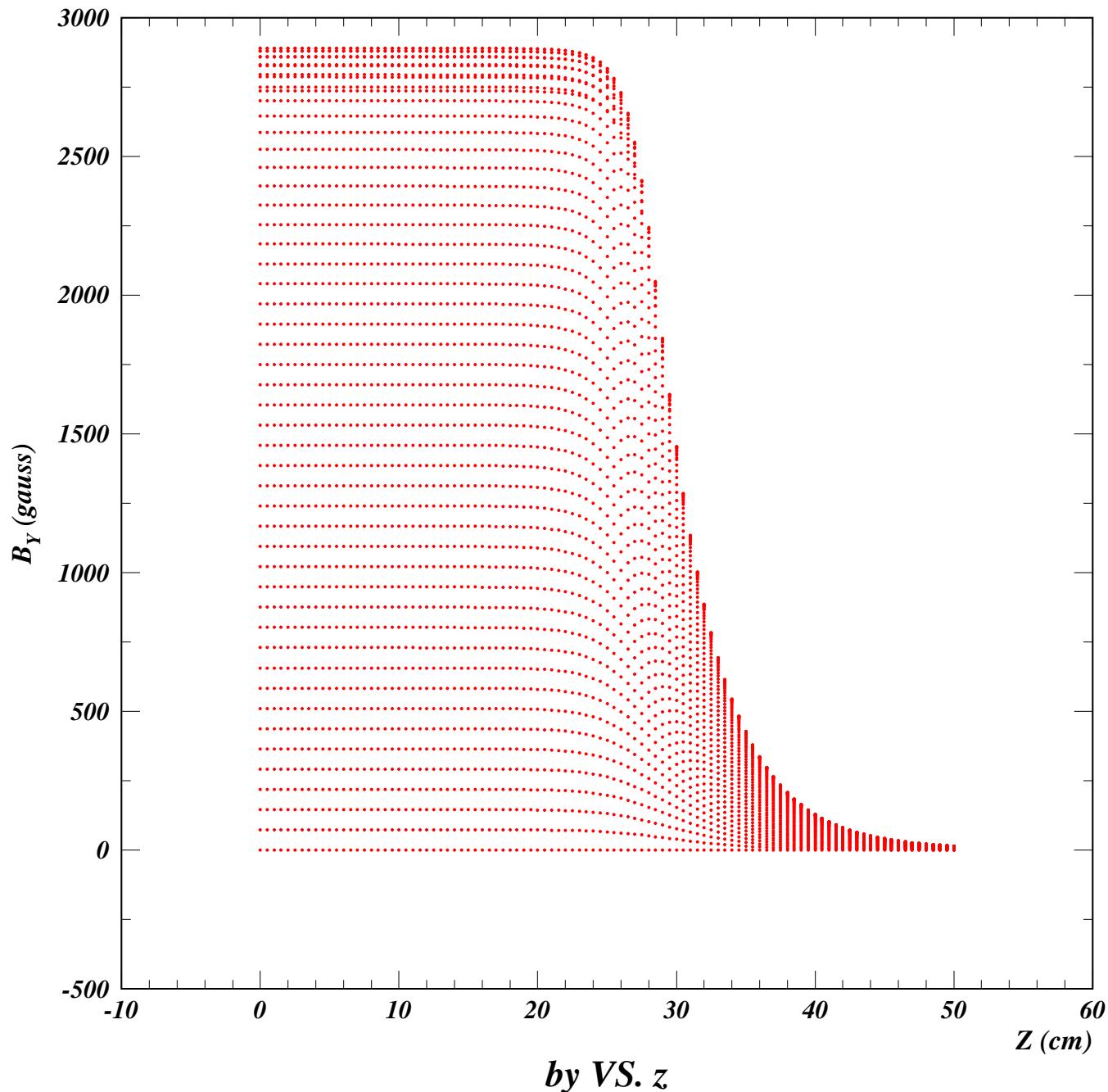


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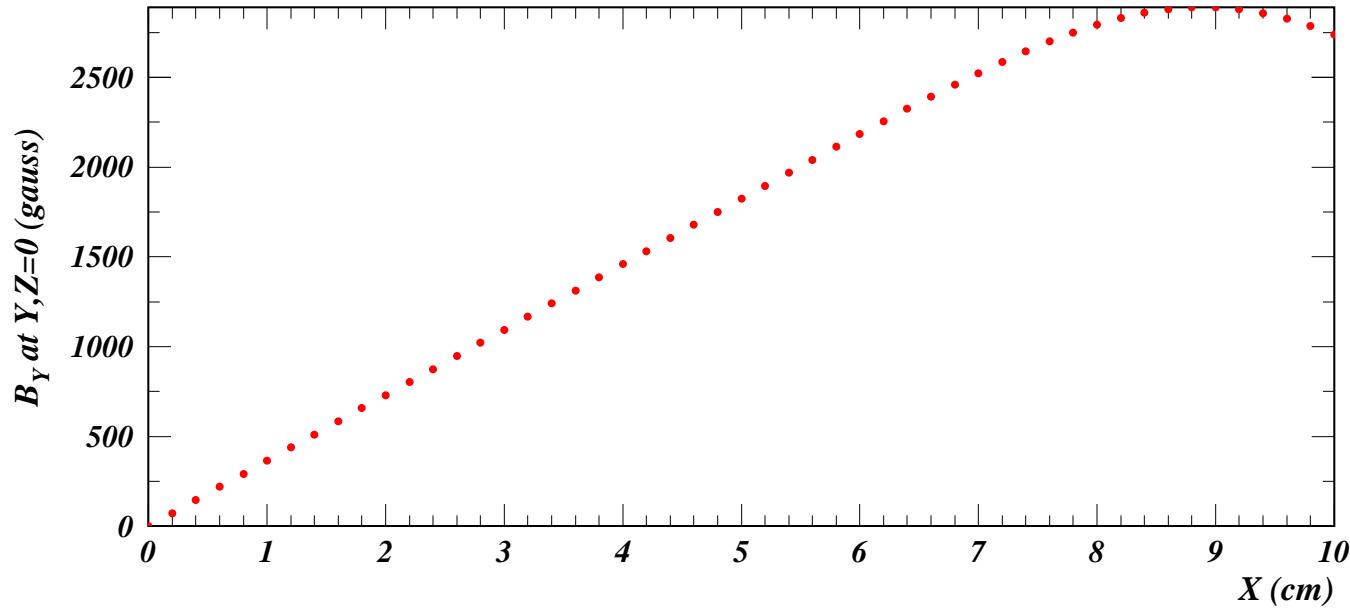
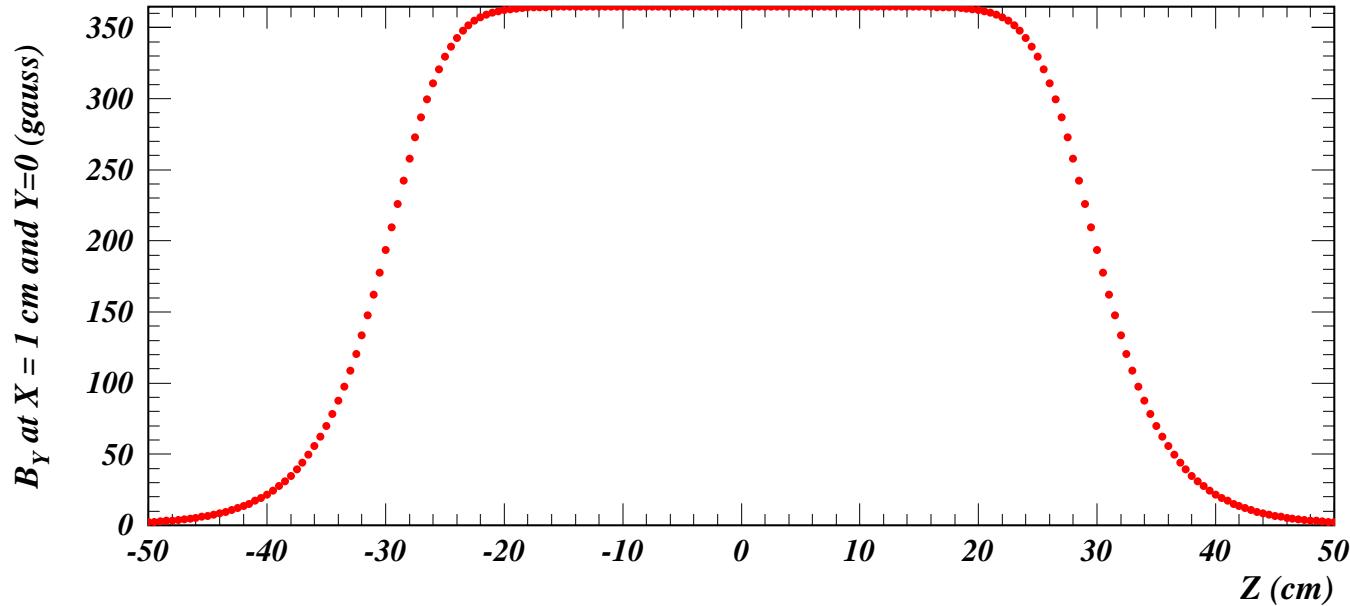
Final design. 114 A. 3.6 T/m.



