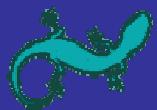


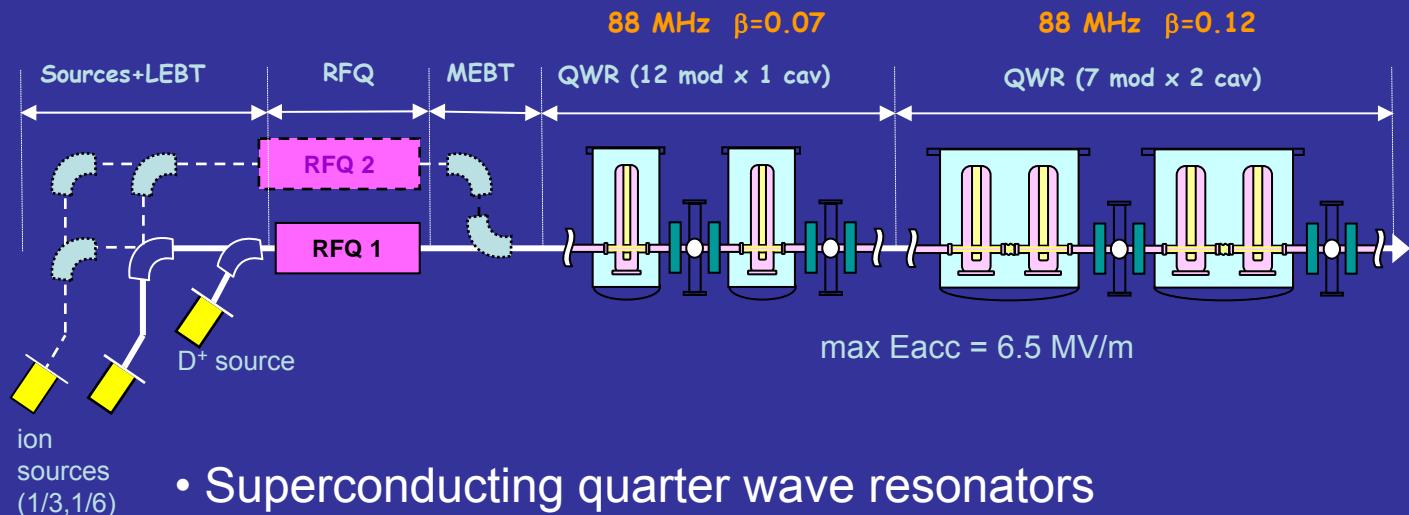
SPIRAL 2

RESONATORS





SPIRAL 2 Linac



- Superconducting quarter wave resonators
 - $\beta = 0.07$ 88MHz QWRs CEA/SACLAY
 - $\beta = 0.12$ 88MHz QWRs IPN/ORSAY
- options : warm quadrupoles instead of SC solenoids / short cryostats
- RF optimization , RF coupling
- mechanics / RF
- 4K tests
- cryomodule overview



Quarter-wave resonators ($\lambda/4$)

Requirements for SPIRAL 2 :

- ❖ bulk niobium technology
- ❖ 4K operation
- ❖ 88 MHz frequency
- ❖ minimum beam pipe diameter 30 mm
- ❖ separation of cavity vacuum and isolation vacuum
- ❖ RF losses < 7 W @ 6.5 MV/m
- ❖ specifications on maximum surface field:
 - Ep < 40 MV/m
 - Bp < 80 mT (at 8 MV/m)
- ❖ accelerating field definition adopted for the project

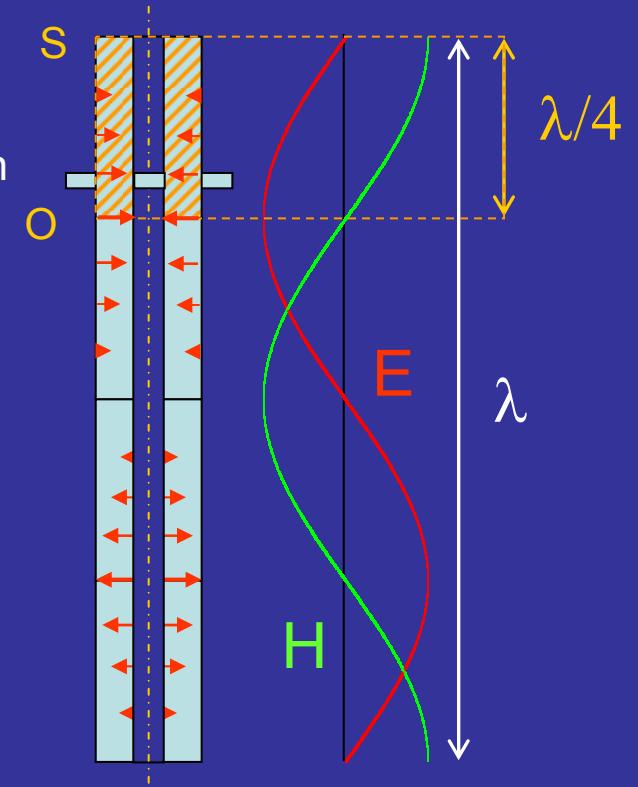
$$E_{acc} = \frac{V_{acc}}{\beta \lambda}$$



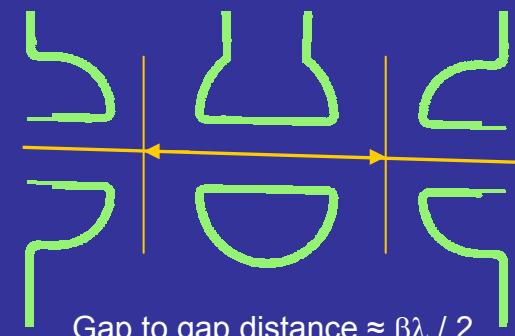
Quarter-wave resonators ($\lambda/4$) optimization

Cavity RF design:

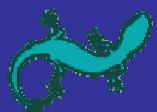
- ❖ basic starting geometry : coaxial guide of length $\approx \lambda/4$ of the TEM mode
 - one Open end (electric region),
 - one Short-circuit (magnetic region)
- transverse electric field : the beam has to travel across the cavity on a radial path, through the stem → 2 accelerating gaps
- ❖ optimal β mainly dependant on the distance between gap centers: β_{opt} varies with cavity diameter and drift tube lengths



