



Shaping Electrostatic Conditions in the Stalk of the ERL -750 kV Electron Gun

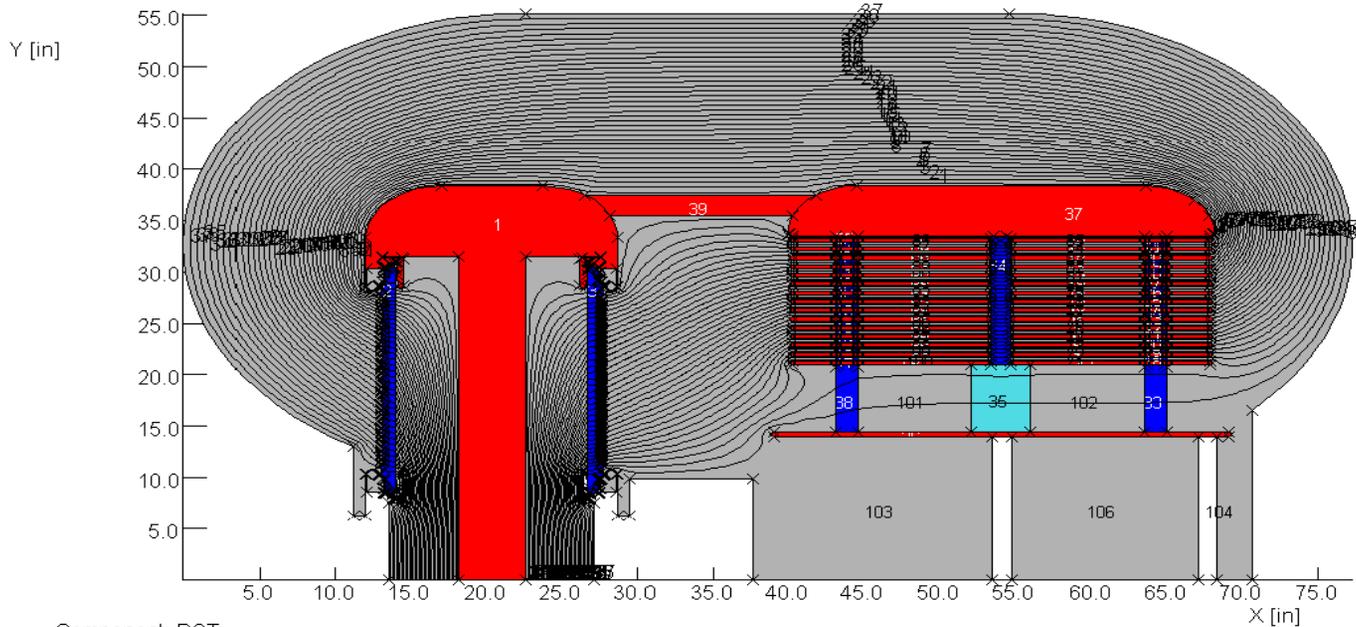
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Advisors: Karl Smolenski and Bruce Dunham

Cornell University

Laboratory for Elementary-Particle Physics



UNITS	
Length	: in
Flux density	: C m ⁻²
Field strength	: V m ⁻¹
Potential	: V
Conductivity	: S m ⁻¹
Source density	: microC m ⁻³
Power	: W
Force	: N
Energy	: J
Mass	: kg

PROBLEM DATA	
C:\Documents and Settings\dstone\Opera Models\gunTanv5.st	
Linear elements	
XY symmetry	
Scalar potential	
Electric fields	
Static solution	
Scale factor: 1.0	
23058 elements	
11737 nodes	
106 regions	

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- -750 kV power supply (left), electron gun (right)
- SF₆ tank ($\epsilon_r \approx 3$) surrounding power supply and gun (held at ground), about 1.4 m tall
- Highest fields at corona rings protecting triple junctions inside ceramic
- Equipotentials unevenly distributed throughout apparatus

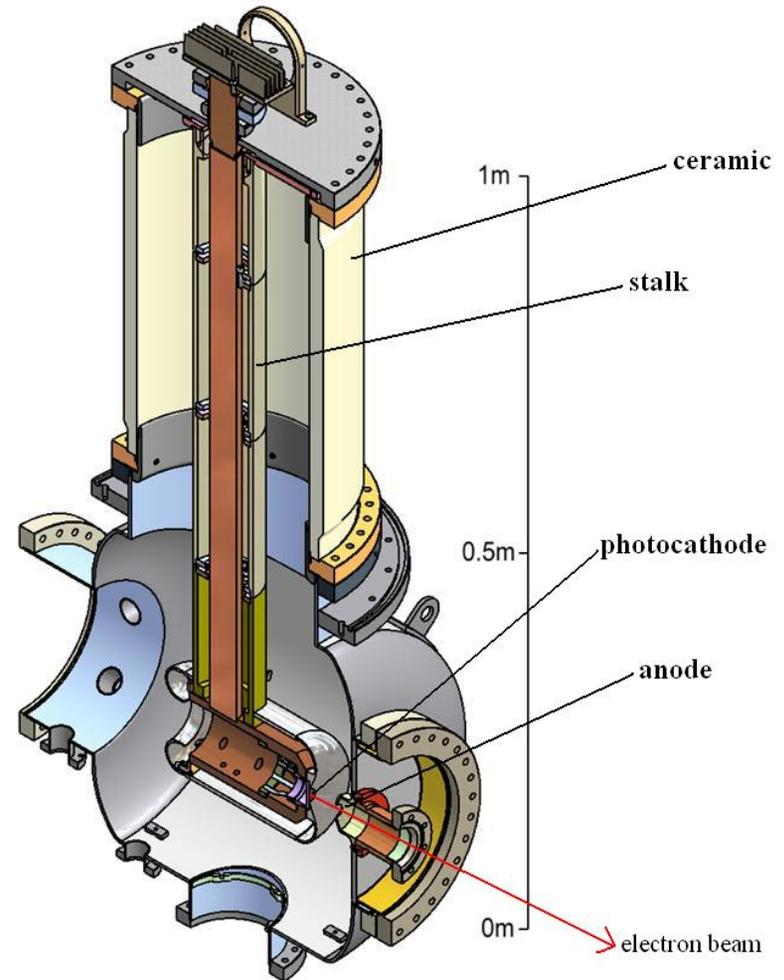


- **Electron gun:**

- Photocathode, pulsed laser, stalk, ceramic under vacuum
- Cathode at -750 kV w.r.t. anode/electrode chamber
- 2 ps laser pulses centered on photocathode (GaAs), produce beam to be powered to 100 MeV with 100 mA current
- Ceramic (alumina, $\epsilon_r \approx 10$) a single corrugated cylinder