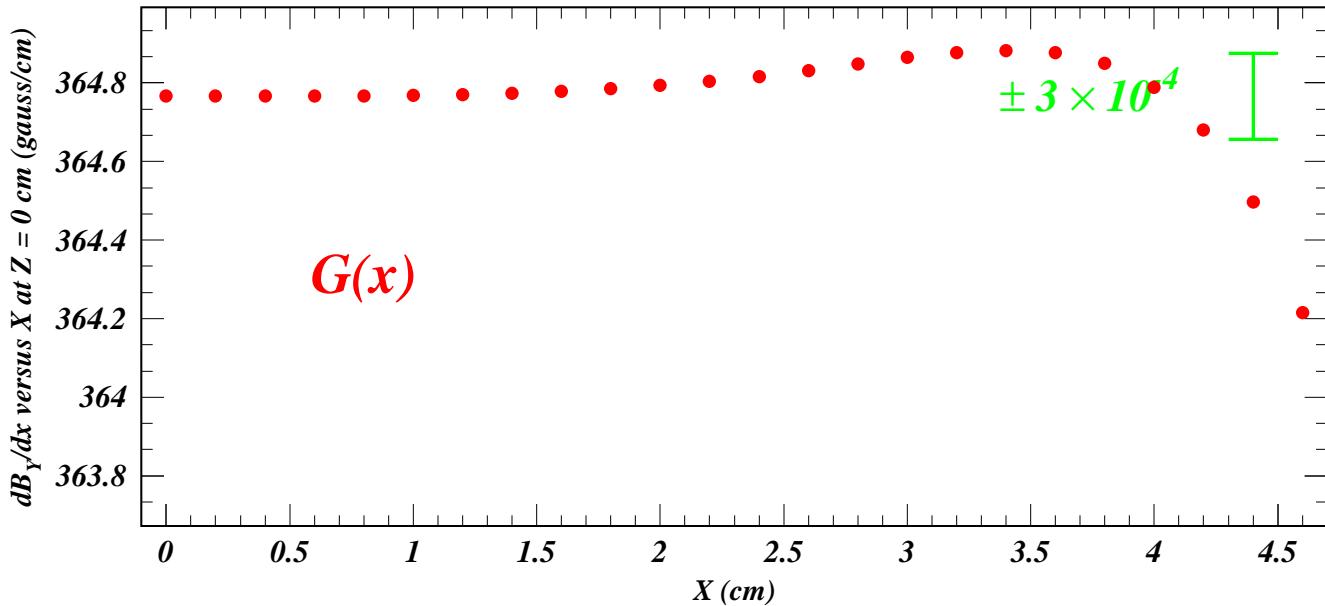
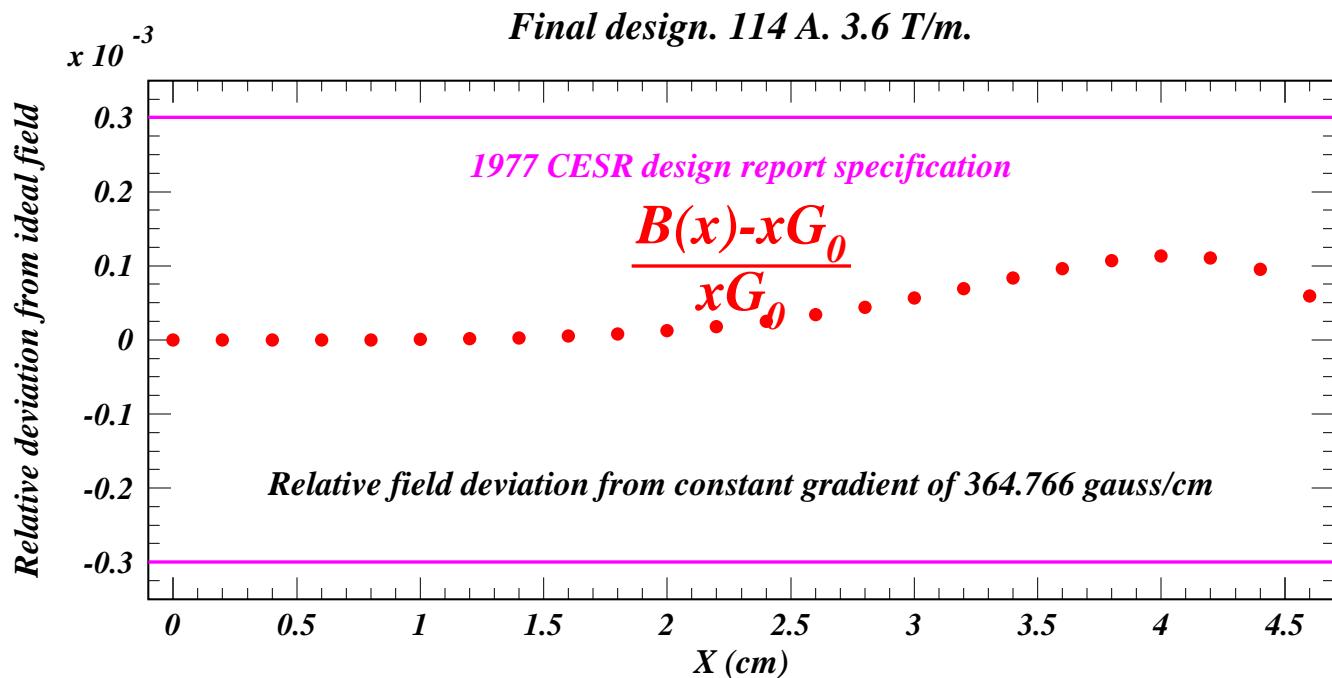
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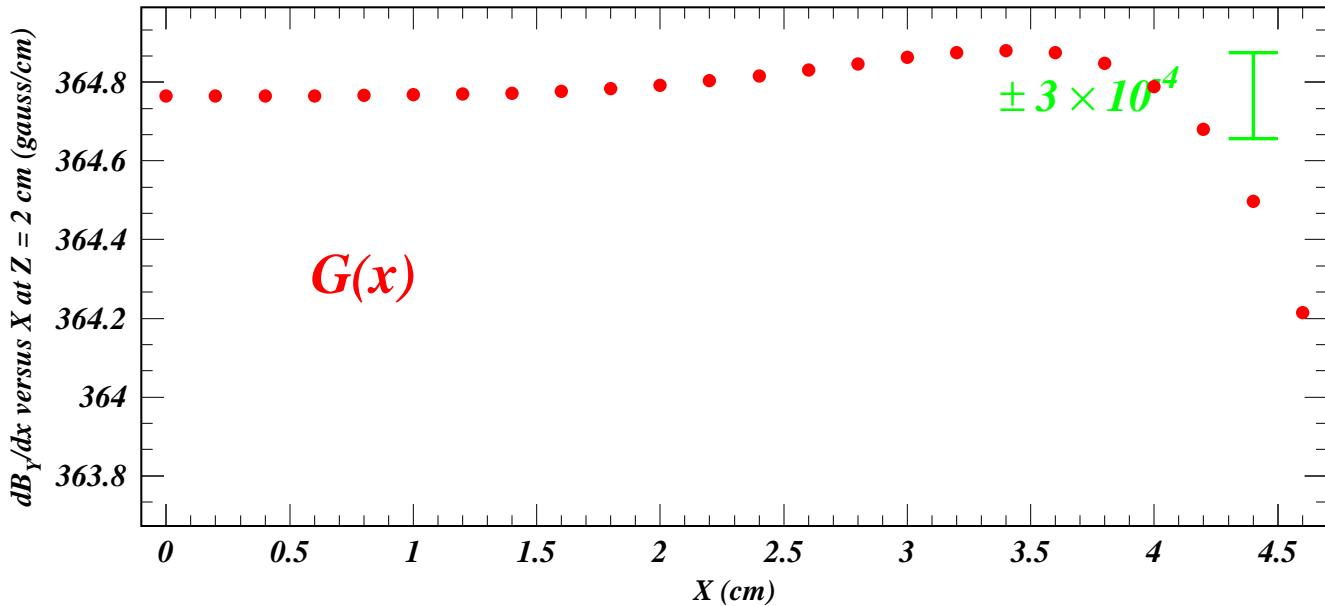
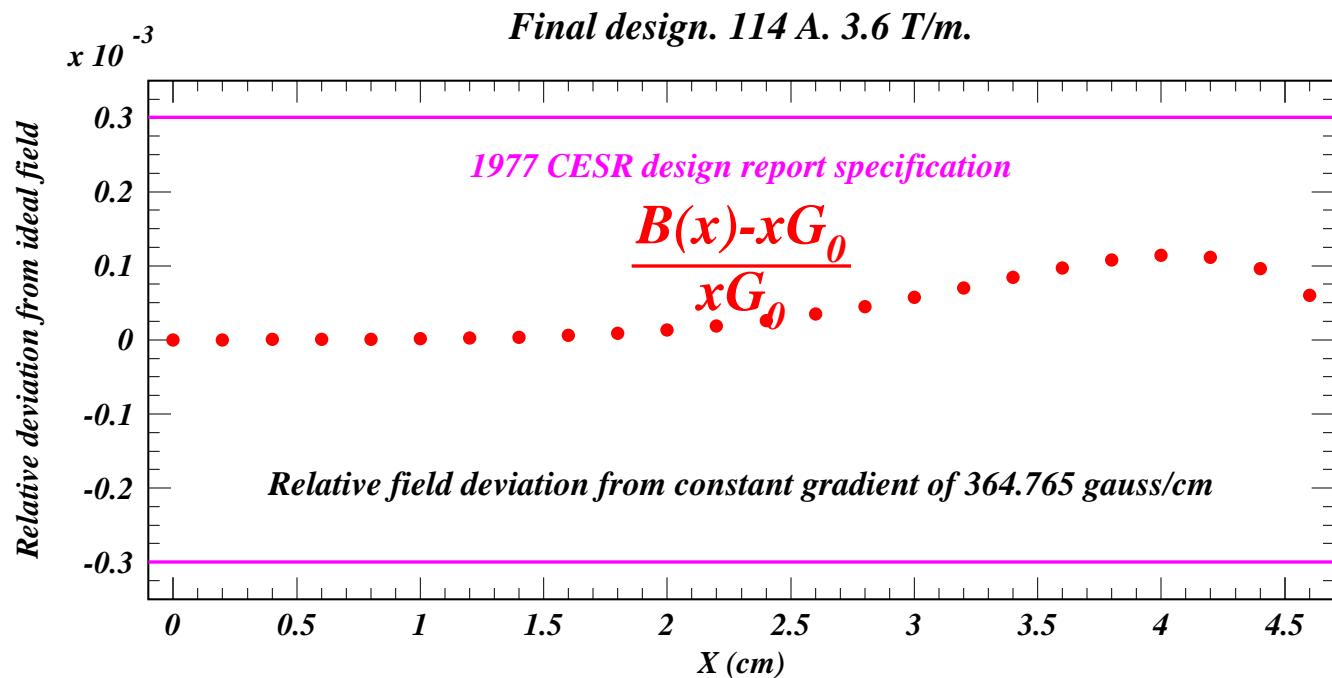