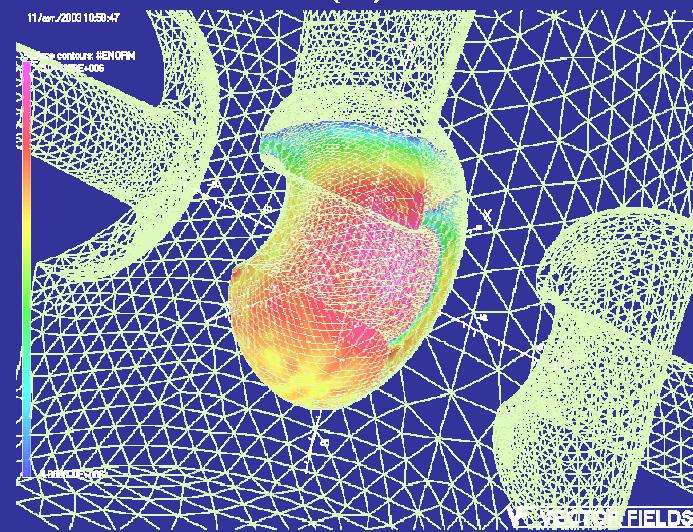
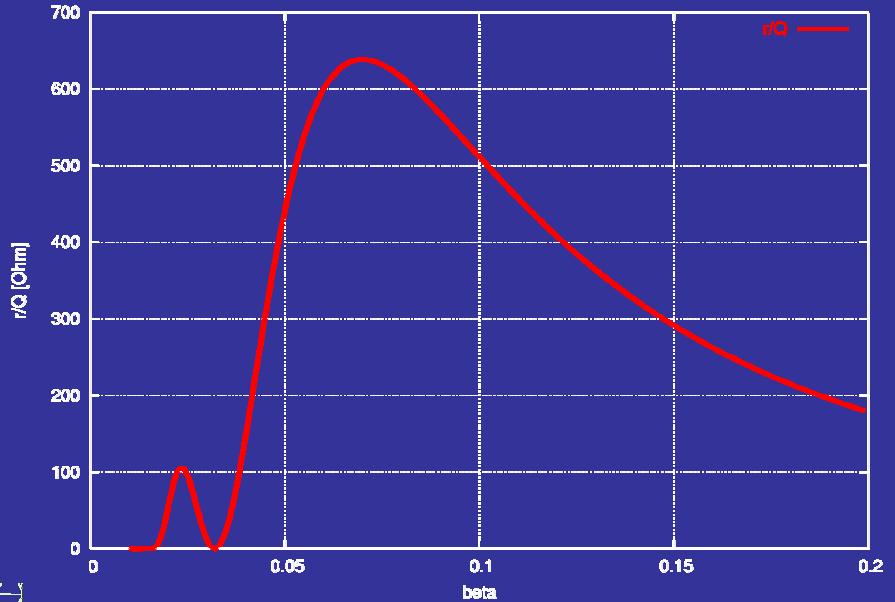
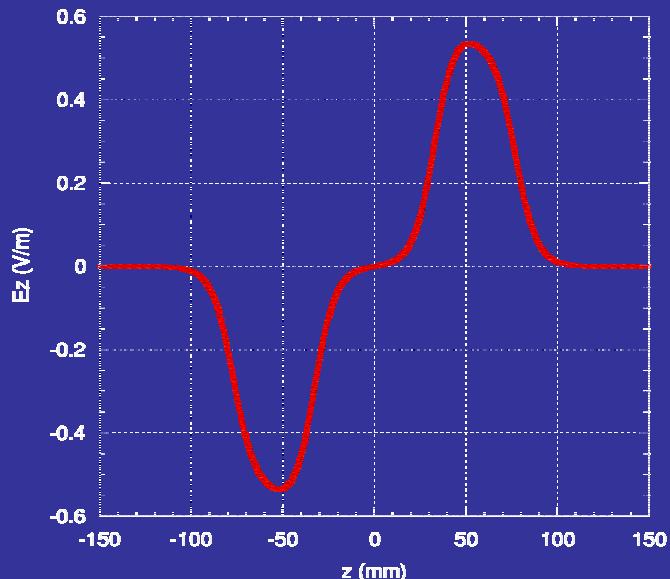
- ❖ The main objectives of the design were
 - to achieve high accelerating voltages
 - to reduce E_p/E_{acc} and B_p/E_{acc}
 - to ease chemistry and HPR



