOM power to loads
  - Short space available



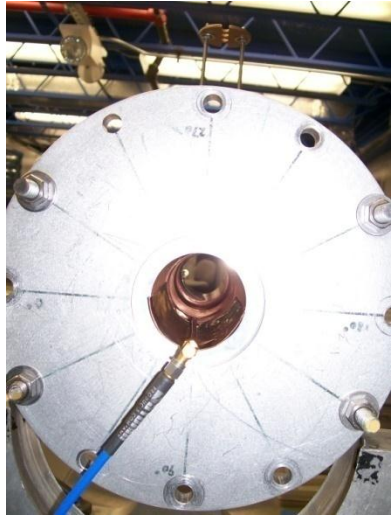
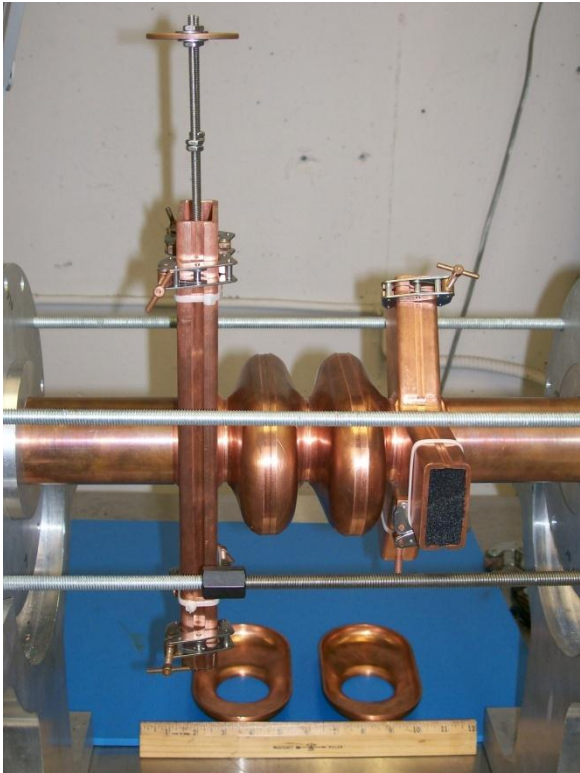
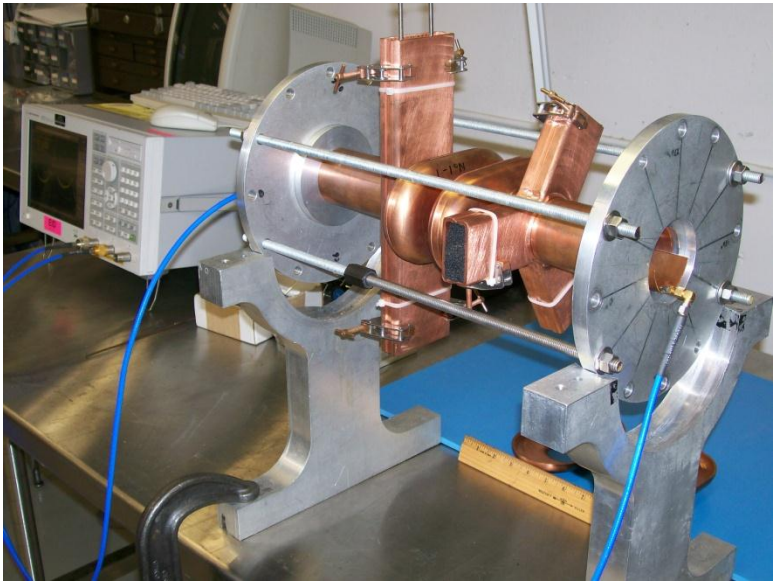


# Copper prototype, first reported in ICFA Shanghai Workshop, April, 2008

$R_{//}/Q$  and  $R_{\perp}/Q$   
Calculated from  
MWS eigen solver



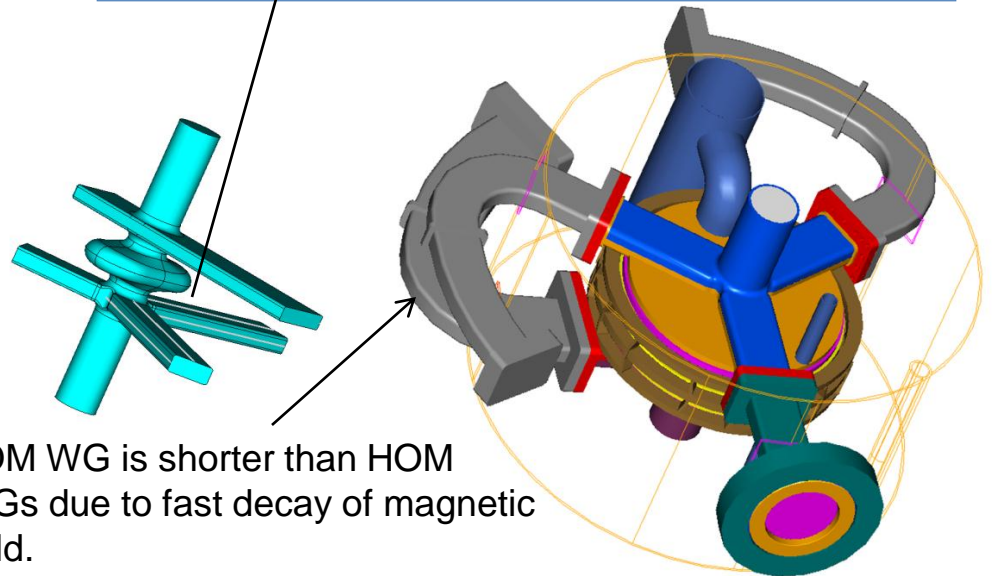
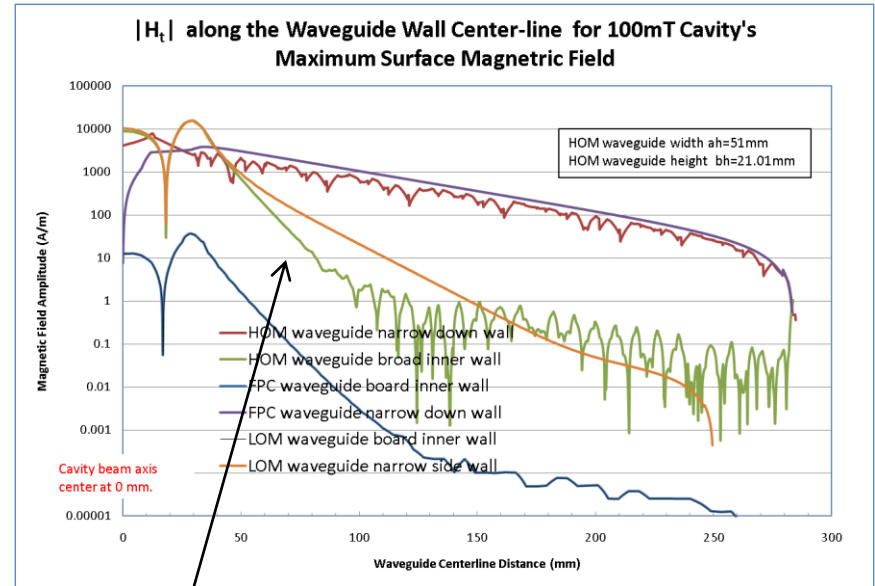
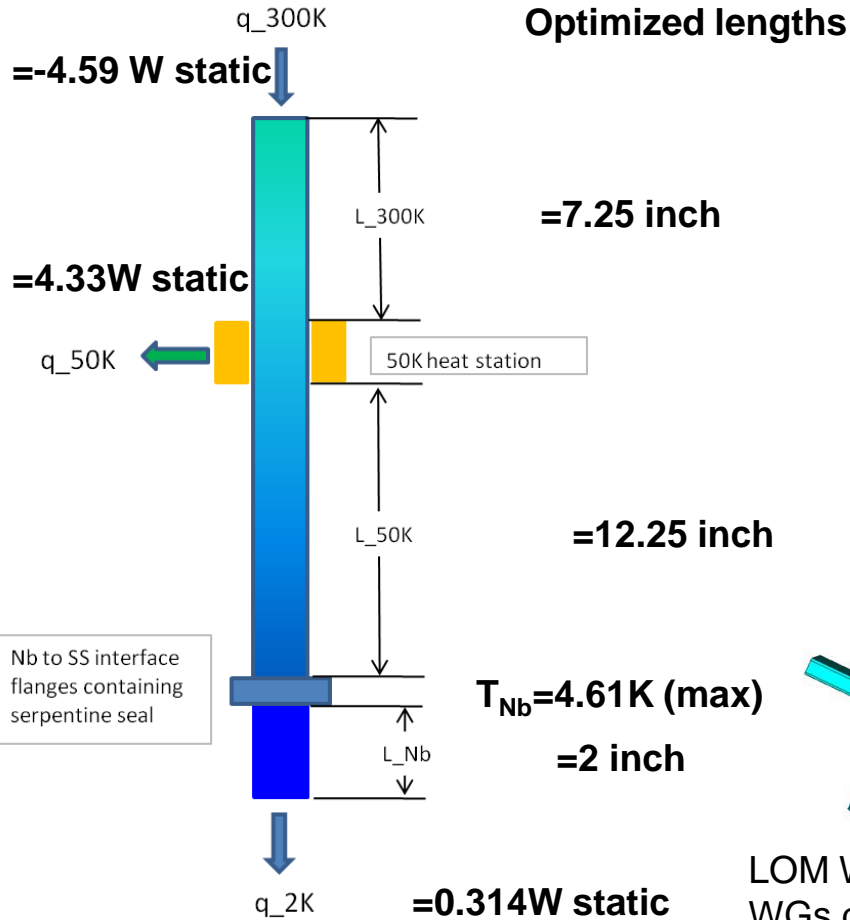
urrent (peak)