Final design. 114 A. 3.6 T/m.



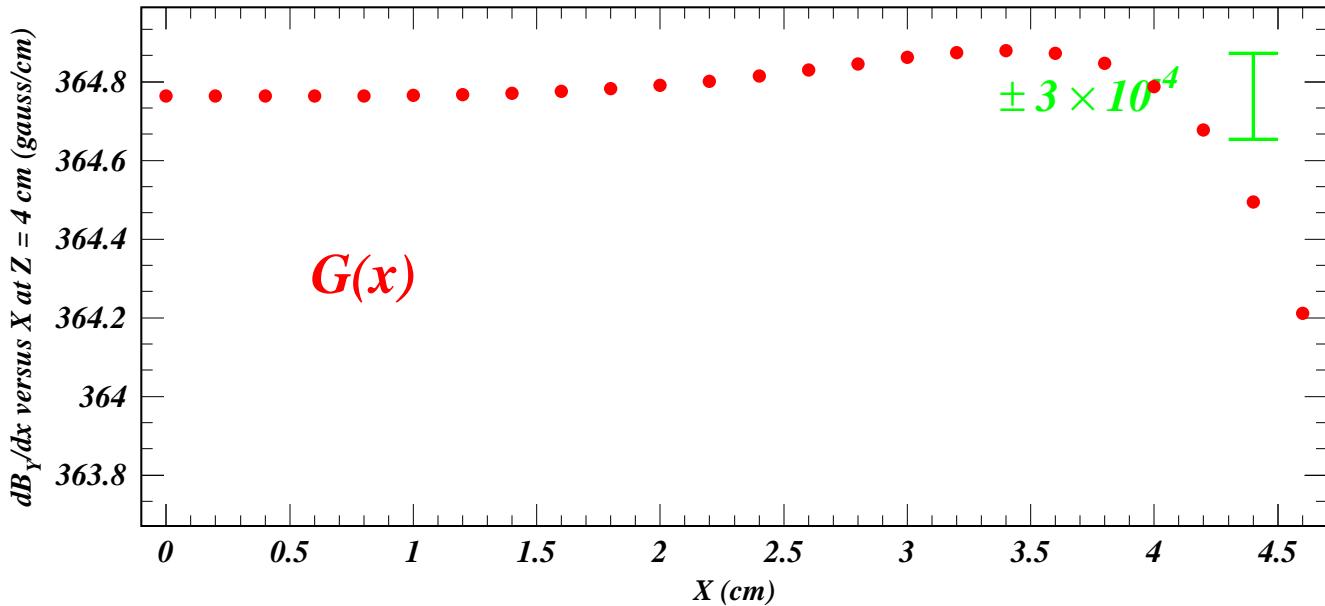
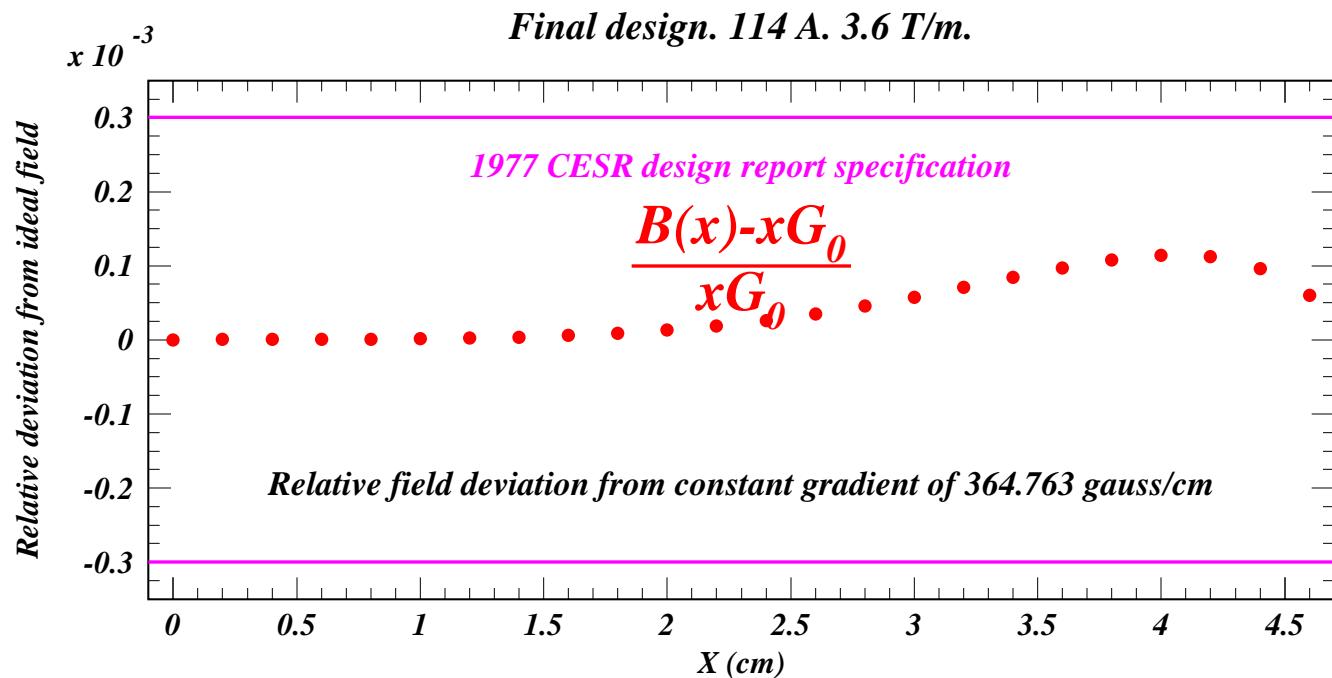
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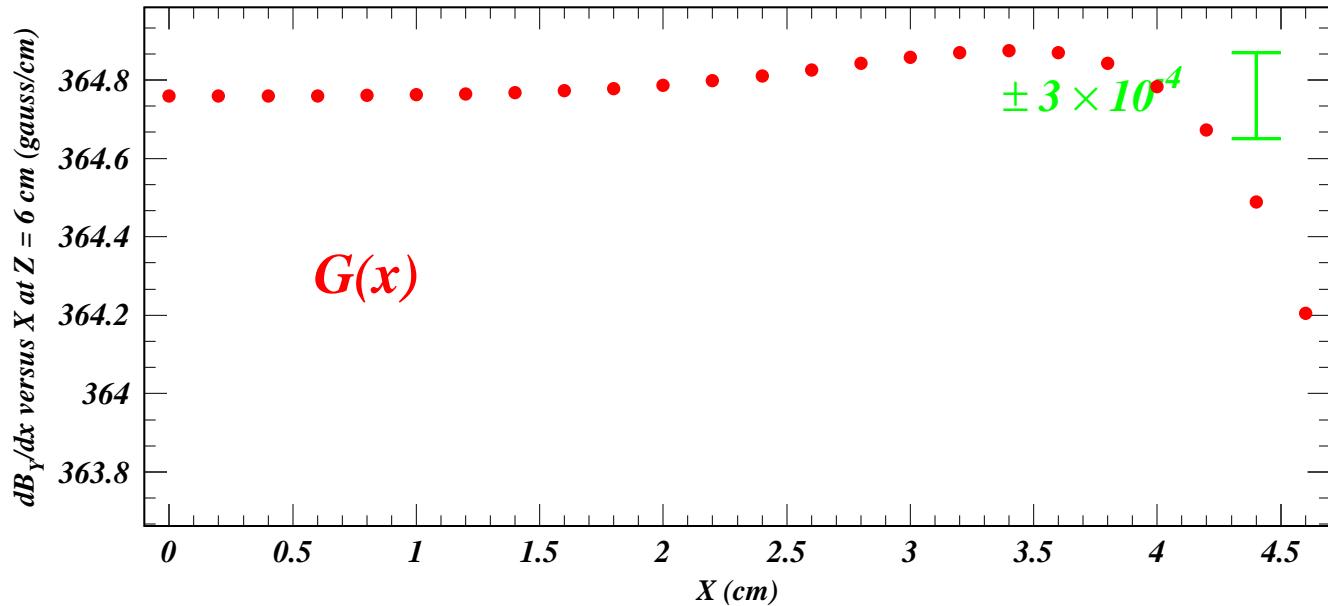