Gap to gap distance $\approx \beta\lambda / 2$



$\beta = 0.07$ cavity RF parameters

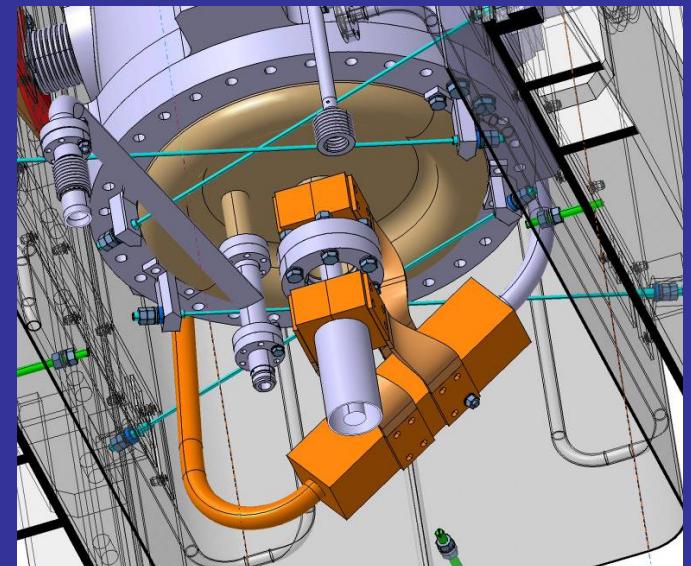
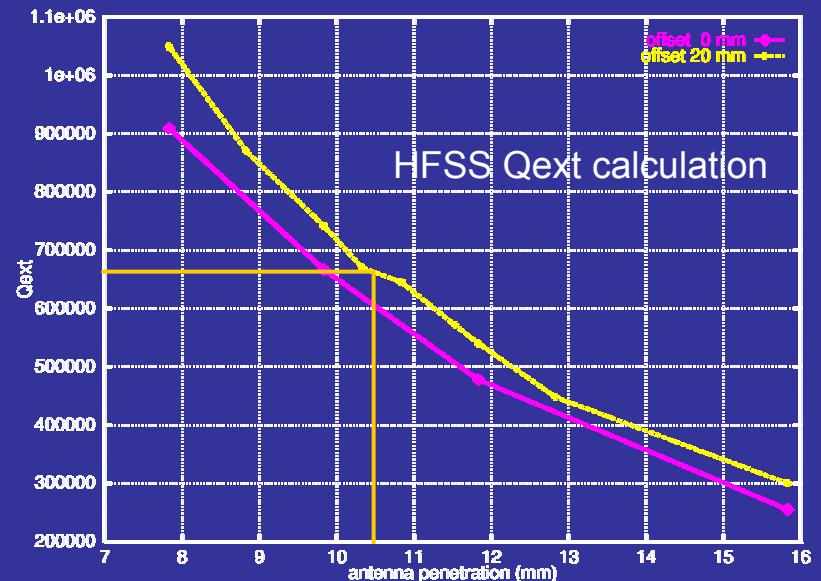
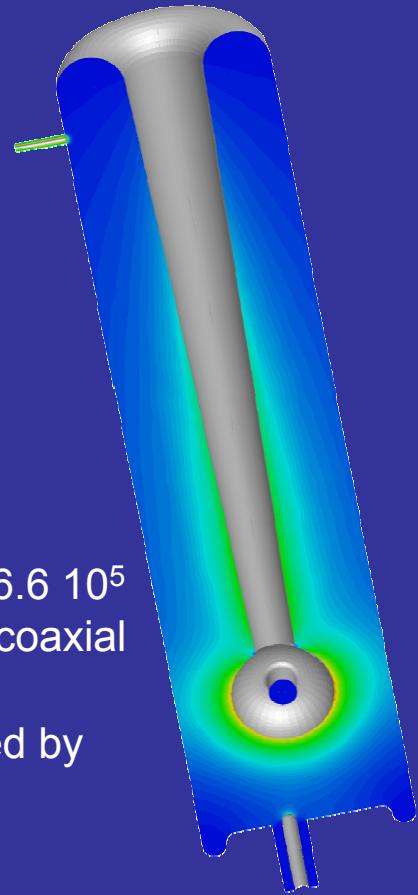


Frequency (MHz)	88
Optimal β	0.07
r/Q (Ω) @ optimal β	632
E_p/E_{acc}	5.0
B_p/E_{acc} (mT/MV/m)	8.75
Q_0 @ $R_s = 10$ nOhms	$2.2 \cdot 10^9$



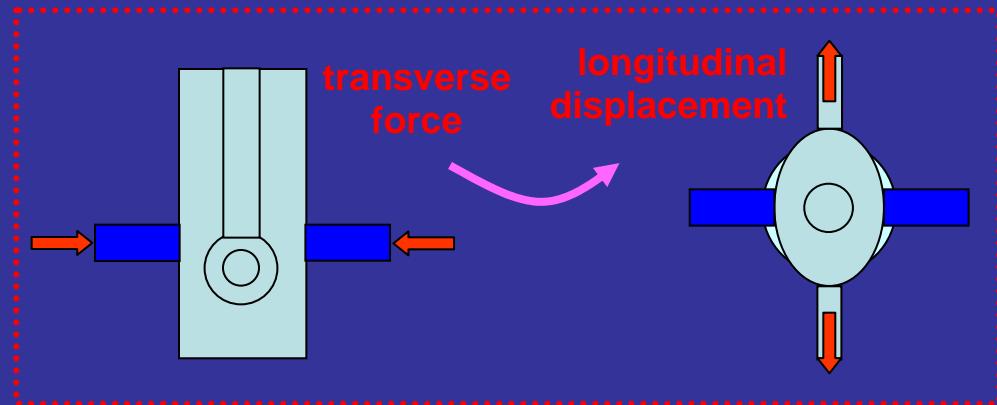
$\beta = 0.07$ cavity RF coupling

- ❖ nominal Qext= $6.6 \cdot 10^5$
 - ❖ Ø 36 mm 50Ω coaxial line
 - ❖ coupler designed by LPSC Grenoble
-
- ❖ antenna in a low H area
 - ❖ no extra opening in He tank





$\beta = 0.07$ cavity tuning

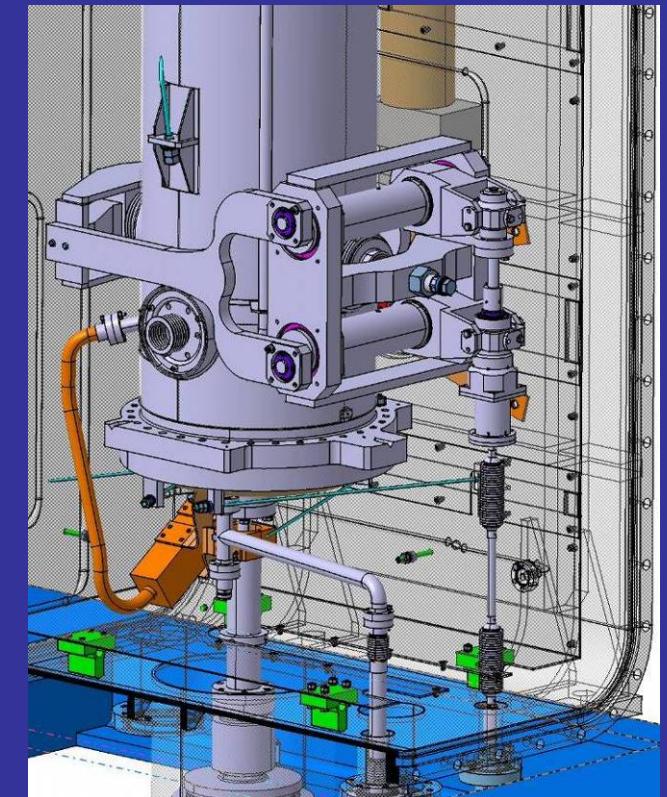


- ❖ transverse CTS
- ❖ saves longitudinal space
- ❖ low stress on drift tube welds
- ❖ computed tuning range ± 24 kHz at 4 K