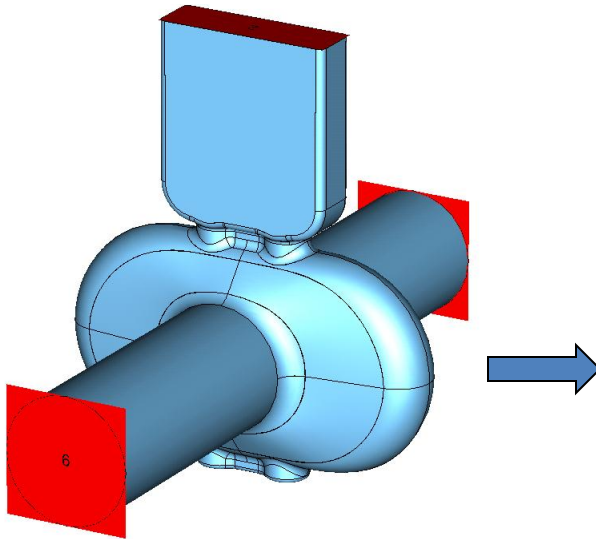
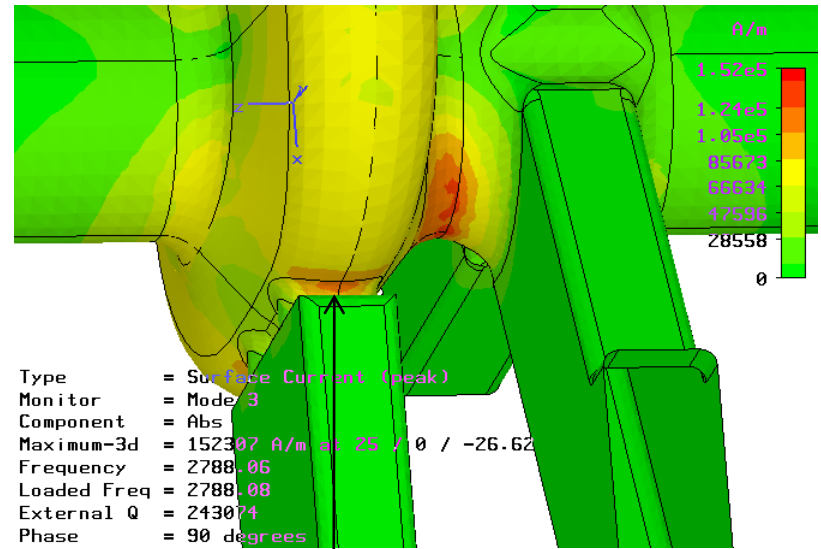
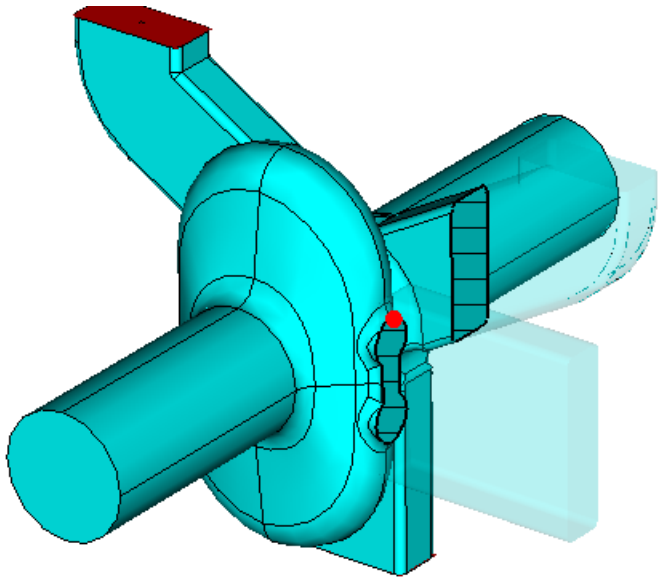
- Bench Qext measurement by using
- RF absorbers on WG ports
  - Clamping copper parts (low contact loss)
  - Weak coupling to VNA
  - Rotatable antennas to suppress the unwanted modes.