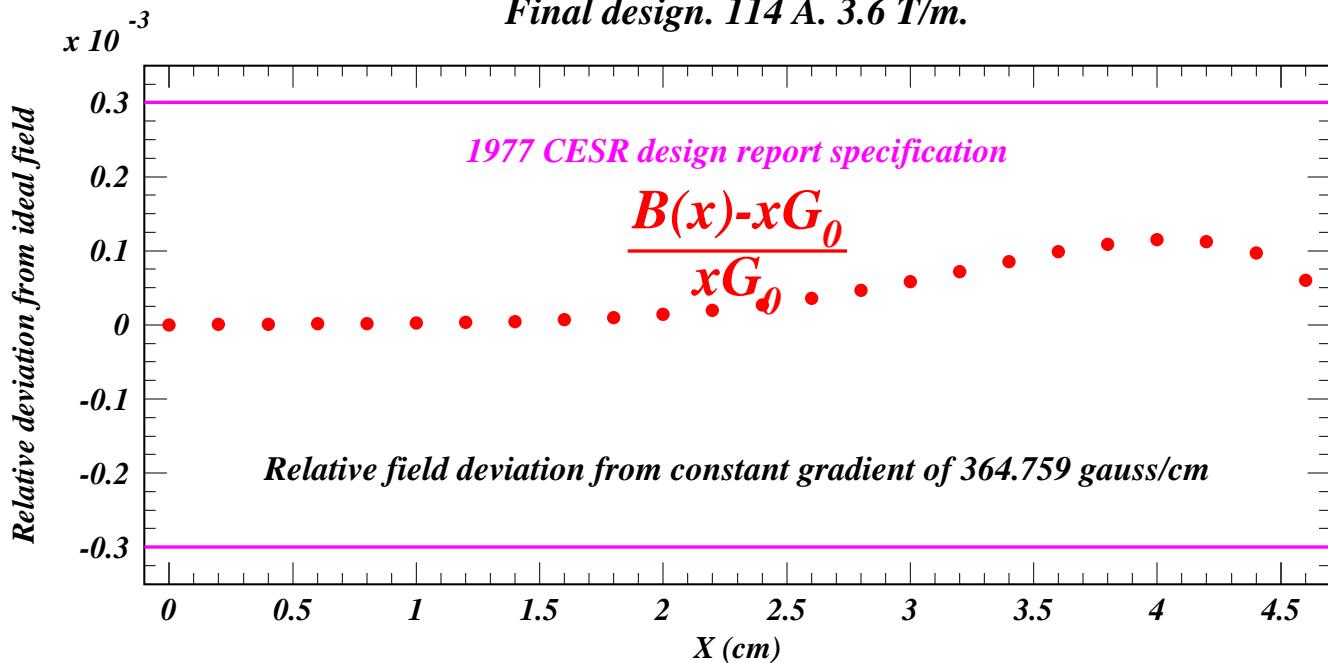


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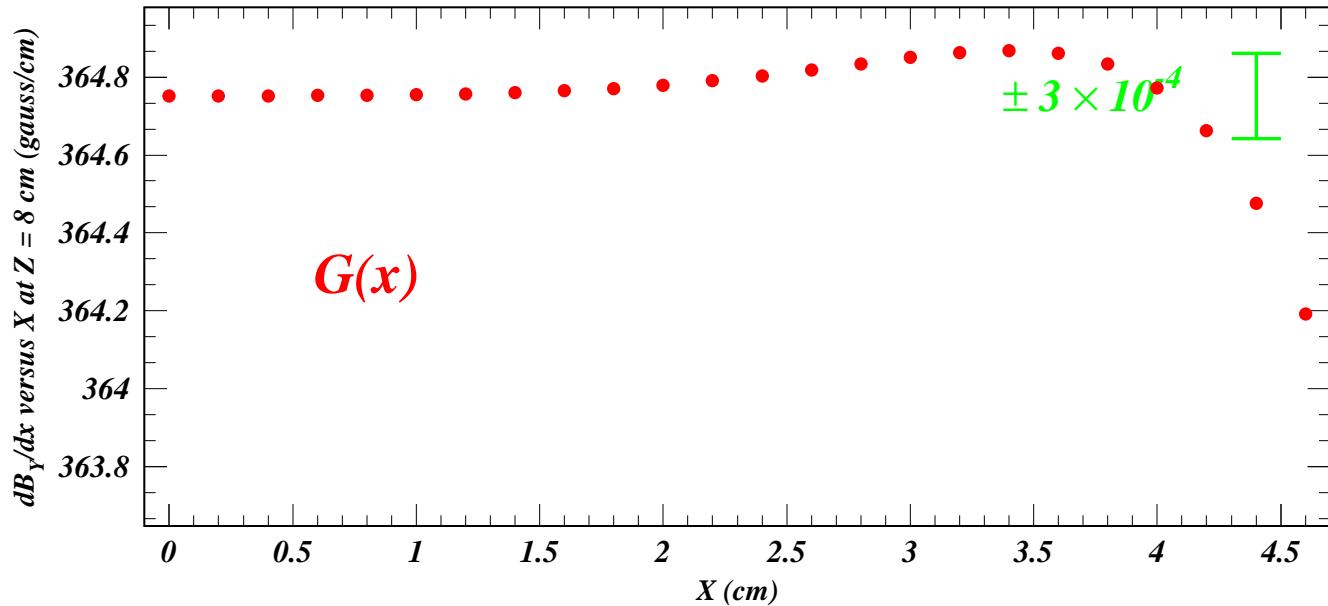
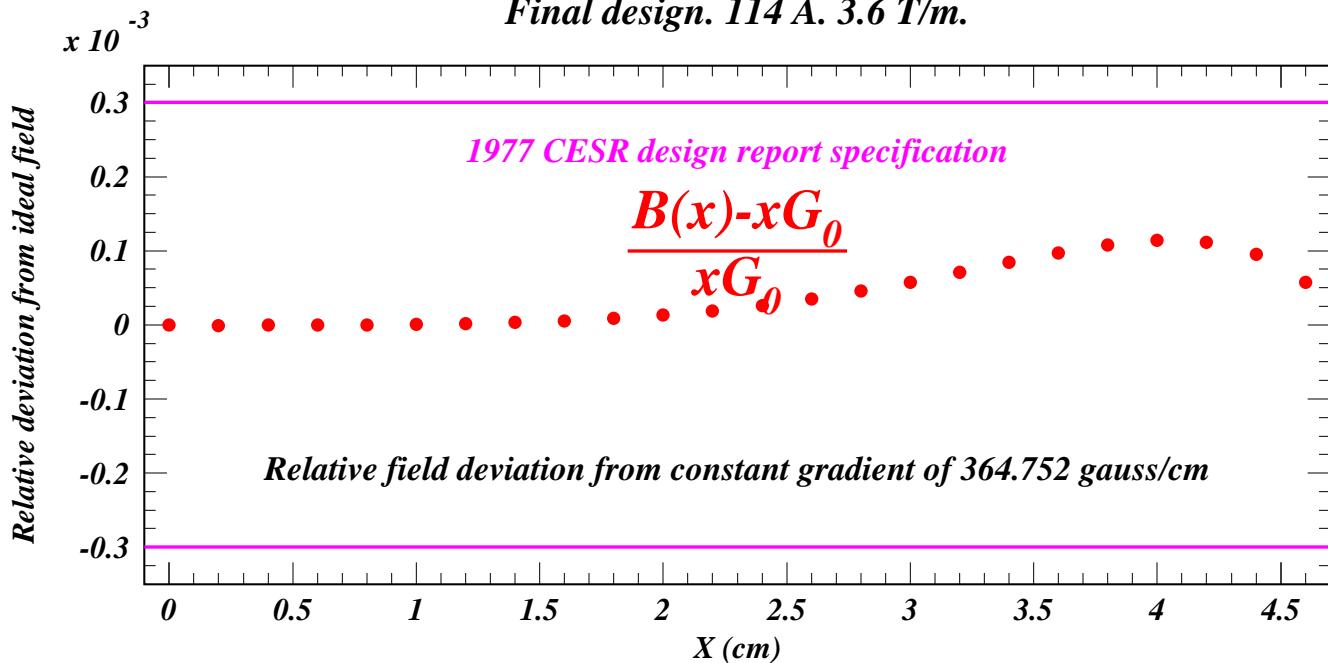