Mesh for mechanical/RF coupled calculations
CASTEM + i-DEAS + SOPRANO



SPIRAL2 resonators



SRF05 G. Devanz – 07/11/05



$\beta = 0.07$ cavity frequency stability

He bath pressure variations

Expected $\Delta P \sim 10$ mbar

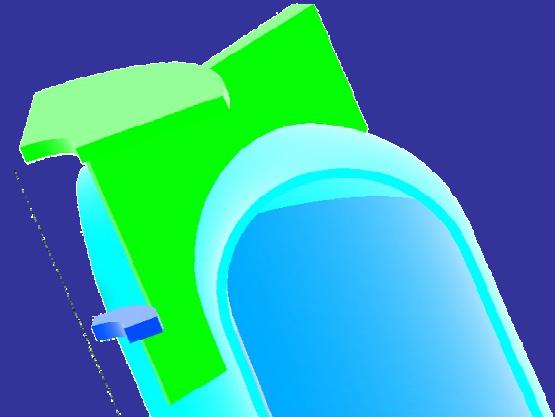
cavity BW = 132 Hz :

$$\Delta f_{\text{pressure}} < \text{BW}/10 \quad |\Delta f/\Delta P| = 1 \text{ Hz/mbar}$$

80 % of $\Delta f_{\text{pressure}}$ due to vertical stem displacement

With 4 mm thickness $\Delta f/\Delta P = -2.5 \text{ Hz/mbar}$

adding a stiffener $\Delta f/\Delta P = -1 \text{ Hz/mbar}$



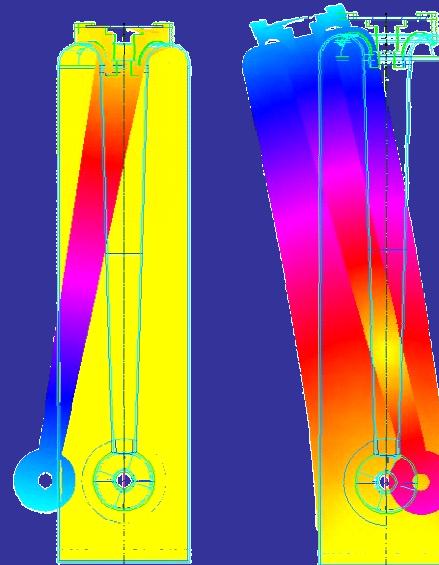
Mechanical modes

Mode 1 @ 43 Hz with
stiffener

High sensitivity :