- **Cathode Voltage**

- Cathode must use conditioning, HPR, electrochemical polishing, etc. to decrease imperfections



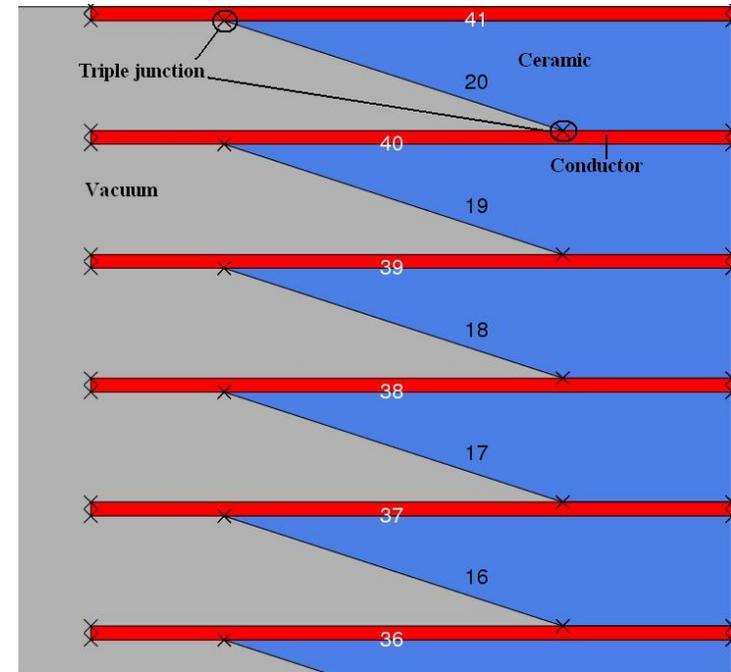


- **Ultra-High Vacuum (UHV)**

- Maintained to prevent voltage breakdown- desorbed or leftover gas can initiate breakdown
- In gun, $p \approx 10^{-11}$ torr to prevent decay of QE in photocathode

- **High Voltage (HV)**

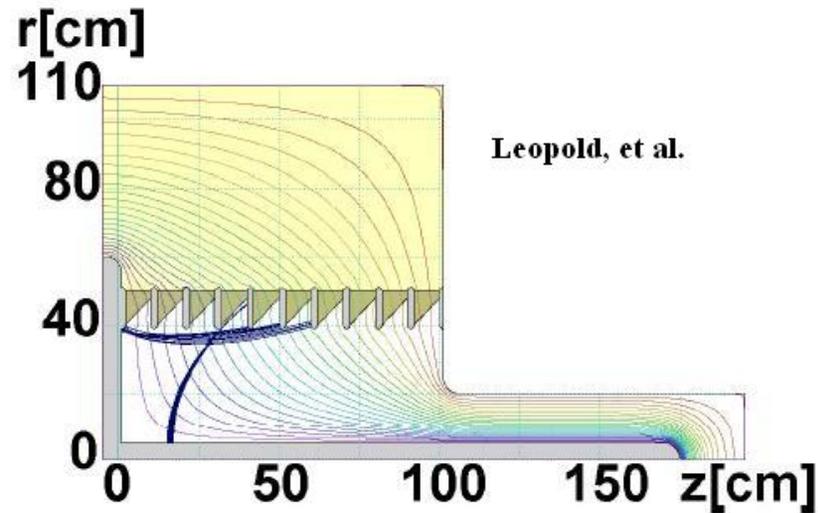
- Breakdown occurs in most gaps w/ excess field strength > 20 MV/m
- Initiated by microprotrusions and other e^- emission sites, strong fields at triple junctions, desorbed gas, small gap separations, etc. (excessive surface area exacerbates these problems)
- Once initiated, if electron current impacts ceramic, secondary emission and electron avalanches can occur, irreversibly destroying ceramic



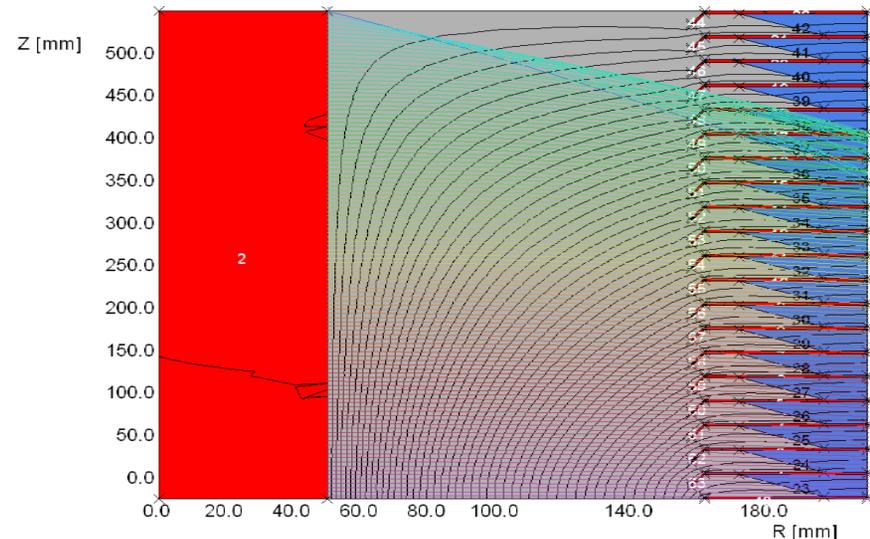


• Ceramic Design

- Stacked/graded insulator design (J.G. Leopold, et al.)
 - No noticeable variation in field with variation in ceramic angle
 - Insignificant shaping of field with conductor rings separated by linear potential steps
 - Conductor rings suggested by others (Sinclair, Haimson, etc.) used to protect ceramic from electron impacts