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Final design. 114 A. 3.6 T/m.

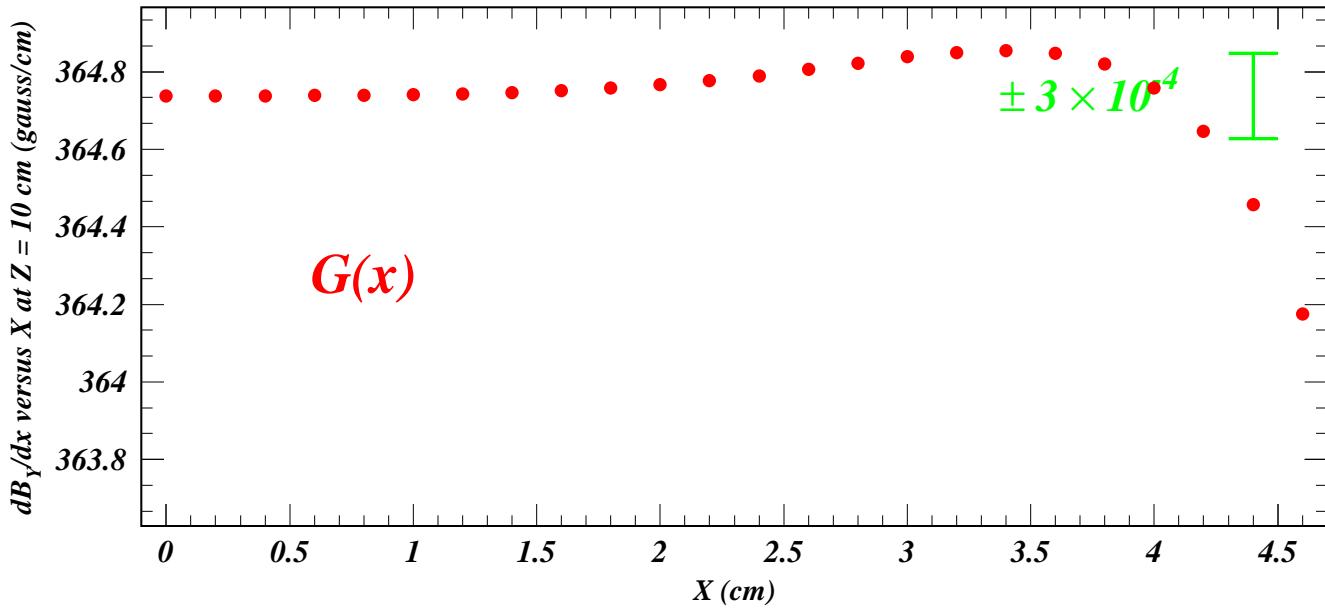
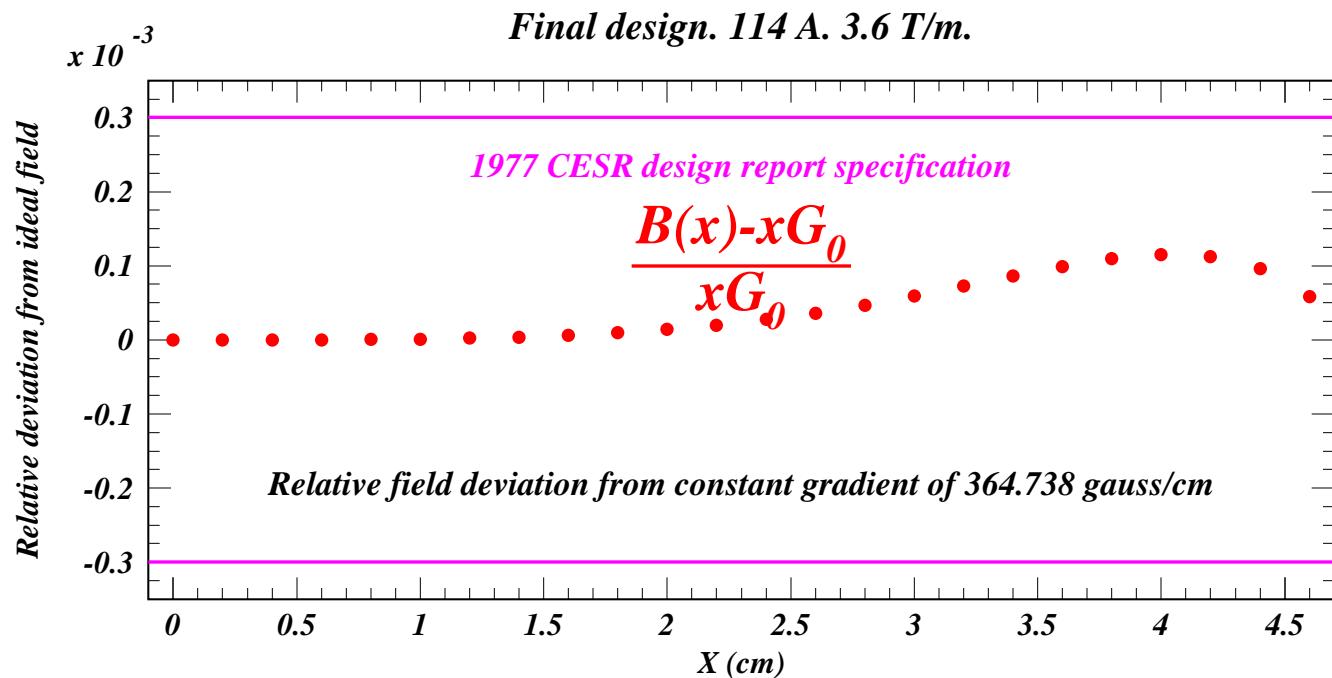