Transverse : 500 kHz/mm

Longitudinal : 650 kHz/mm



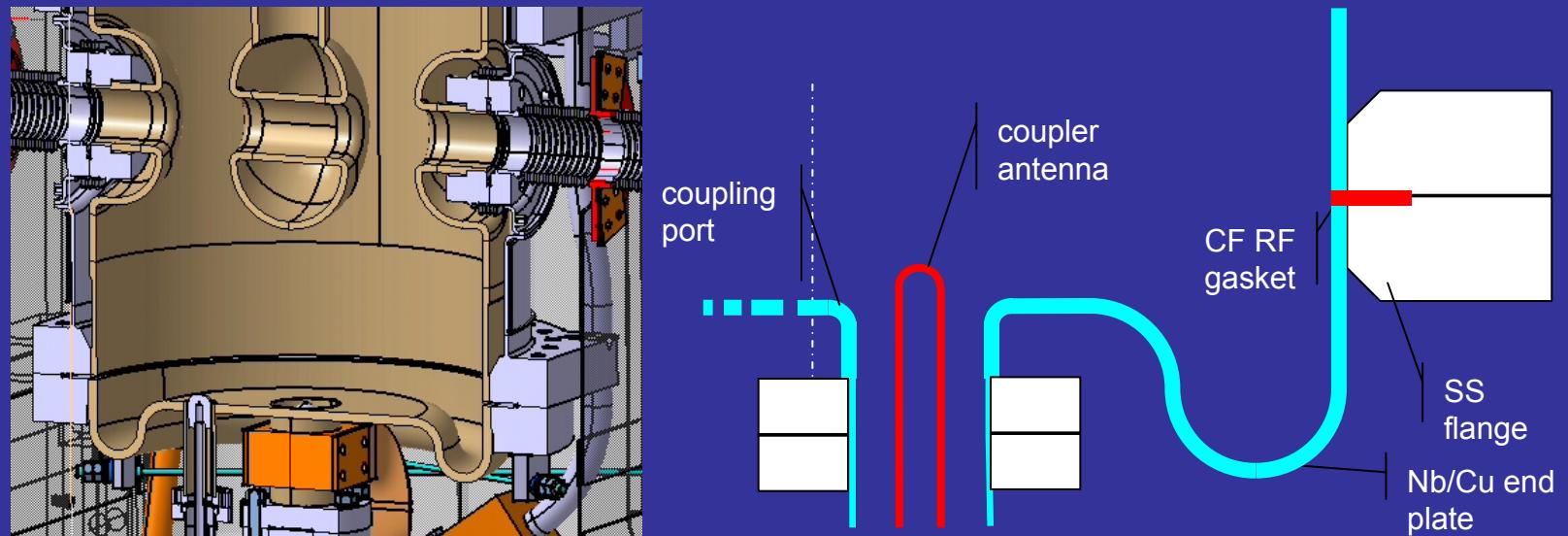
Mode 2 @ 126 Hz with
stiffener

If needed, room is provided to include a Legnaro type damper



$\beta = 0.07$ cavity bottom plate

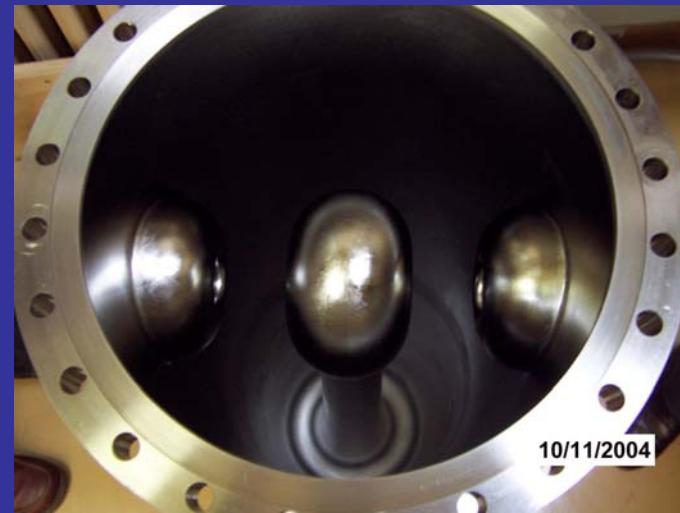
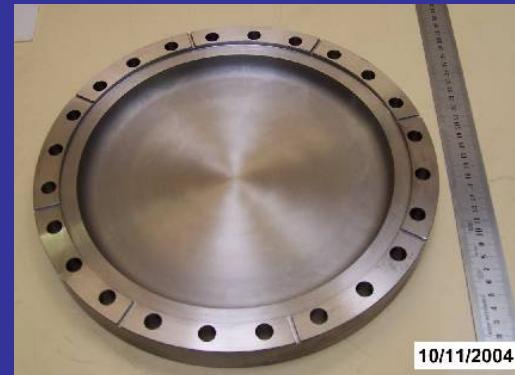
- ❖ Large opening for High Pressure Rinsing
- ❖ Nb sputtered copper plate
- ❖ H field very low in the cavity low end region : the plate can be cooled by conduction due to high thermal conductivity of copper
- ❖ Stainless steel He vessel -> 316LN flange brazed on the cavity
- ❖ Copper RF gasket position should be as low as possible
- ❖ S-shape :
 - ❖ mechanical compliance (differential shrinkage)
 - ❖ reduced coupler antenna penetration for required Q_{ext}
 - ❖ passes pressure qualification tests at 2.5 bars (vertical cryostat test)





$\beta = 0.07$ cavity Prototype cavity

- ❖ Manufactured by ACCEL
- ❖ Differs from the final cavity :
 - NbTi end-plate and flange
 - vacuum tightness : copper ring + indium seal
 - 3 mm Niobium