45 Degree Stacked Ceramic with Conductor Protrusion: Potential and Electron Tracks

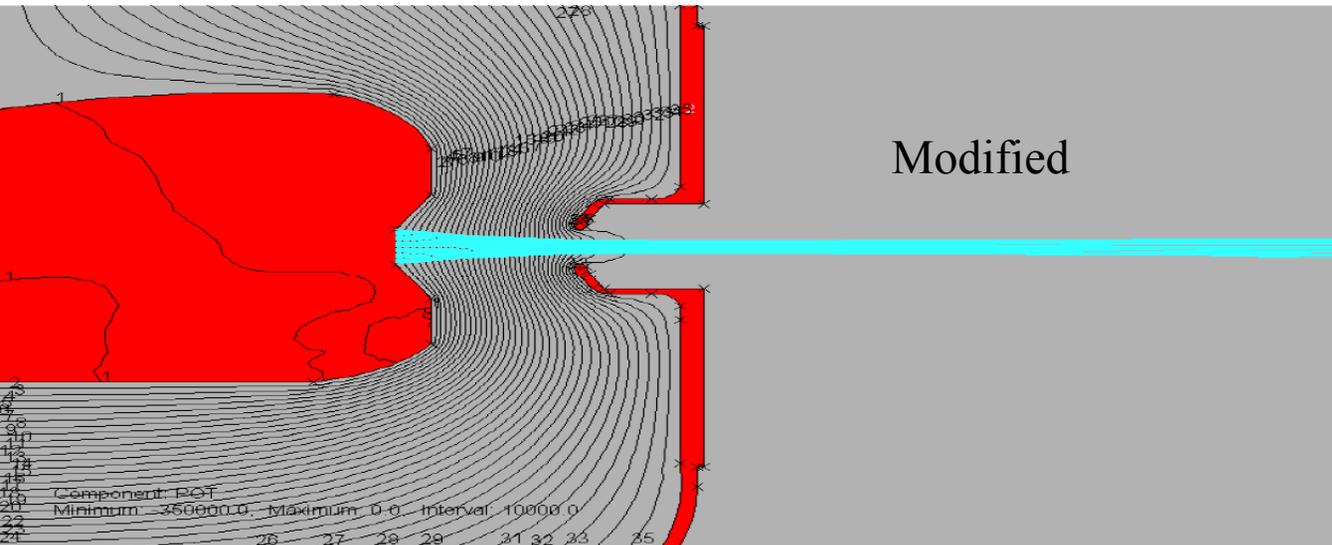
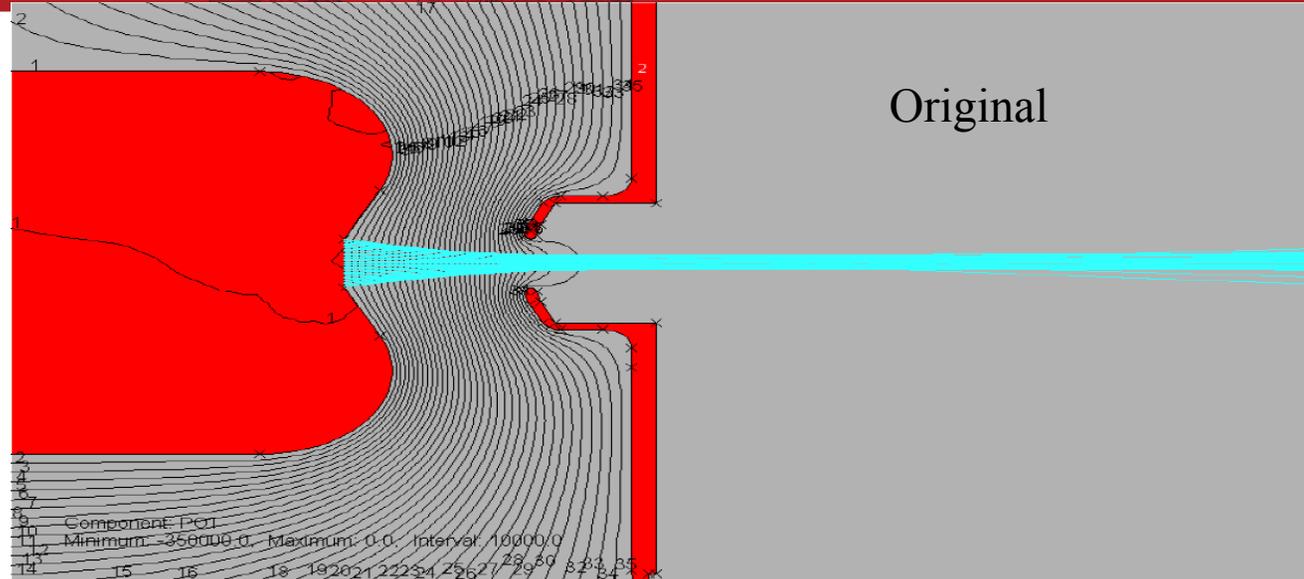


UNITS	
Length	mm
Flux density	C m ⁻²
Field strength	V mm ⁻¹
Potential	V
Conductivity	S mm ⁻¹
Source density	C cm ⁻³
Power	W
Force	N
Energy	J
Mass	kg

PROBLEM DATA	
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Linear elements	
Axi-symmetry	
Scalar potential	
Electric fields	
Static solution	
Scale factor	1.0
36149 elements	
18230 nodes	
63 regions	



- Surface area reduction
 - Reduced curvature of Pierce Electrodes surrounding photocathode