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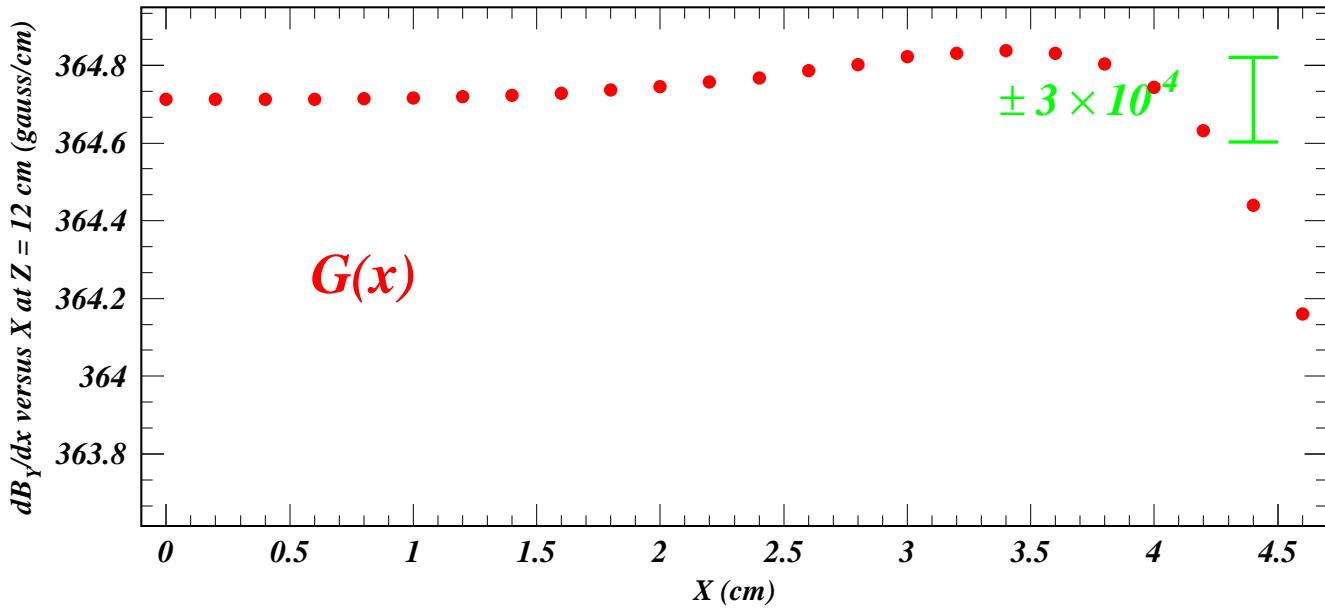
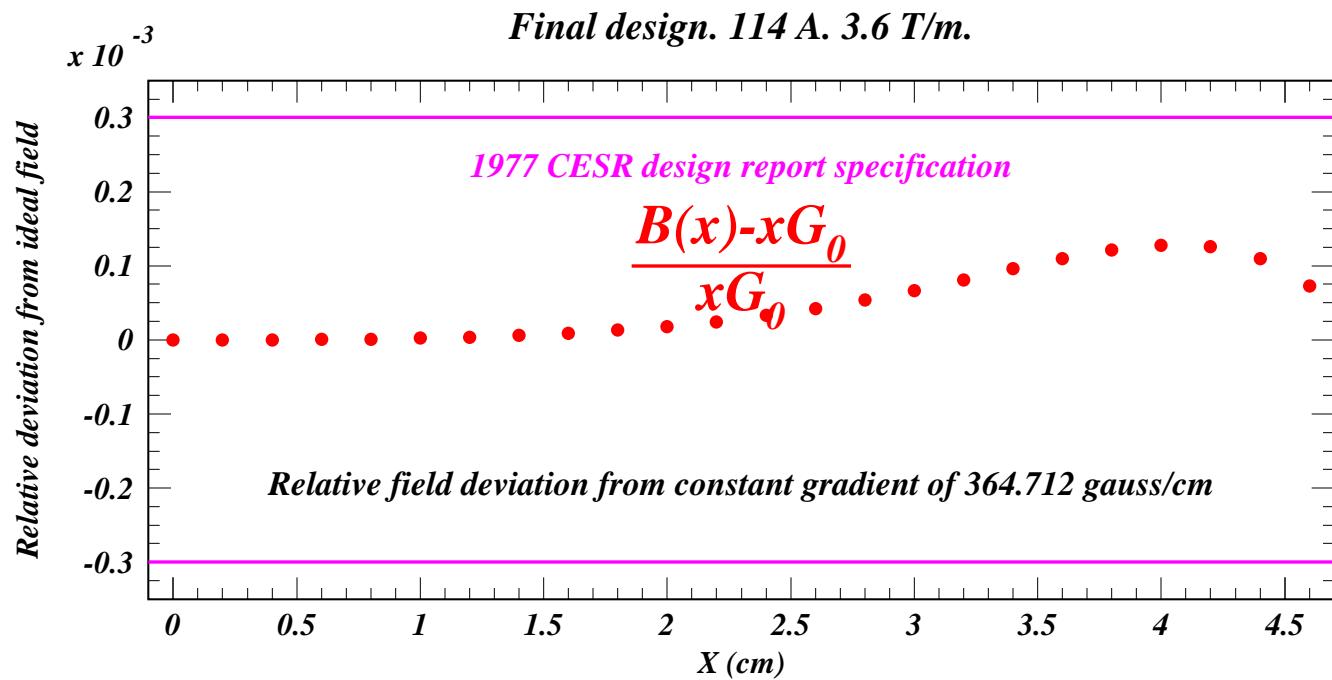
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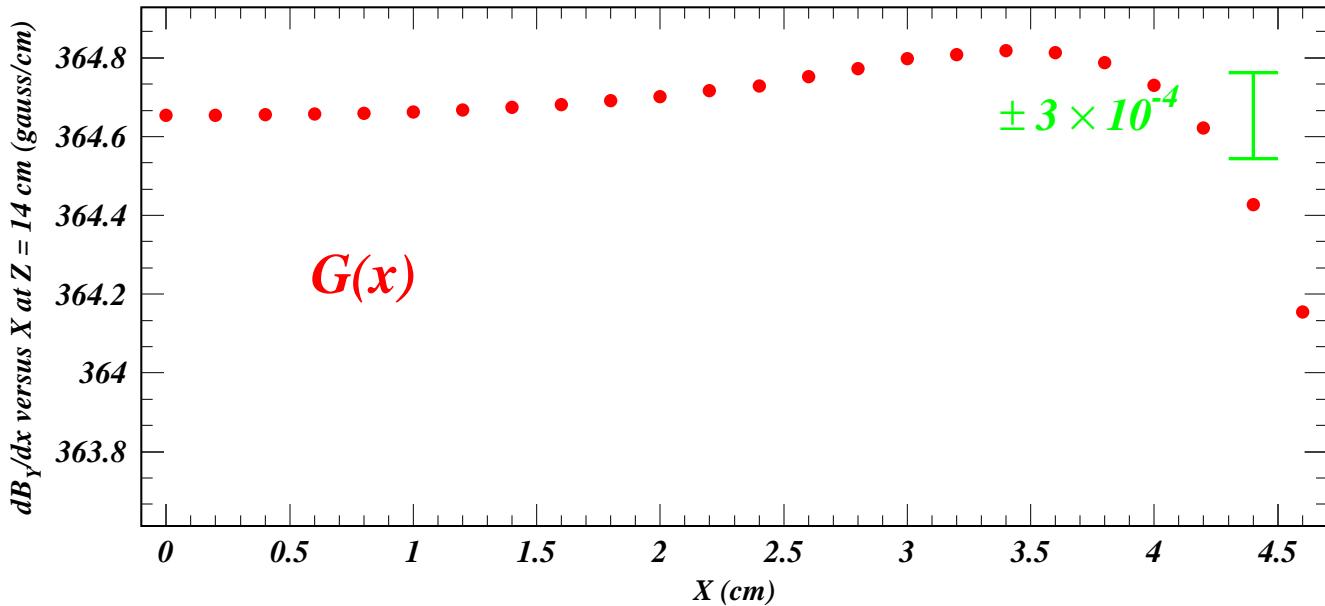