Cavity preparation at Saclay

Chemical polishing

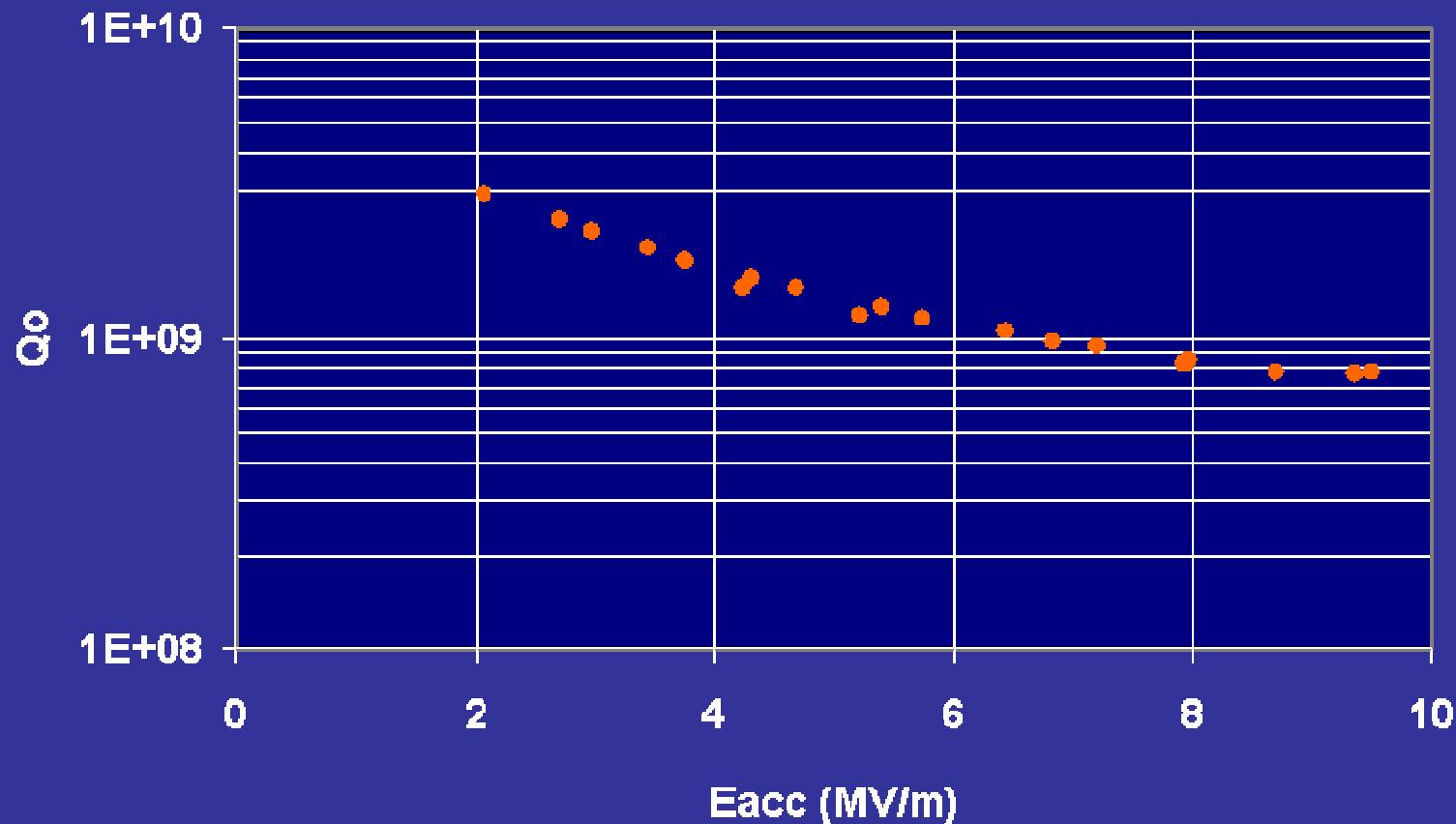


High pressure rinsing





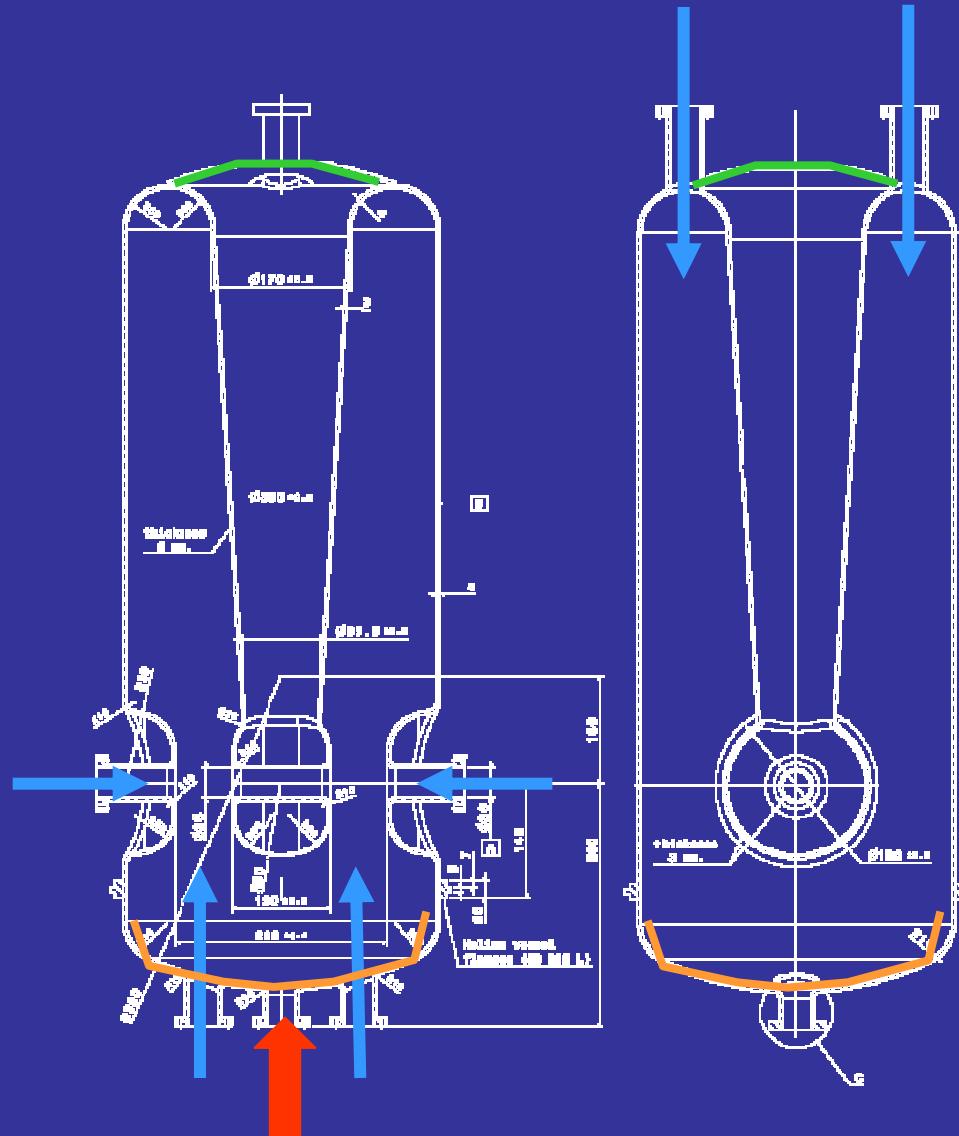
$\beta = 0.07$ cavity vertical cryostat test



- ❖ Limited by partial quench at 9.5 MV/m
- ❖ Tests at 4.2 K and 1.8 K with same overall behavior. Extra test done in June with a SC Nb/Cu gasket with the same behavior at high field
- ❖ Quench attributed to thermal runaway in NbTi bottom plate ($\lambda_{NbTi} \approx 0.3$ W/m.K + defect ?). The stem region is not thermally affected
- ❖ $Q_0 = 10^9$ @ 6.5 MV/m $P_{wall} = 3.8$ W < Maximum specified losses of 7 W