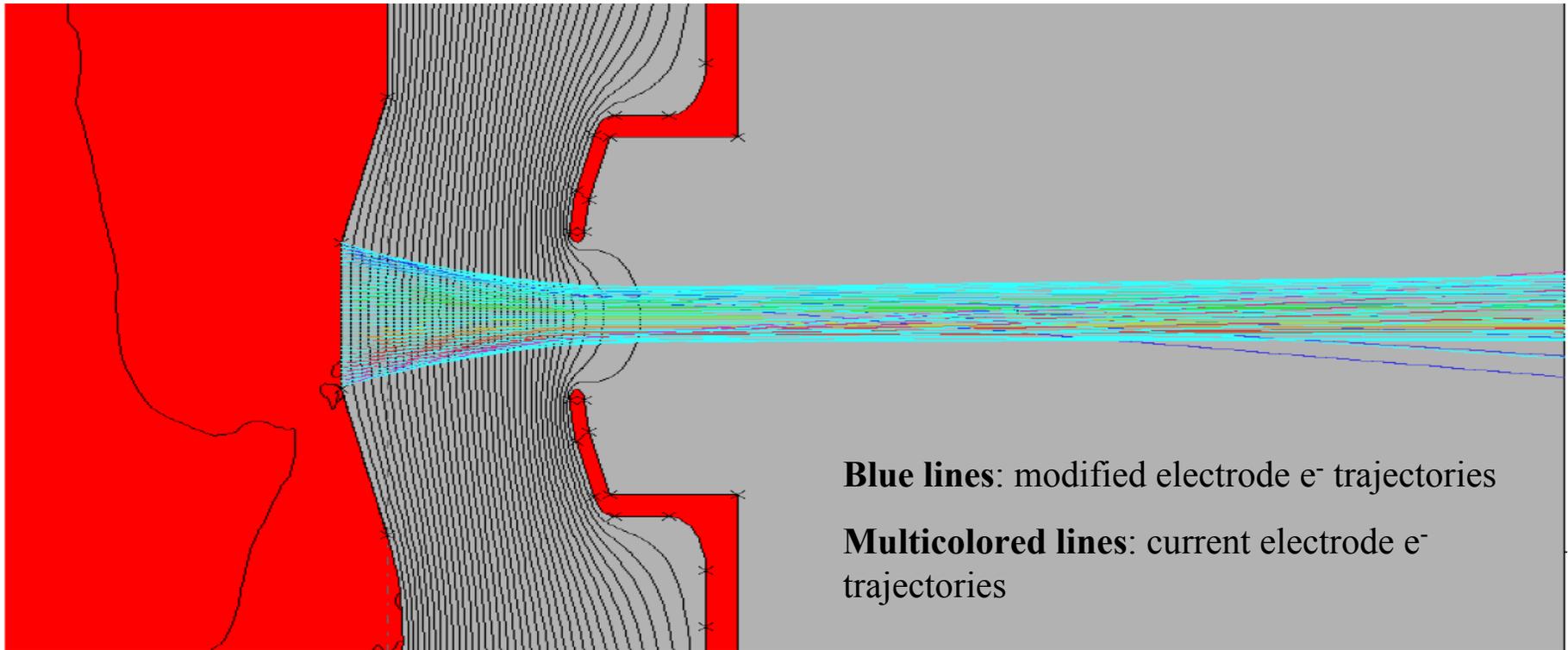


- Curvature reduction
 - Decreases local field enhancements



- **Minor improvements in modified design**

- No quantitative measurements able to be taken
- Less aberrations in beam path, a more uniform e^- distribution, but wider beam
- Space charge analysis not used





- **Magnetic Fields**

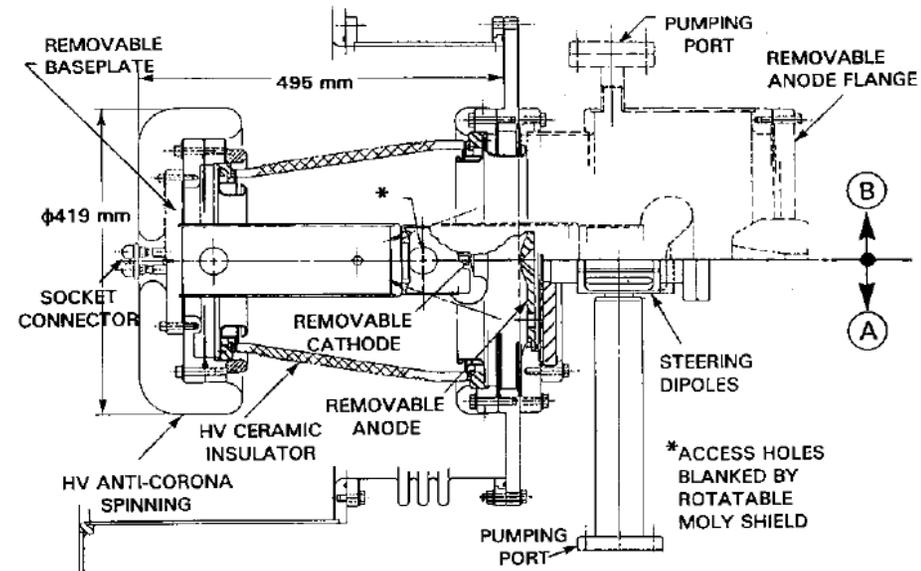
- Use magnetic fields to deflect particles downward (ϕ -directed field) or in a spiral towards ground (z -directed field)
- For z -directed field (solenoid field, helical e^- trajectory):

$$B = \frac{mv}{qr}$$

- $m=m_e$, $v \approx .9c$, $q= -e$, $r = .16$ m
- $|B| \approx 10$ - 100 gauss
 - 4,000 to 50,000 wire turns around ceramic