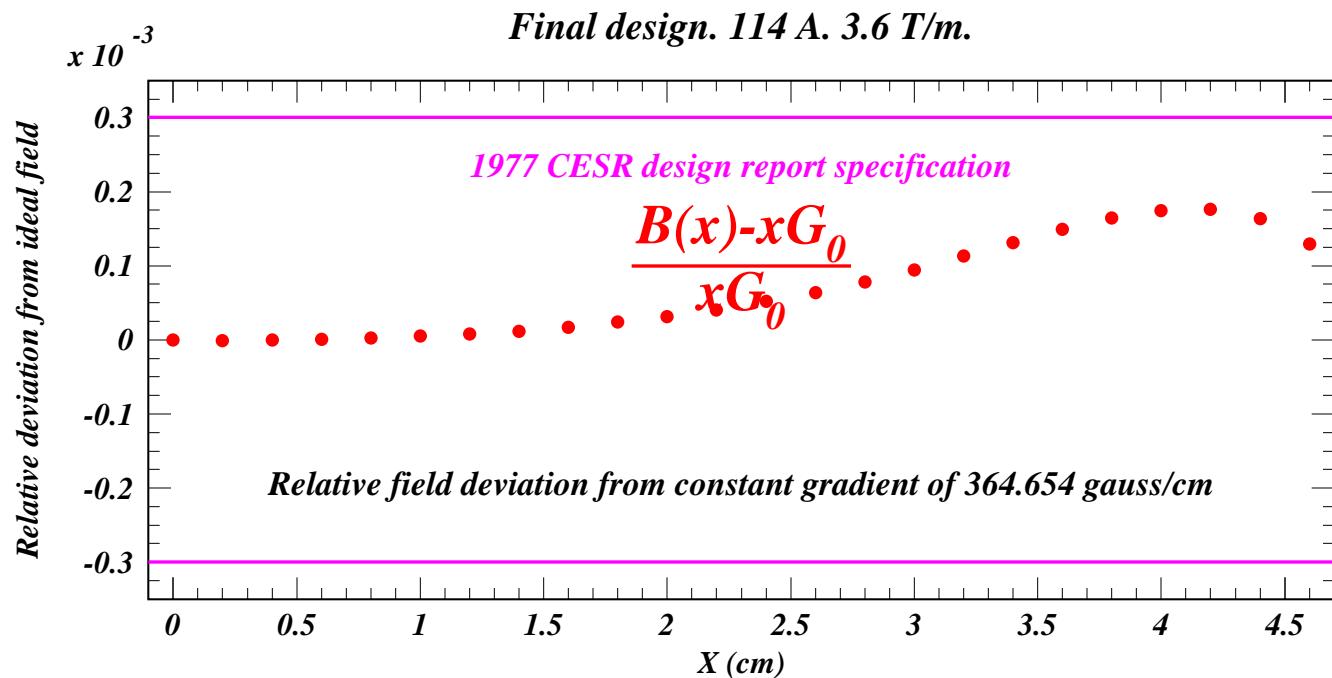
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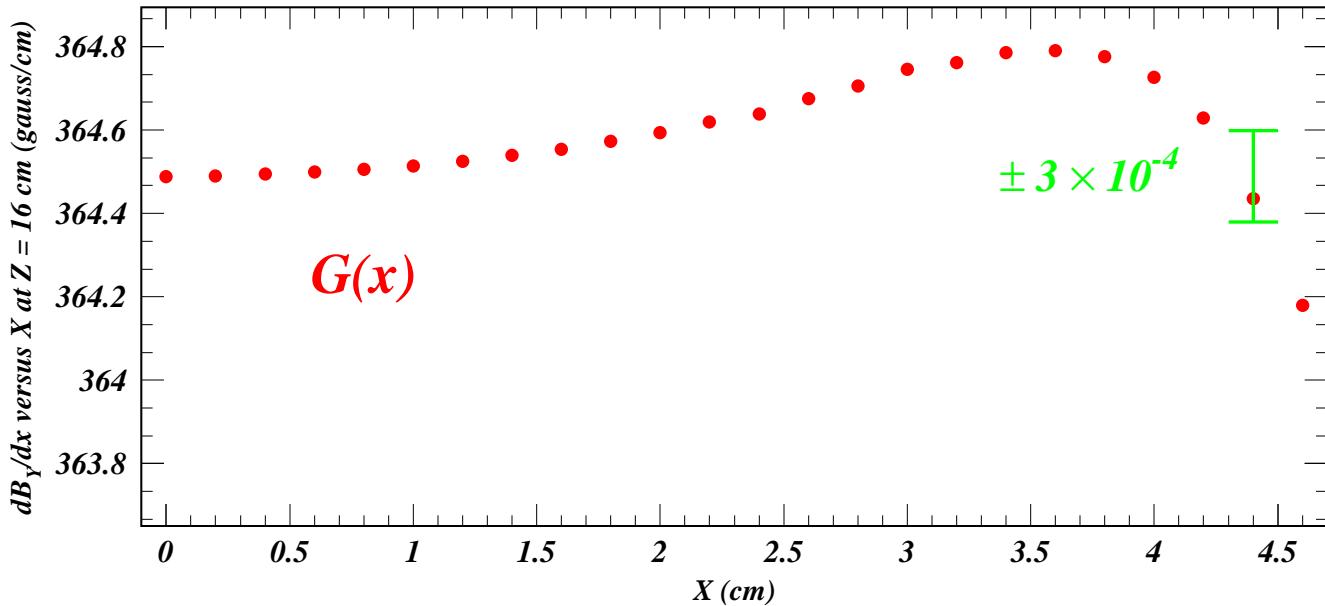
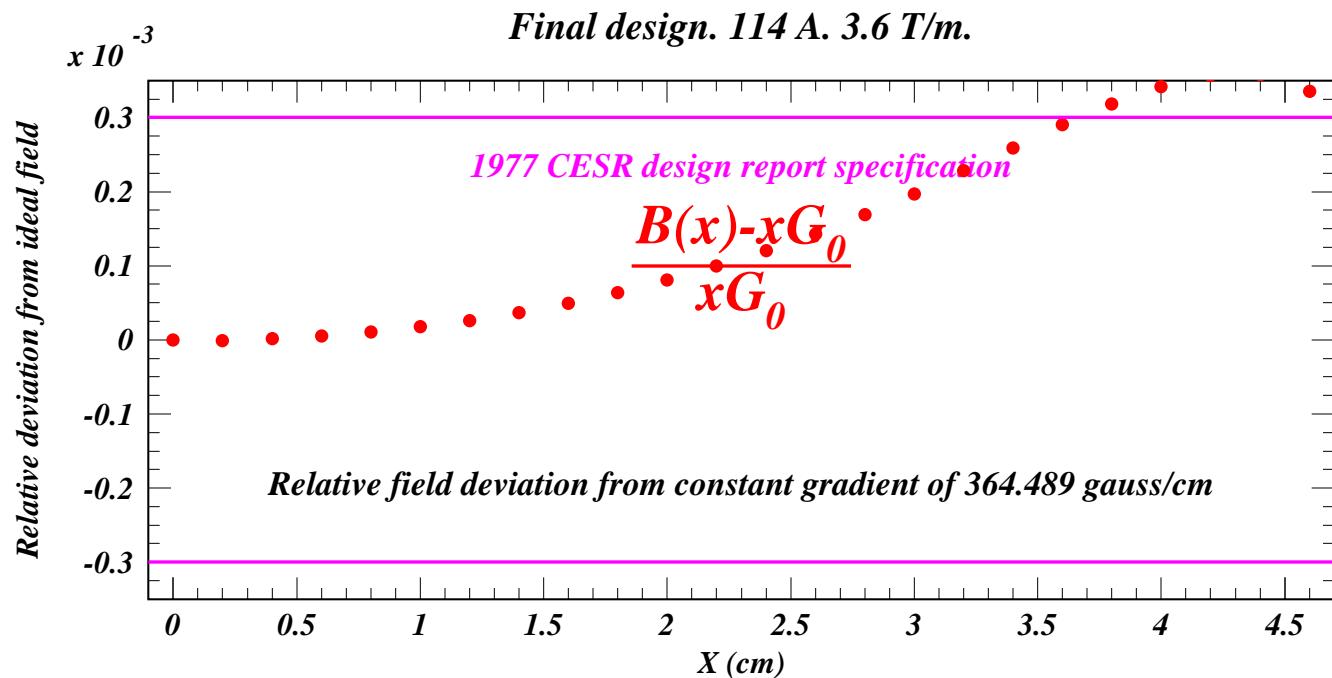