$\beta = 0.12$ QWR Mechanical Design

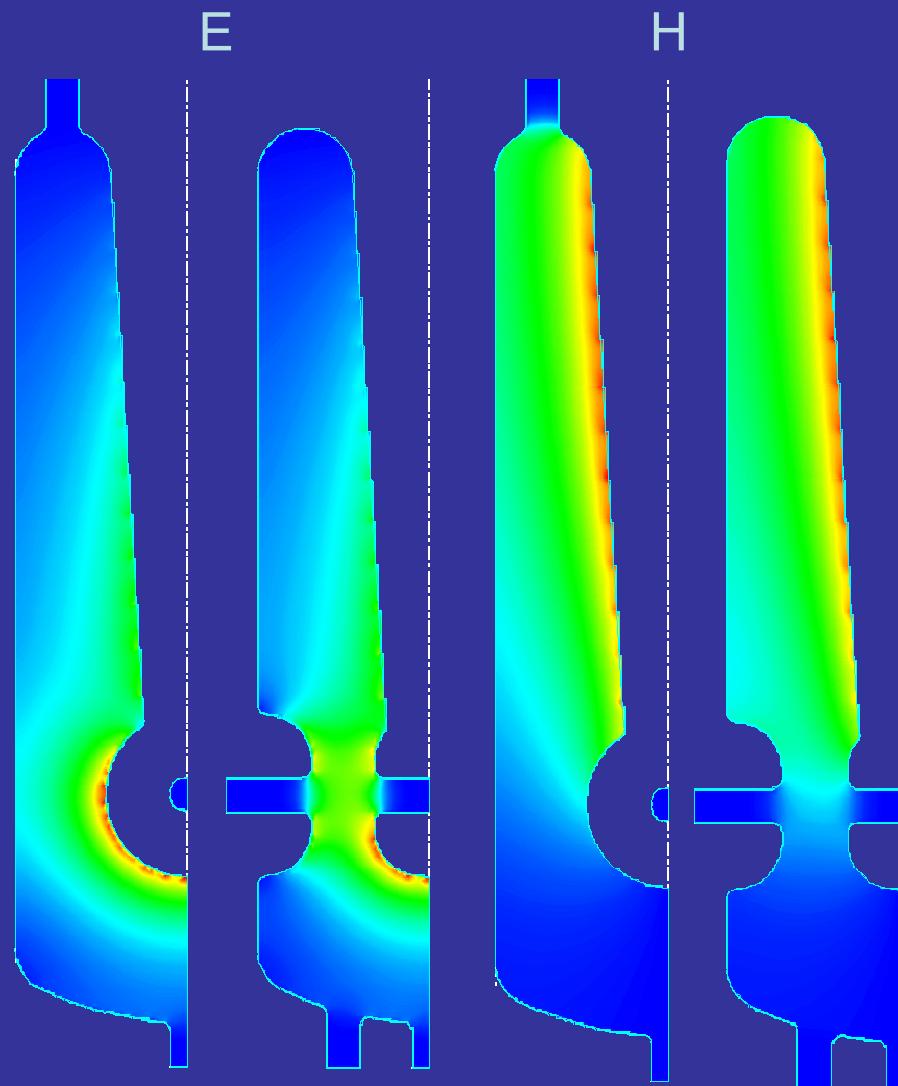


SPIRAL2 resonators

- ❖ Welded bottom plate
- ❖ Nb thickness: 4 mm (except the stem: 3 mm)
- ❖ Beam tubes aperture: Ø36 mm
- ❖ RF coupling by Ø36 mm port
- ❖ Stiffening plate on top-torus
- ❖ 6 ports for HPR
- ❖ Ø418 mm SS flange brazed on cavity bottom allows to weld the He tank



$\beta = 0.12$ cavity RF parameters

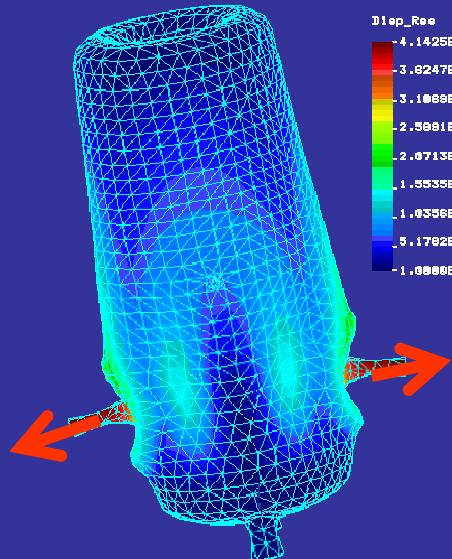


Frequency (MHz)	88
Optimal β	0.12
$r/Q (\Omega)$ @ optimal β	518
E_p/E_{acc}	5.6
B_p/E_{acc} (mT/MV/m)	10.2
Q_0 @ $R_s = 12.5$ nOhms	$3.0 \cdot 10^9$

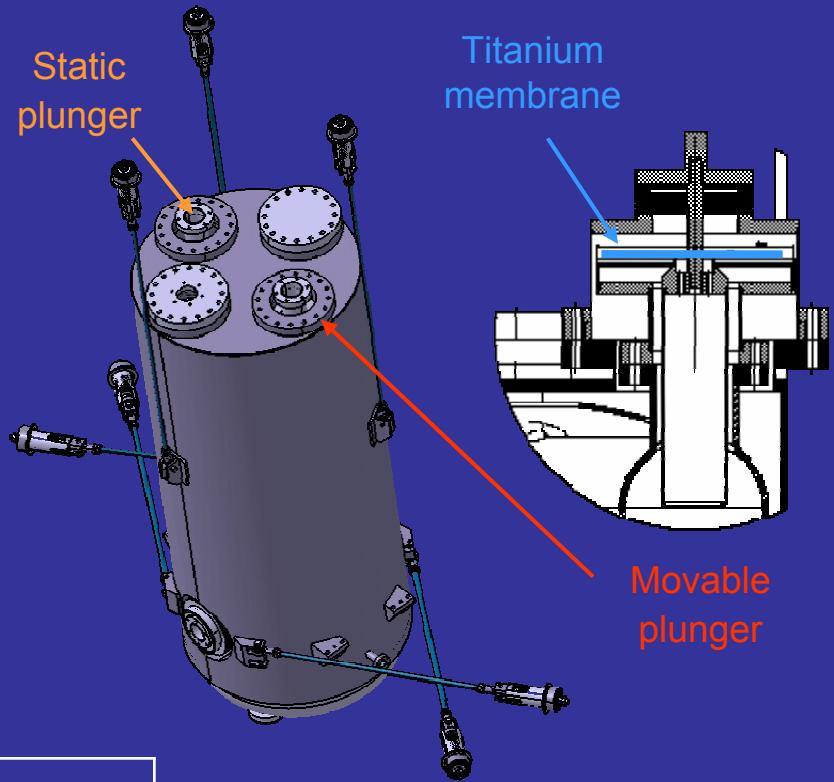


$\beta = 0.12$ cavity tuning

2 systems are studied



Tuning by pulling the beam tubes



COSMOS & MICAV calculations	
Maximum stress for 1 bar [MPa]	< 36
Stiffness [kN/mm]	16
Tuning sens. using beam tubes [kHz/mm]	31
Tuning sens. using one Ø30 plunger [kHz/mm]	1.2

Tuning using SC plungers



$\beta = 0.12$ prototype

- ❖ Manufactured by Zanon
- ❖ Includes the stainless steel flange needed to attach the He tank