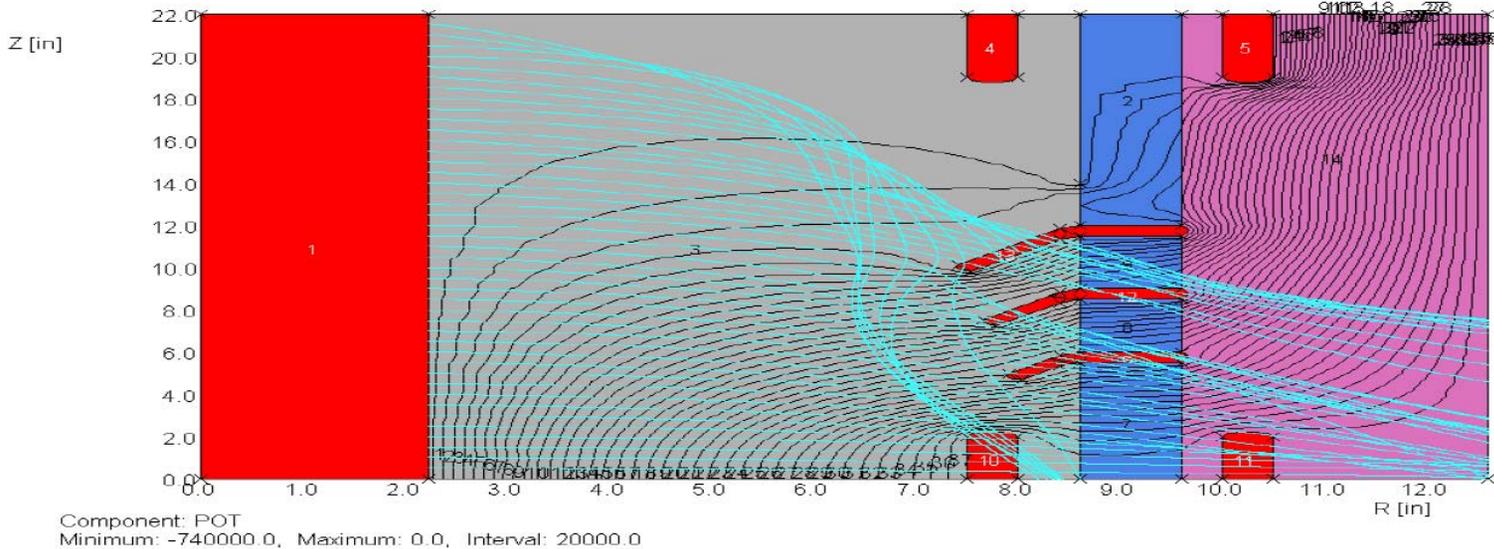


- Non linear potential steps and conductor ring separation
 - Discussions with Jacob Haimson (Haimson Research Corporation) and MIT PSFC
 - Two approaches to new design
 - Field curving design- use **E** field to entirely deflect e- towards chamber flange (ground)
 - Uniform field design- use uniform **E** field to evenly distribute e- over conductor rings protecting ceramic



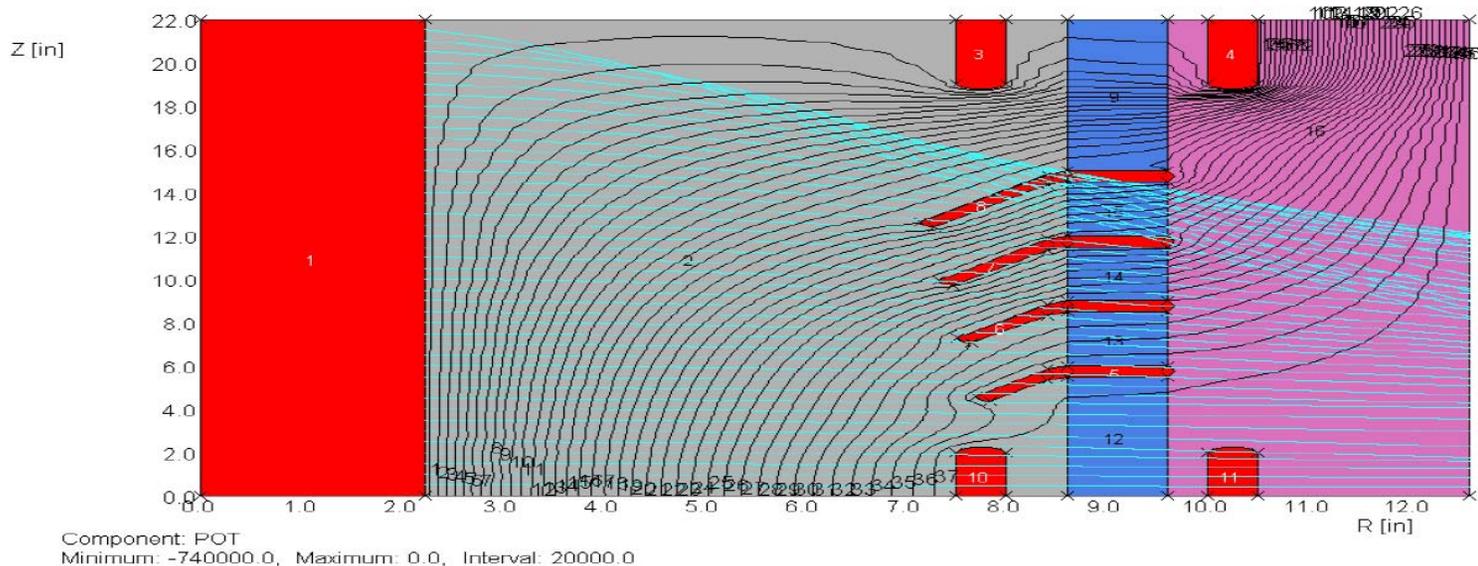


Refocus on Stacked Ceramic Design



- Field curving design

- Uniform field design
 - Note consecutive conductor rings are shorter to prevent secondary emission