# Single-cell cavity LOM/HOM WG damper cryostat solution update

1-D RF-thermal model with SS WG, flange interface (AIMg seal) and heat station for HOM waveguides



# Something new? On-cell LOM/HOM Damping



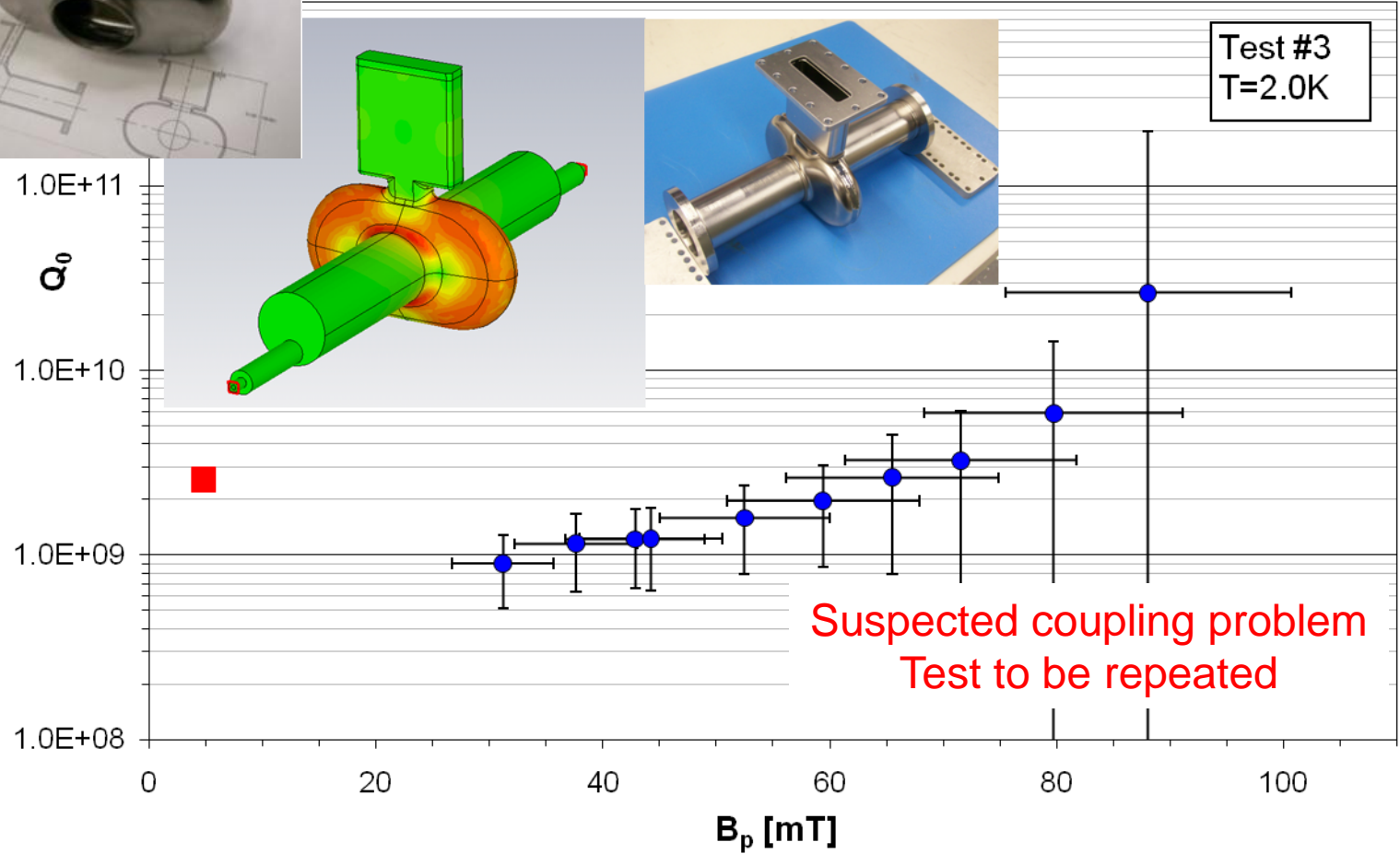
- $B_{\text{neck}}/B_{\text{iris}} \approx 0.8$
- $B_{\text{max}}/V_{\text{def}} = 157.7 \text{ mT/MV}$  (single-cell iris)  
to  $195.6 \text{ mT/MV}$  (+end WG iris)
- dummy “dog bone” stub, one on-cell damper is better than two, more promising.
- LOM-WG mode, 2.176GHz,  $R/Q=22.3\Omega$   
 $Q_{\text{ext}}=21$ .
- To be confirmed

# Proof-of-principle model of on-cell damper crab cavity



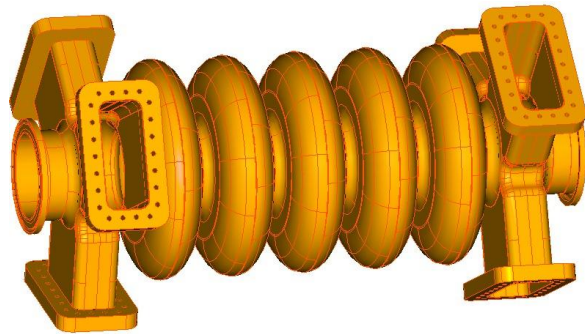
● TM110-pi    ■ TM010

by Peter, Gigi, Ben and Haipeng etc on Nov. 11, 2009.



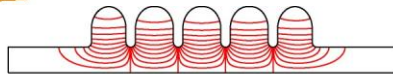
# High-current Proton driver cavity?

- Development from electron cavity for  $\geq 100$  mA

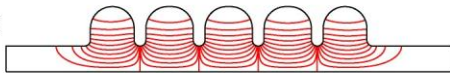


F. Marhauser  
PAC09

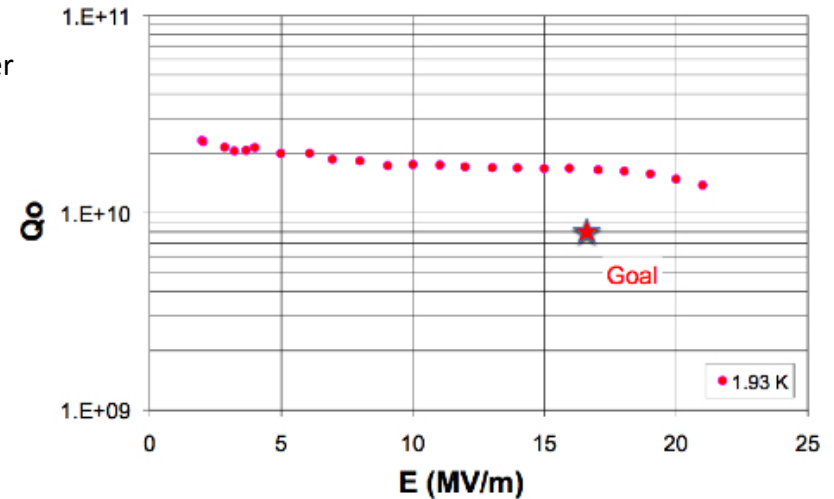
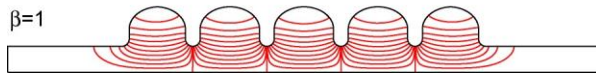
$\beta=0.65$