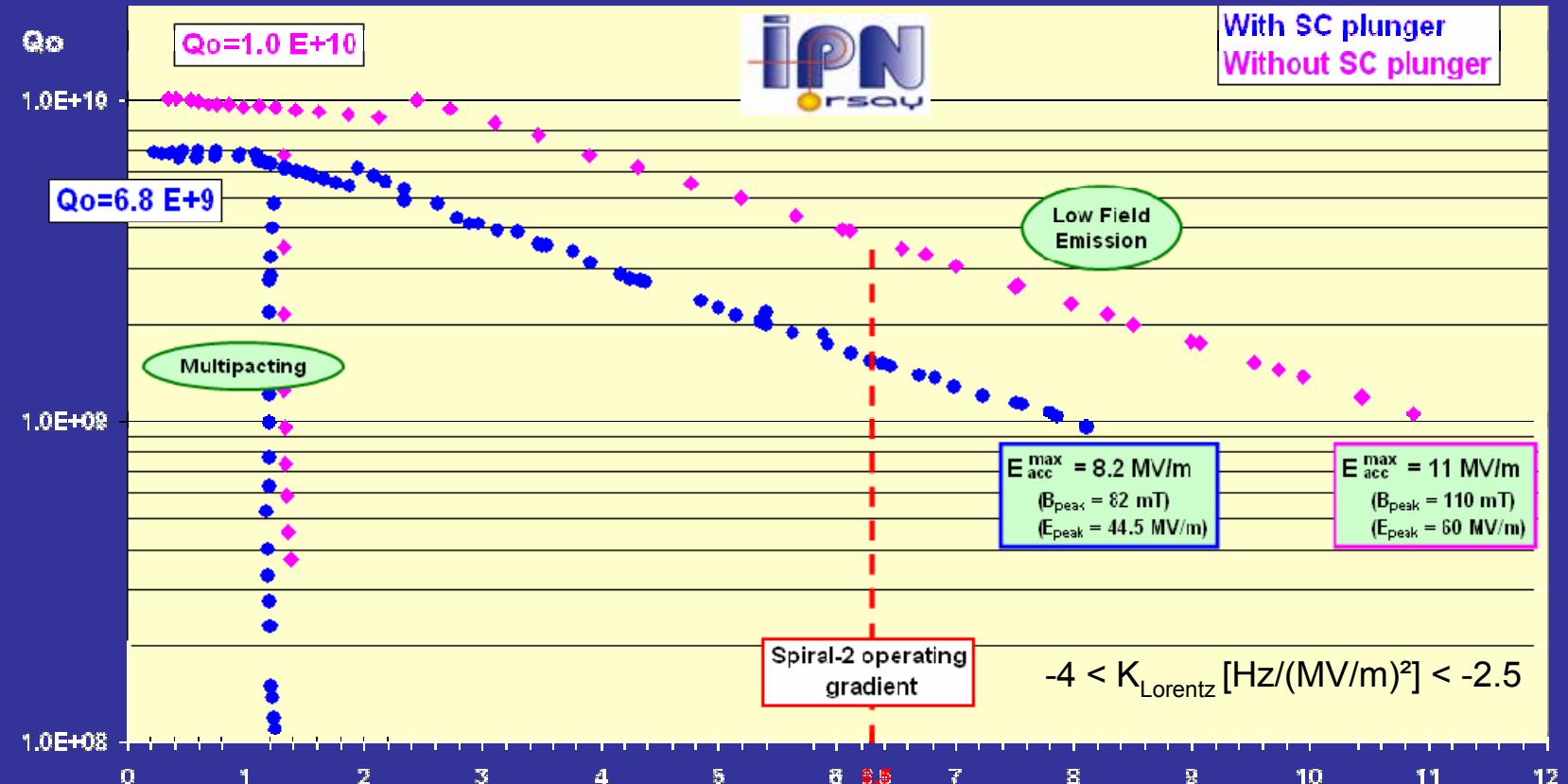


Stiffening
on top torus





$\beta = 0.12$ Vertical cryostat test

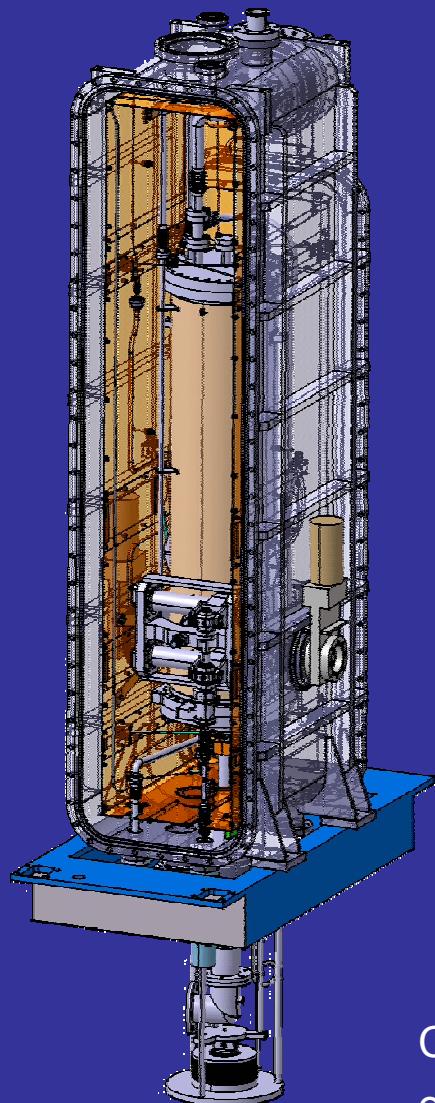


- ❖ Limited by power source at 11 MV/m.
- ❖ Limited by quench with SC plunger ($\Delta f \approx 65 \text{ kHz}$)
- ❖ $Q_0 = 1.5 \times 10^9$ @ 6.5 MV/m $P_{\text{wall}} = 4 \text{ W} <$ Maximum specified losses of 10 W

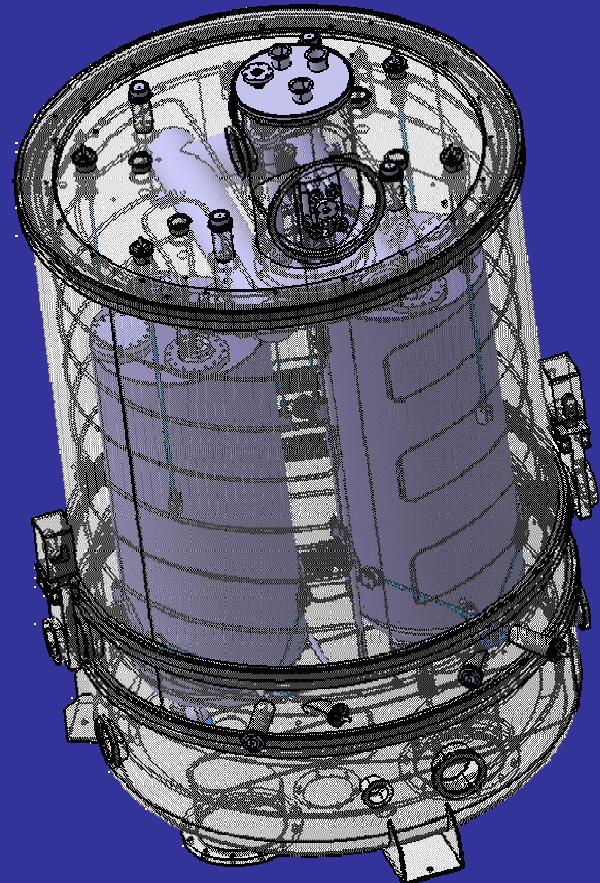


Cryostats overview

High β



Low β



Construction of a fully equipped cryostat for each β starting in 2005