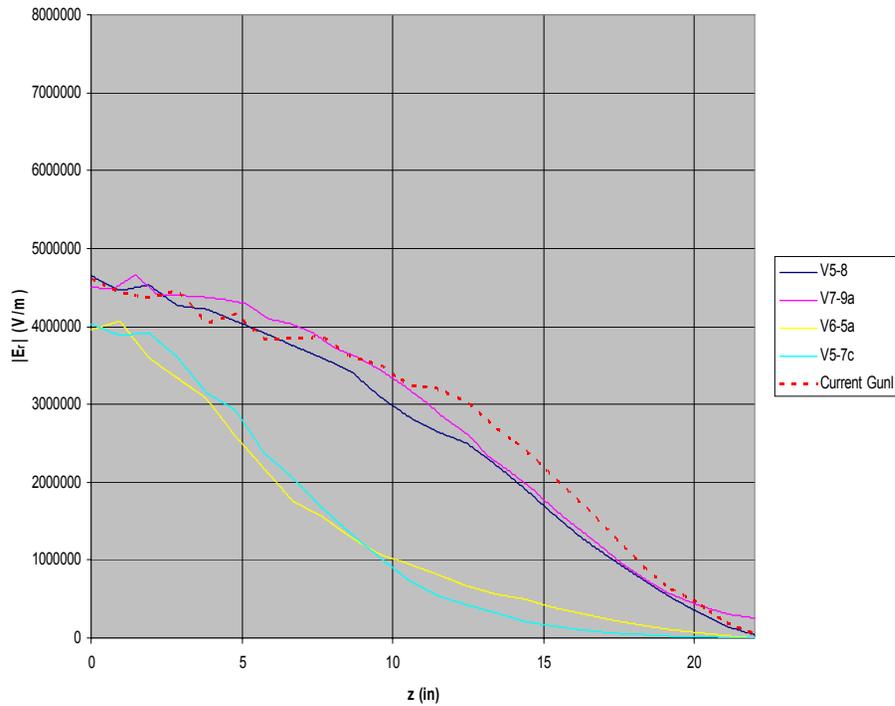


- **Most efficient configuration determined by:**
 - The value of $|E_{\perp}|$ or $|E_r|$, the magnitude of the perpendicular electric field component at the surface of the stalk. A greater perpendicular field component reduces the work function, ϕ , of a metal and increases field emission.
 - The value of ρ_e ($.5\epsilon_0 E^2$), the electric field energy density in the stalk-ceramic configuration. A constant or symmetric distribution of energy density throughout the area of concern is desirable to reduce field enhancements.
 - The value of $|E_{\max}|$, the magnitude of the maximum electric field strength at key locations in the configuration. High voltage breakdown, depending on the conditions, occurs around 20 MV/m in Cornell's gun case. It is attempted to keep maximum fields strengths below 12 MV/m in the models.
 - The engineering and machining feasibility of the geometry of the configuration. Limitations such as brazing effectiveness and metal machinability will constrain the models.