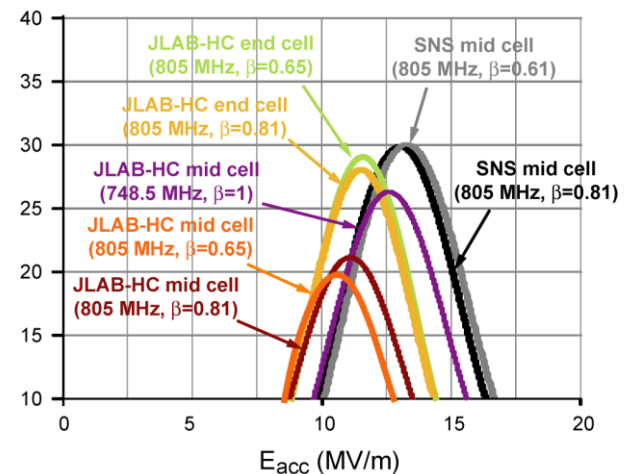
$\beta=0.81$



$\beta=1$

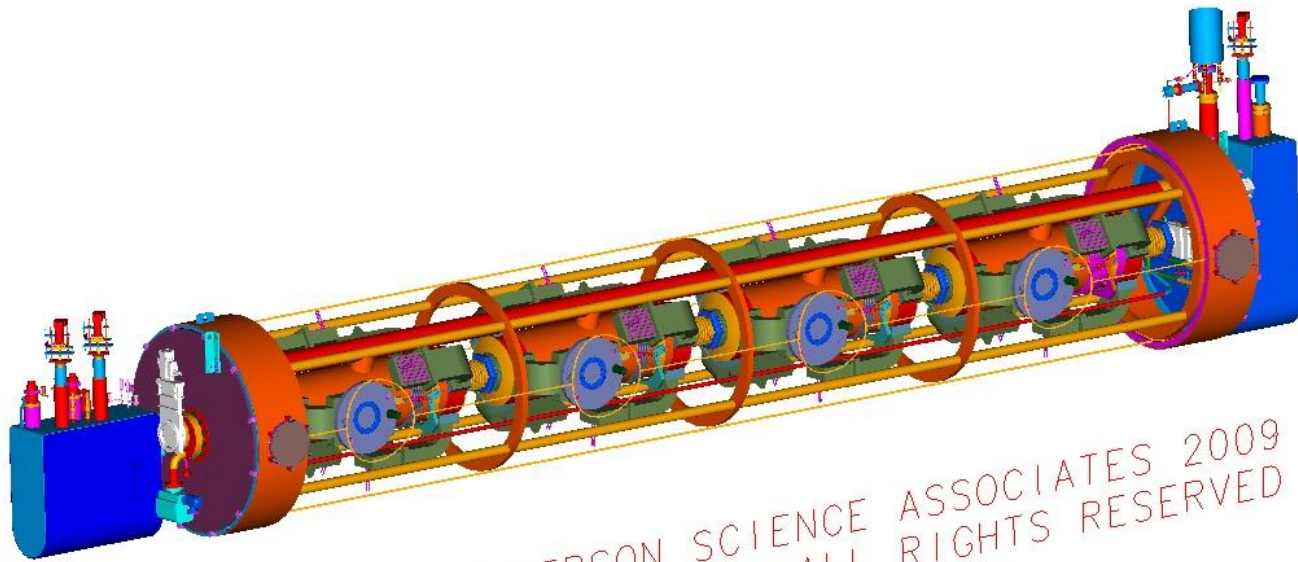


impact energy (eV)



# E.g. high current cryomodule

- JLab 704 MHz module (based on modified SNS layout)
- Could be economical if can operate in BCS dominated regime
- Very large apertures (halo!) Very high BBU threshold
- Use TV band RF sources



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# WG Summary

- HC Cavity shape chosen for good efficiency, HOM properties
- 5-cells good compromise at 748.5 MHz.
  - BBU > 1A.
  - Good packing factor, ~10 MV/m real estate gradient.
  - Fits in existing Jlab infrastructure (just).
- Waveguide HOM dampers give good Q's, loads at 300K.
- Waveguide FPC/warm window has high power capacity.
- Module concept is compact and based on experience.
- Hardware prototypes Successful at 748.5 & 1497 MHz
- May find new applications
- On-cell damper looks promising

# Discussion

Effective HOM damping frequency range **Cut-off to infinity**

Coupling to high frequency modes? **Yes?**

Measured and/or simulated HOM Q-values for given cavity design vs. frequency **Good agreement between simulation and measurement**

TJNAF designs and results **yes, see above**

Maximum HOM power handling and extraction **>20 kW**

Estimate of the heat load to ~2K and all other intercept temperatures at full HOM power **12 static, 64 dynamic W per cavity, ~92W at 50K.**

Coupling to the fundamental mode and suppression **anything you want**

Cleanness challenges and solutions **no problem**

Cleaning of waveguide sections **standard procedures**

Extra beamline length required per cavity (compared to linac without HOM damping) **less than 1 cell length**



# Discussion 2

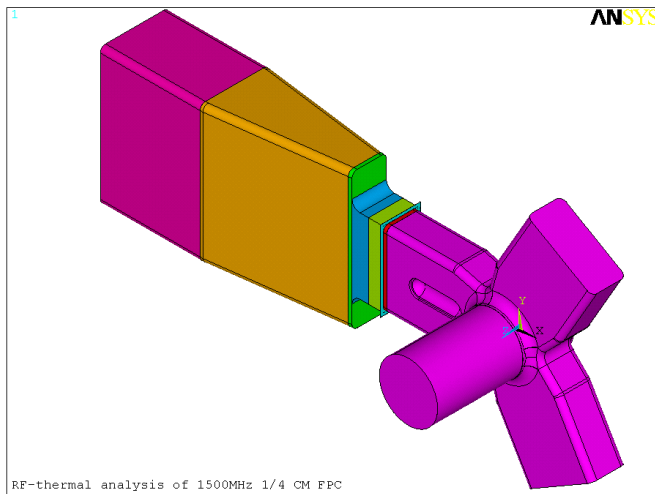
Mechanical / fabrication challenges and solutions **He vessel**  
Cost vs. design and material choices **Cheap and easy**  
Superconducting or normal conducting waveguide sections? **NC, warm loads for anything above 200  $\mu$ A**  
Number of waveguides per cavity required **1-6**  
Length of waveguide section **just long enough?**  
Absorber inside or outside of vacuum vessel? **Inside for broad-band**  
Water cooling vs. cryogenics; risks involved **Water, if needed**  
Temperature of loads at end of waveguides **Toasty?**  
Shielding of IR radiation from warm load **Not an issue?**  
Water cooling and mechanical cavity vibrations **Possible?**  
Other challenges, limitations and solutions **FUNDING**

Backup material

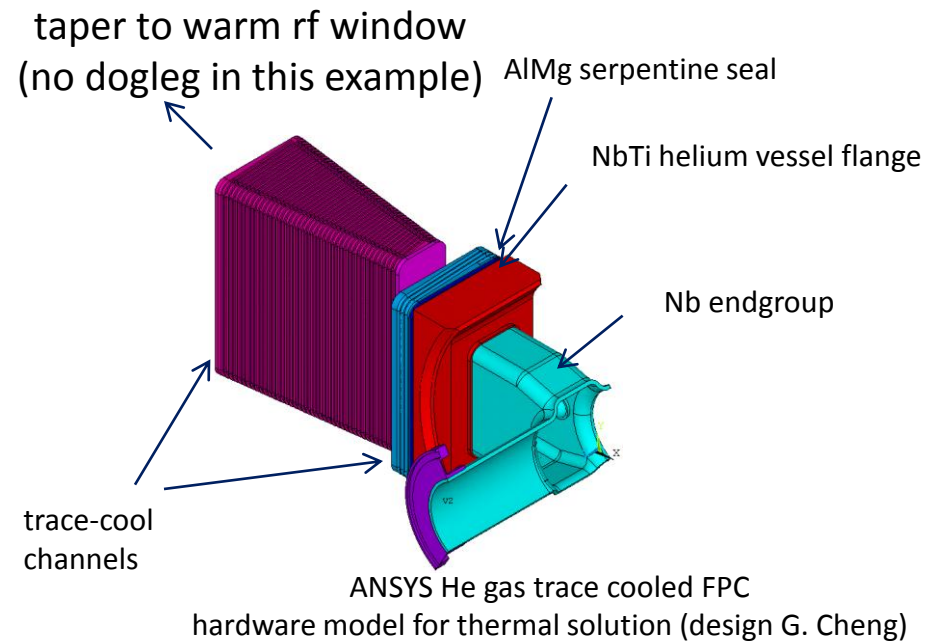
# JLAB HC Cryomodule Development

## Fundamental Power Coupler (FPC)

- ❑ One HOM waveguide steps up in size and used as FPC (does double duty)
- ❑ Length of small waveguide and incorporated bumps determine the coupling factor (10mA injector (not energy recovered):  $Q_{ext} = 9.5e5$ )
- ❑ Issue: Static leak and rf heat leak to 2K needs to be intercepted/minimized
- ❑ Active cooling necessary (e.g. He gas trace cooling of the waveguide)
- ❑ Optimization is challenging, since He gas heats up and covers regime of laminar, transient and turbulent flow → highly non-linear problem only solvable with multi-physics code (ANSYS)
- ❑ Warm-to-cold transition still needs to be further optimized



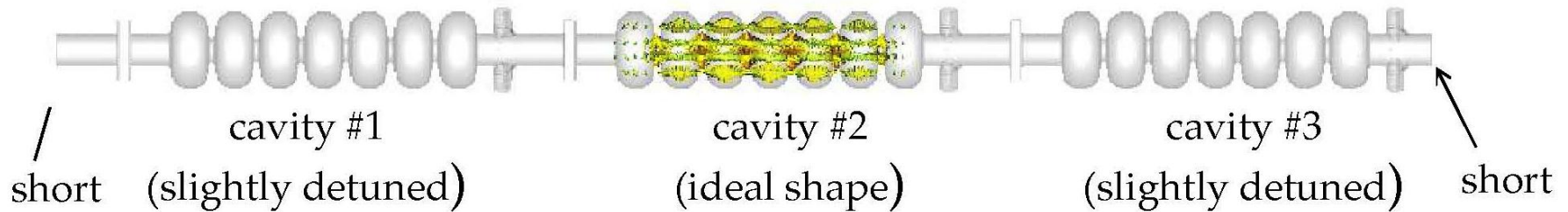
ANSYS vacuum model for RF solution



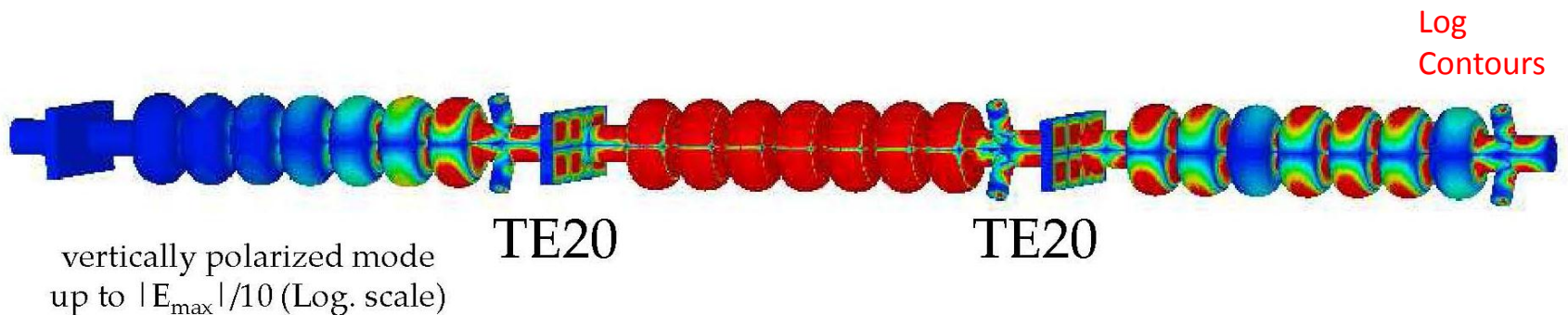
# Simulation of real module conditions

## CST Microwave Studio Eigenmode Solver Simulations (MWS) - Trying to resemble real World -

### □ Simulation of cavity string



- how far and strong the field propagates in neighboring cavities may depend on detuning
- cavities share 2 HOM couplers and 2 FPCs (except for cavity at end of cryomodule)



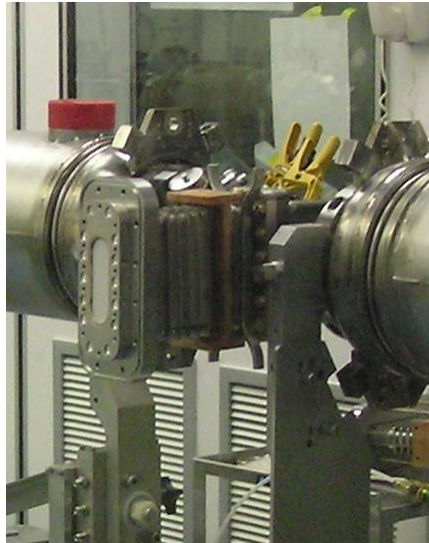
# Power couplers

- Various coupler configurations are available



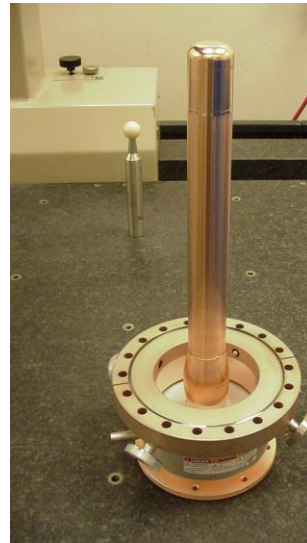
CEBAF waveguide

- Peak power up to 6 kW CW
- 2K and 300 K windows
- Dogleg shields cold window from beam.