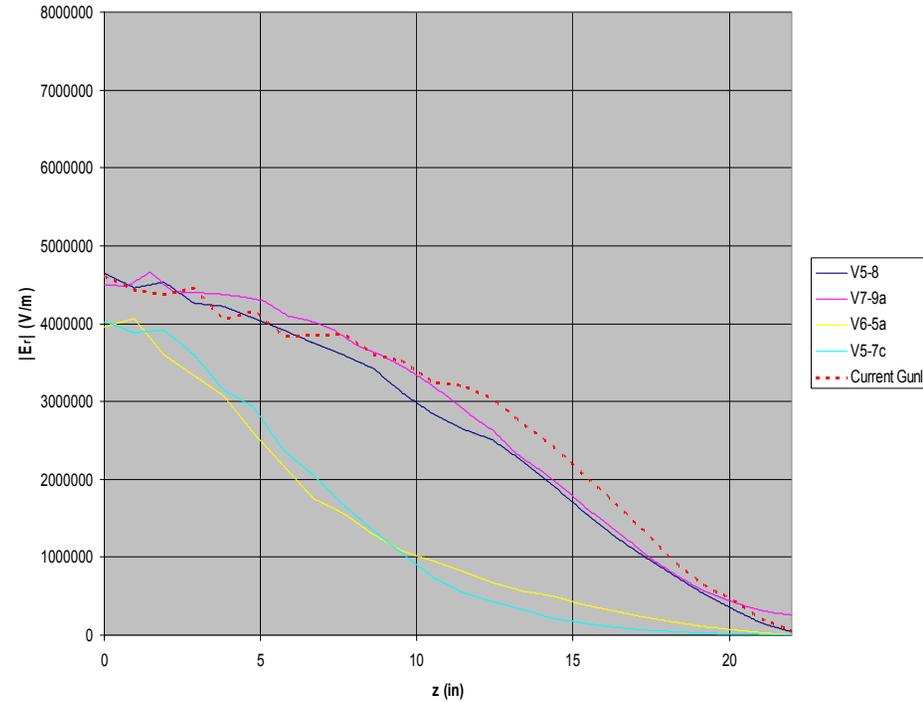


- Comparison of $|E_{\perp}|$ at $r = 2.225$ and $r = 2.5$

$|E_r|$ at $r=2.225$ Across All Models



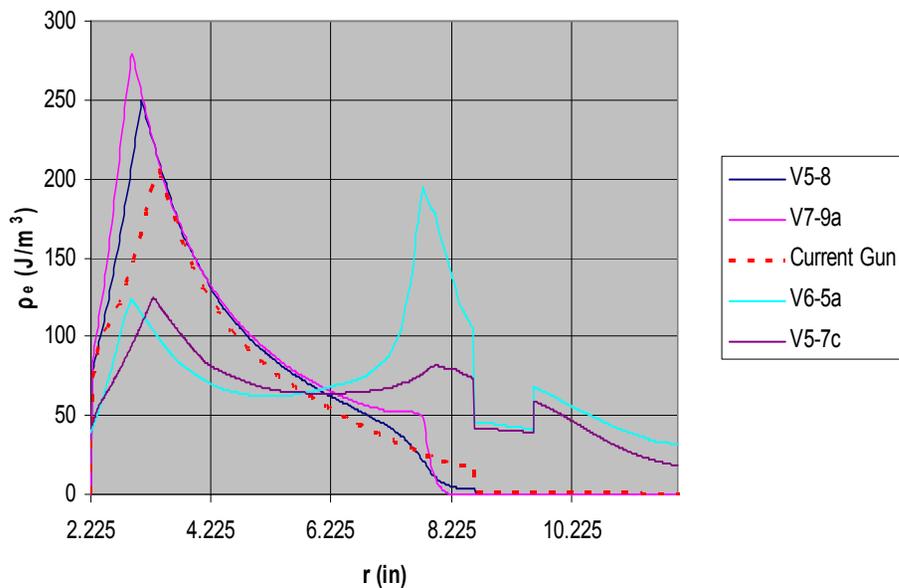
$|E_r|$ at $r=2.225$ Across All Models



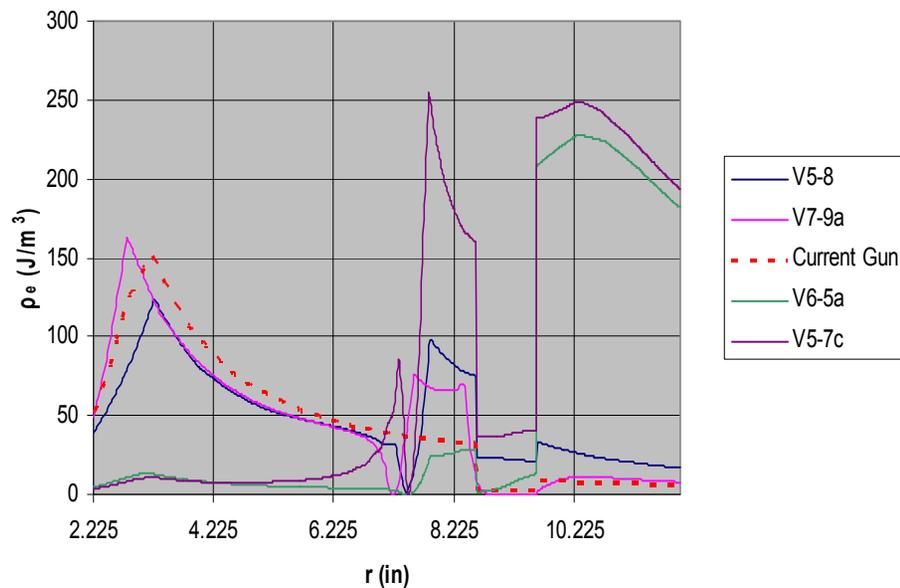


- Comparison of ρ_e at $z=4$, $z=10$, $z=16$

Energy Density at $z=4$ Across All Models

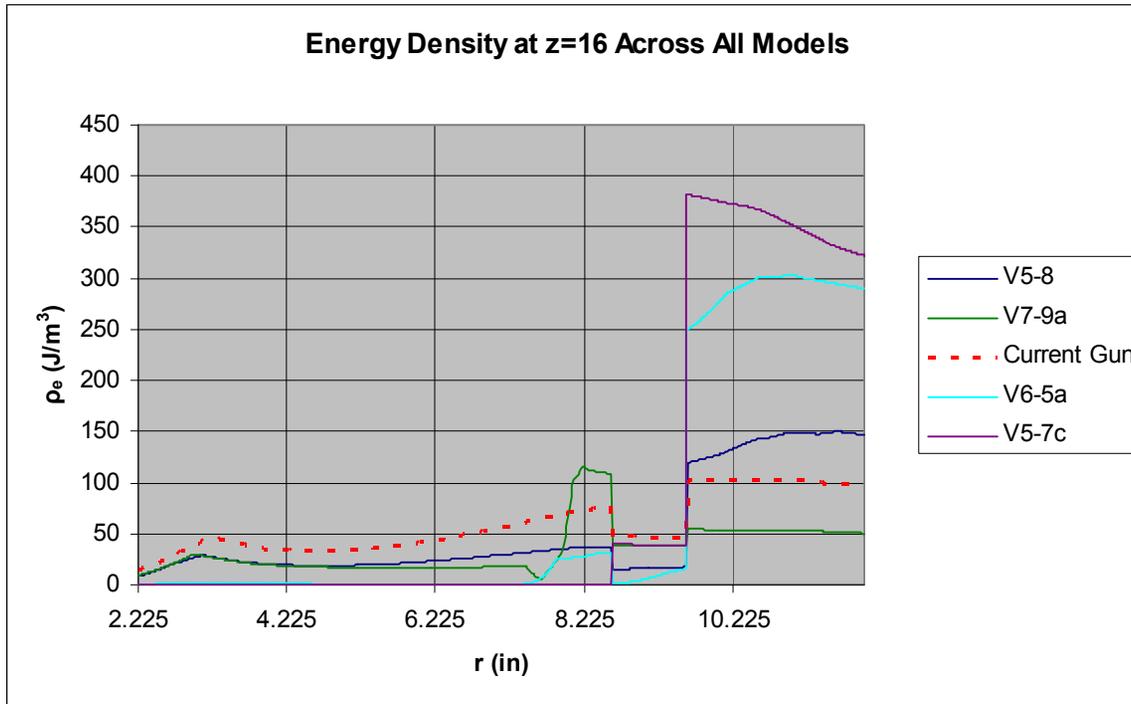


Energy Density at $z=10$ Across All Models





- Comparison of ρ_e at $z=4$, $z=10$, $z=16$ (cont'd)





- Comparison of maximum value of $|E|$ at crucial locations throughout models

		$ E_{\max} (\text{MV/m})$					
Location	r (in)	z (in)	6-5a	5-7c	7-9a	5-8	Original
Inner bottom ring	7.75	2.25	6.08	5.56	1.44	1.74	2.37
Outer Top Ring	10.25	18.75	11.6	10.8	21.3	17.0	17.3