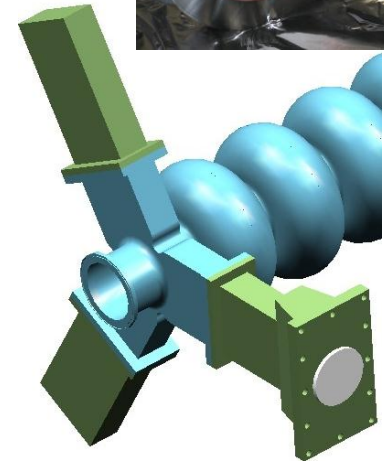
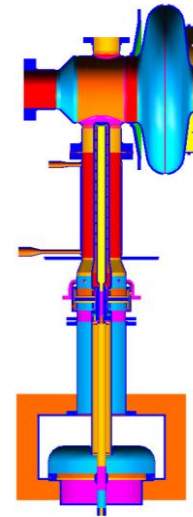
Upgrade WG coupler

- Peak power in up to 13 kW CW
- 300 K window
- Cooling: WG heat stationed at 50K
- Optional active cooling
- Optional double warm window



SNS coax coupler

- Peak power in up to 550 kW (tested up to 2 MW)
- 1.3 ms RF on. 60 pps
- Up to 50 kW average power
- $Q_{\text{ext}} \sim 7 \times 10^5$
- 300 K window
- Cooling: Inner conductor extension: water. Inner conductor: conduction cooling. Outer conductor: GHe flow

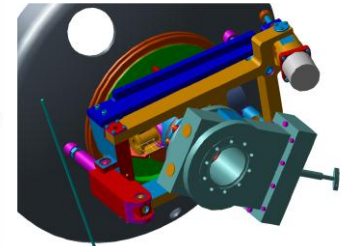
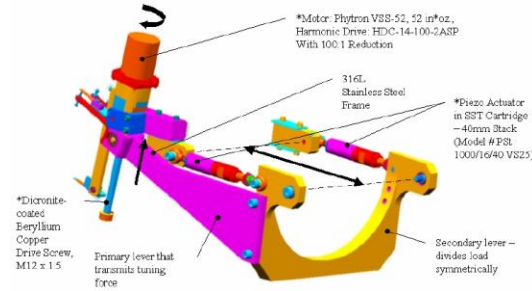
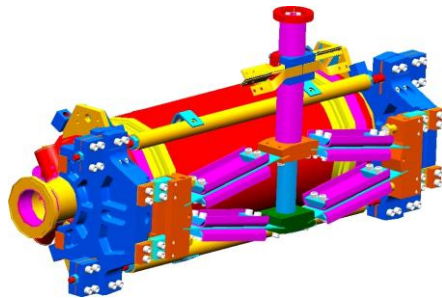
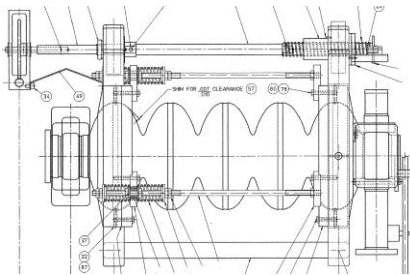
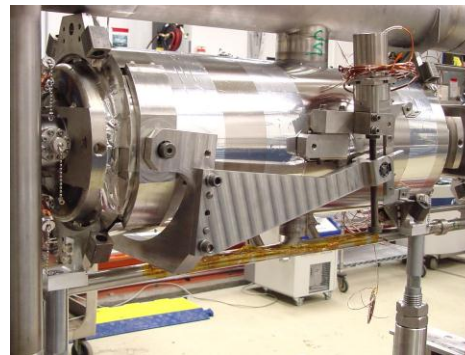
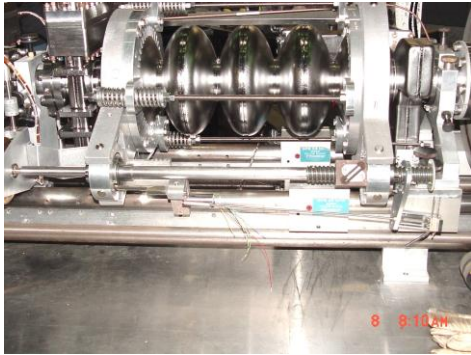


FEL high-power WG

- Peak power in up to 200 kW (Window tested to 1 MW CW)
- 300 K window
- Cooling: Window: water. WG transition: GHe flow
- Dogleg or bend (not shown) to avoid exposure to beam



# Tuners



## Original CEBAF tuner

- Mechanism in LHe.
- Fairly large hysteresis.
- Warm motor (external).
- Rotary feedthroughs
- 10+ years service in CEBAF/FEL

## Upgrade Scissor-type tuner

- Very Low hysteresis.
- Warm motor (external).
- Linear feedthrough (Bellows)
- In service in CEBAF/FEL

## Upgrade zero length tuner

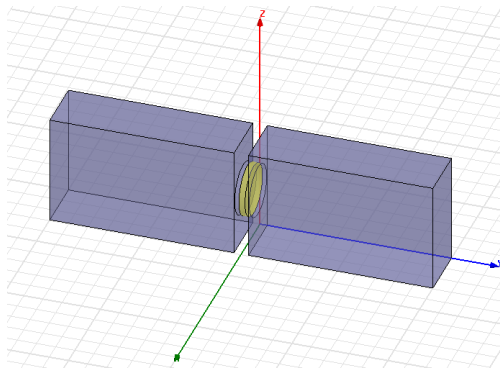
- Low hysteresis.
- Cold motor.
- Tested but not yet installed

## SNS-type tuner

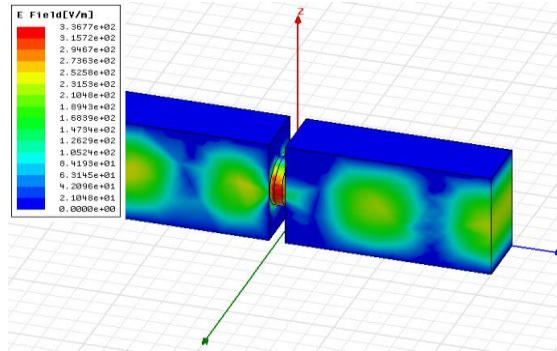
- End mount
- Low hysteresis.
- Cold motor.
- In service in SNS

- JLab has practical experience of several different types of tuners. All have Pros and cons.

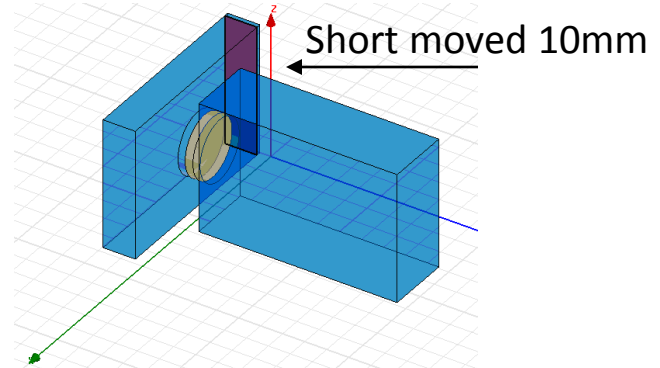
# Ceramic window Matching at 748.5 MHz



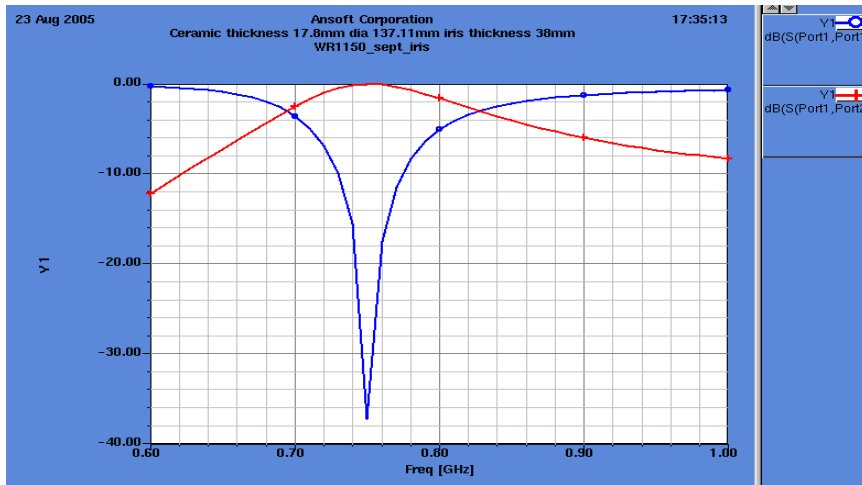
WR1150 ceramic matched in 38.1mm thick iris



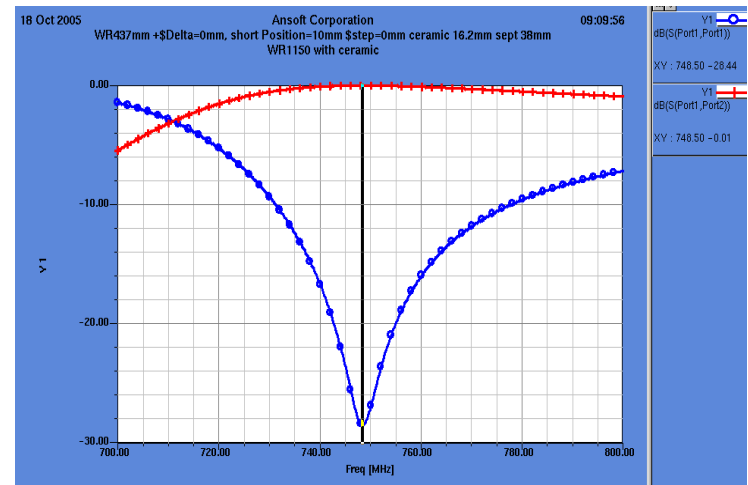
E fields at matching frequency



Ceramic window Matching on T model

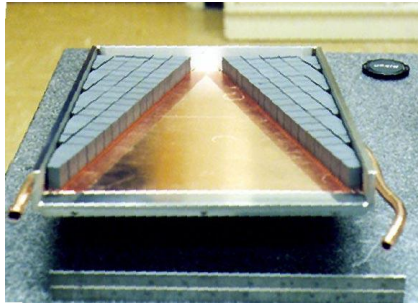


S11 at matching frequency. Ceramic thickness 0.7007in (17.8mm) at 748.5 MHz -37dB

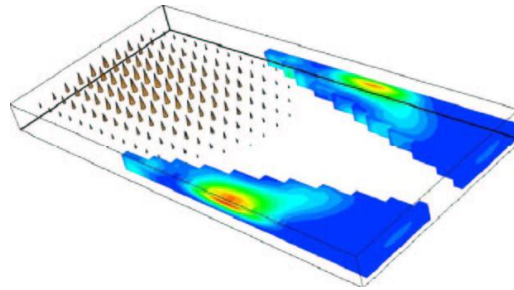


Matching in T model at 748.5 MHz was obtained by changing the iris height from 38.1mm to 50mm and position of the short with 10mm. S11 at matching frequency -28.5dB.

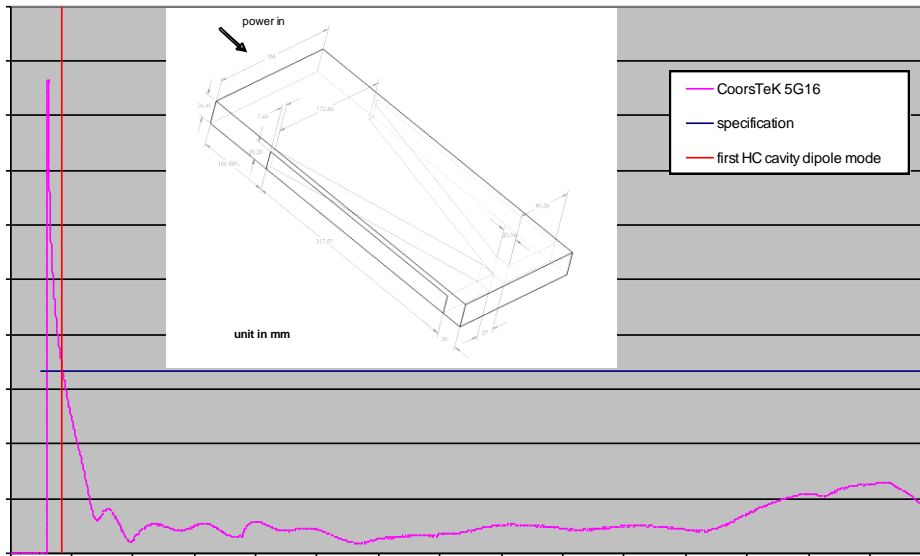
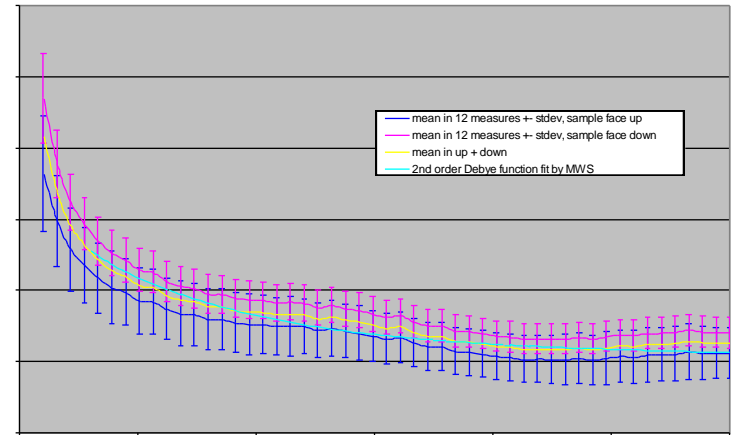
# HOM load match design by MAFIA/HFSS/ANSYS/MWS



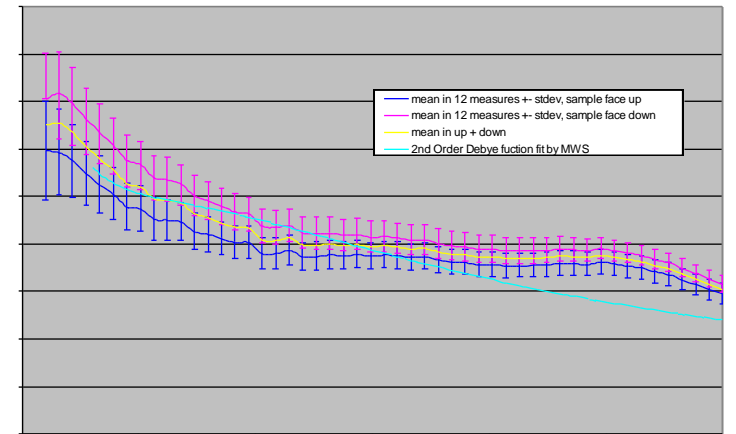
Original SLAC B-factory HOM load



MAFIA simulated electric field plot



More than 5 material vendors and >20 samples have been measured. Many are potentially usable.