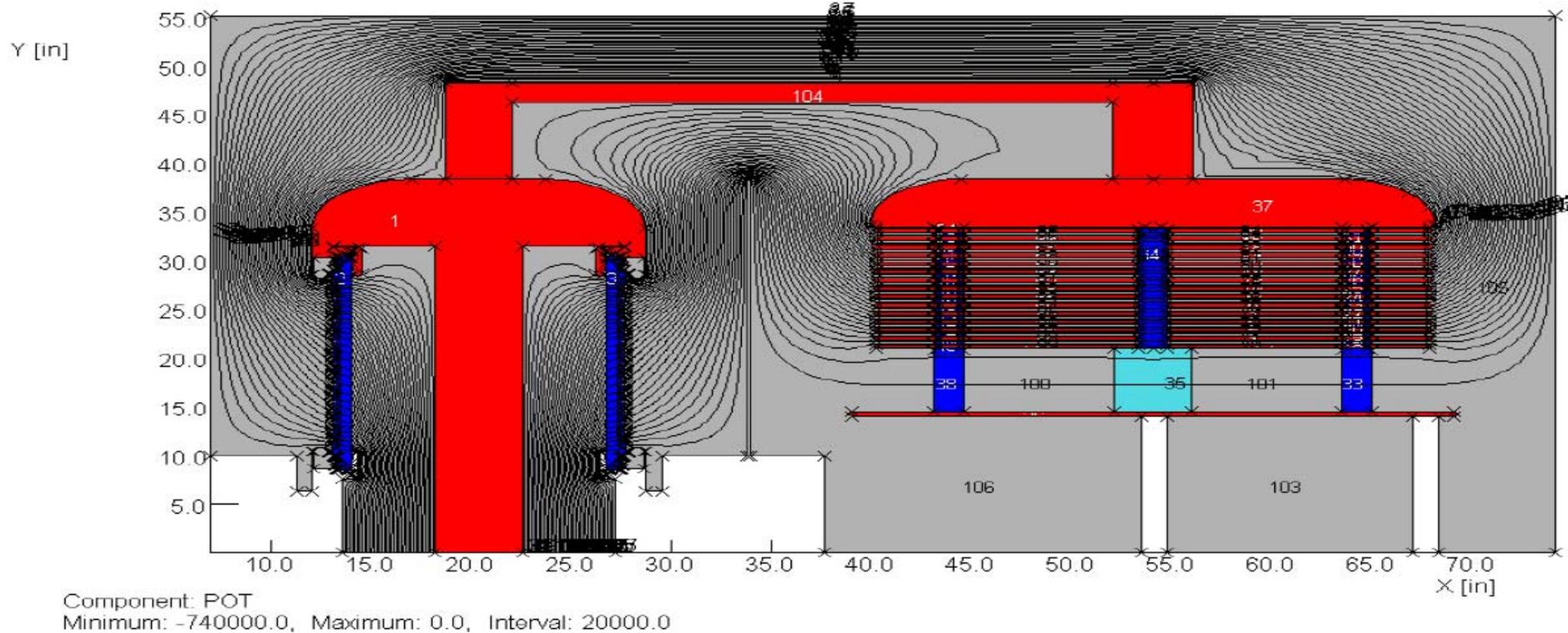


- Model 5-7c (seen in previous slide) most advantageous
 - Uses metal coating/thin sheet at equipotential with stalk
 - Note: so far, any type of coatings on ceramics have failed
 - Electron emission likely to happen anyway, better to focus on deflecting electrons
 - Significantly decreased E_{\perp} at surface of stalk
 - Lower, more constant energy density distribution
 - Lower average maximum value of $|E|$ at critical points
 - Decreased amount of conductor rings ->less brazing



Side Project: Uniform Energy Density Distribution

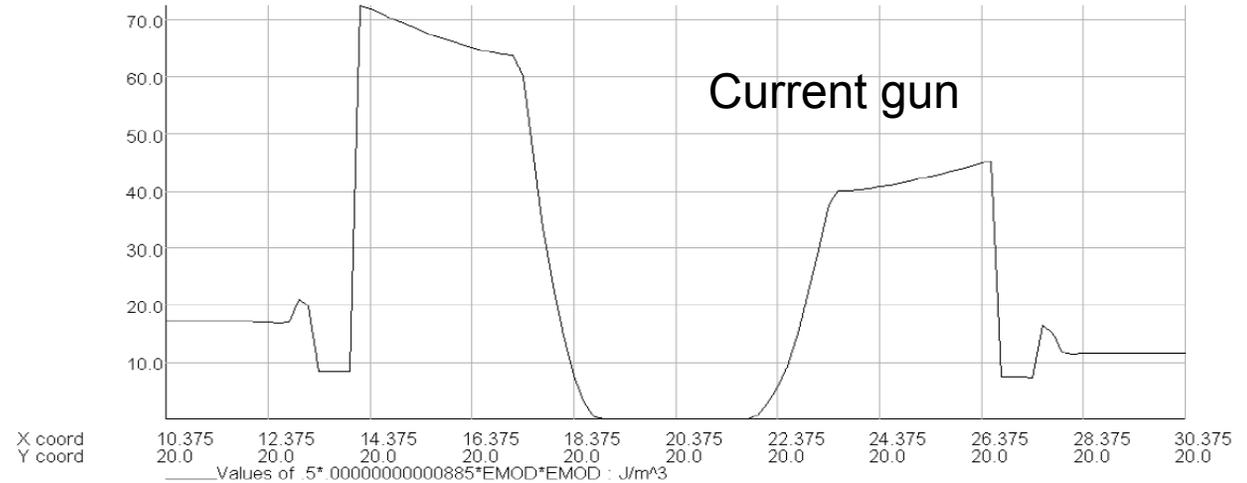
- Can increase field energy density uniformity by compartmentalizing gun and power supply in cylindrical tanks



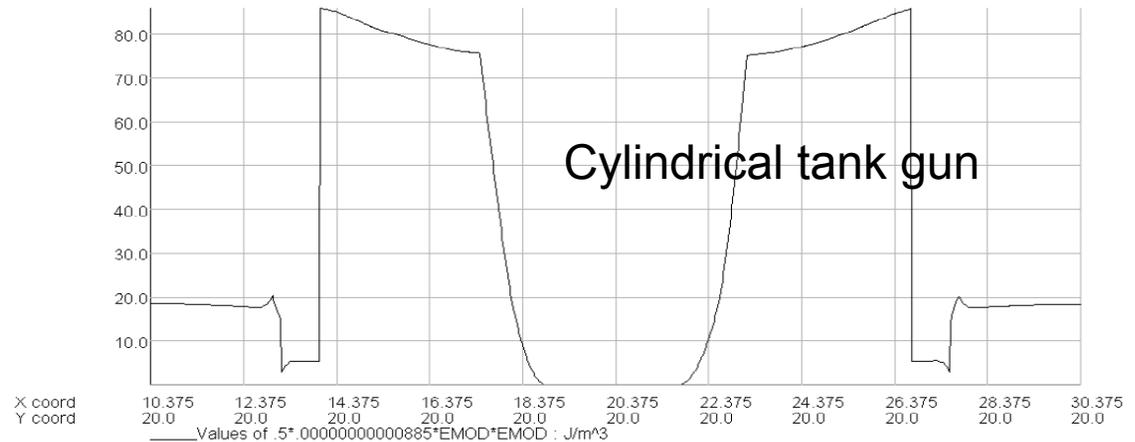


- Comparison of ρ_e in current gun model and cylindrical model

Field Energy Density in Current Gun at z=20 inches



Field Energy Density in Cylinder Gun at z=20 inches





- ERL just getting underway
 - Will need new, more robust gun for further phases
 - Modeling done provides foundation for understanding designs and constraints involved in newer high voltage guns (including stalk/ceramic configuration and cathode surface area reduction)
 - Would also be interesting to follow magnetic field deflection idea
- Perhaps designs will be useful in SLAC, CEBAF, ILC...?



- Thank you
 - Karl Smolenski
 - Bruce Dunham
 - Jacob Haimson
 - Bryan Parry
 - George Lucas



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