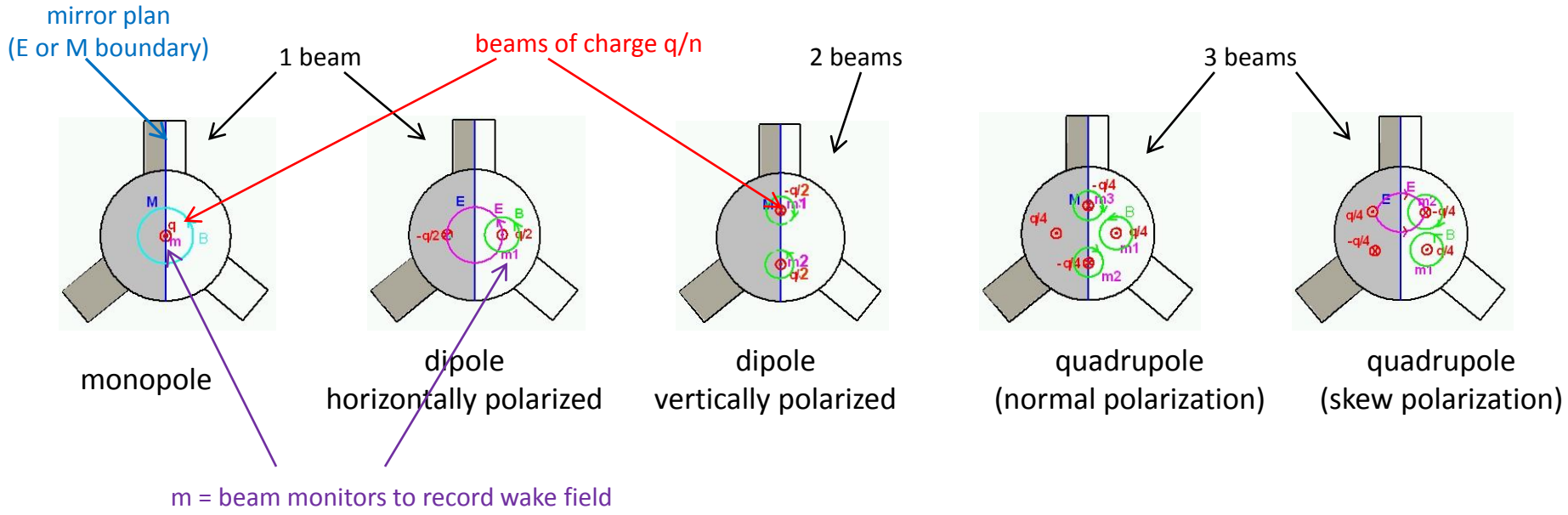


# JLAB HC Cryomodule Development

## Broadband HOM Damping Efficiency

- ❑ HOM damping efficiency is most important aspect of the HC cavity design
- ❑ Cavity broadband coupling impedance simulated using multi-beam excitation scheme
- ❑ Works with MAFIA T3 (does not work yet to our knowledge with CST Particle Studio or GdfidL)
- ❑ Benefit: We can distinguish between HOMs of different field nature and polarizations (monopole, dipole, quadrupole, sextupole,...)
- ❑ Valuable information for high current ERLs (other than dipole modes may become important)

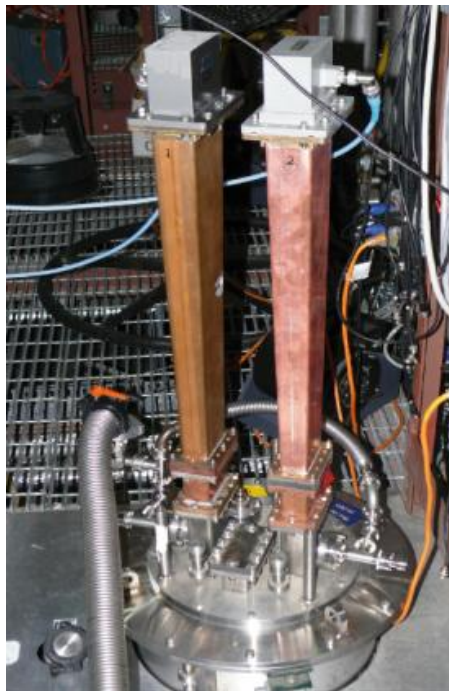
### Multi-Beam Excitation Scheme (MAFIA T3)



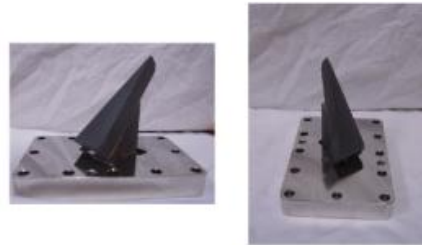
# JLAB HC Cryomodule Development

## HOM Load Material Studies

- ❑ VTA setup built for measurements from room temperature down to 2K
- ❑ Aim: Investigate various HOM material candidates
- ❑ Variability of material complex properties (batch to batch and lot to lot) may be important for large scale installation
- ❑ Further investigations planned on different materials



CEBAF 2K HOM absorber

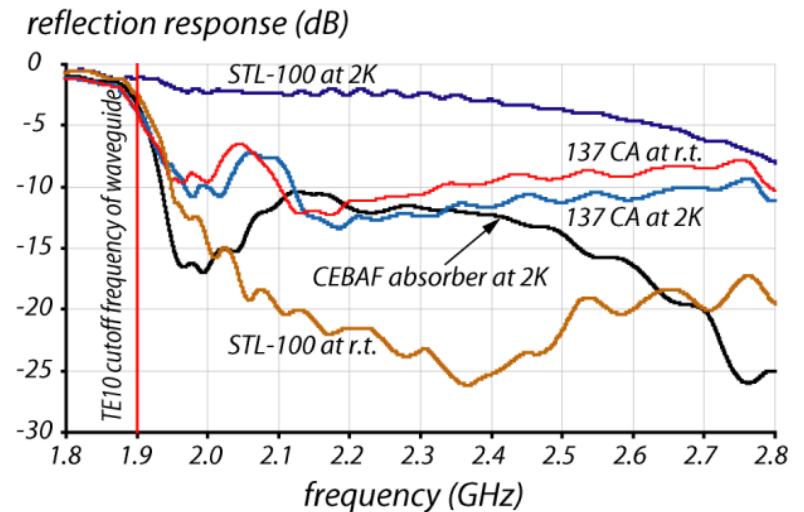


test absorbers



Test setup in the vertical Dewar (left), CEBAF absorber (top right) and two different wedge absorber assemblies (bottom right) made of ceramic AlN-based composites

Ceralloy 137 CA form Ceradyne, Inc.  
STL-100 from Sienna Technologies, Inc.



Reflection response of different AlN-based composites measured at room temperature (r.t.) and 2 K.