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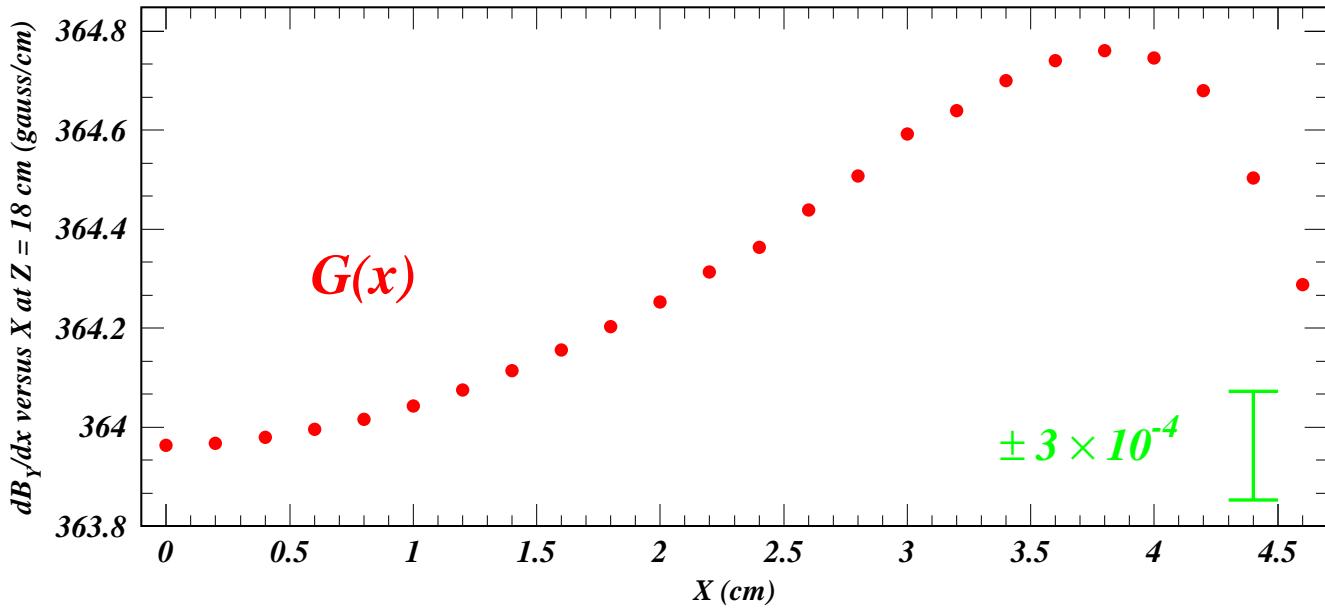
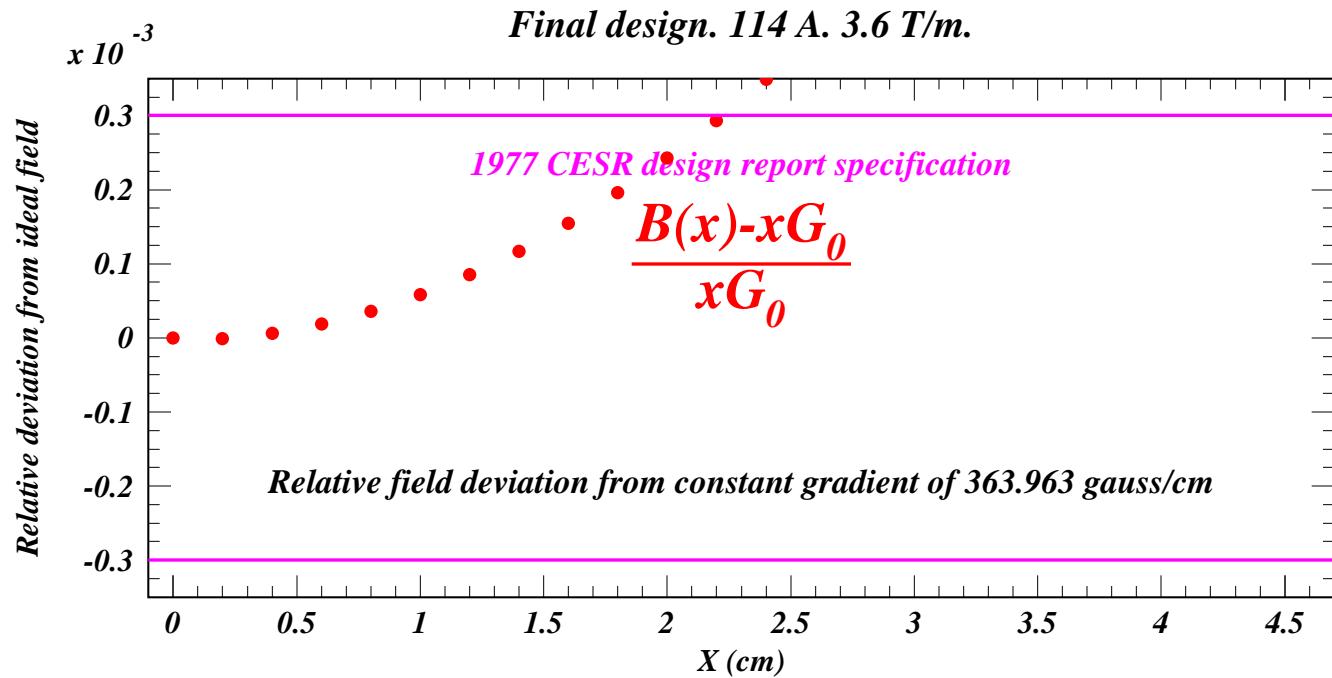
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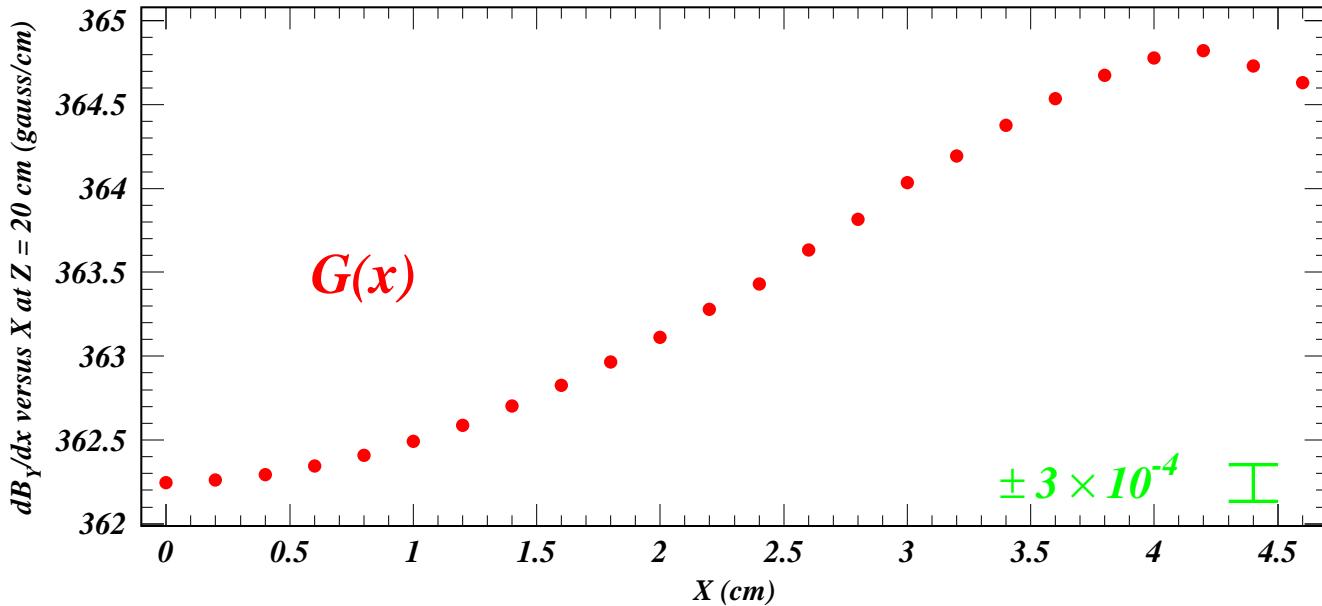
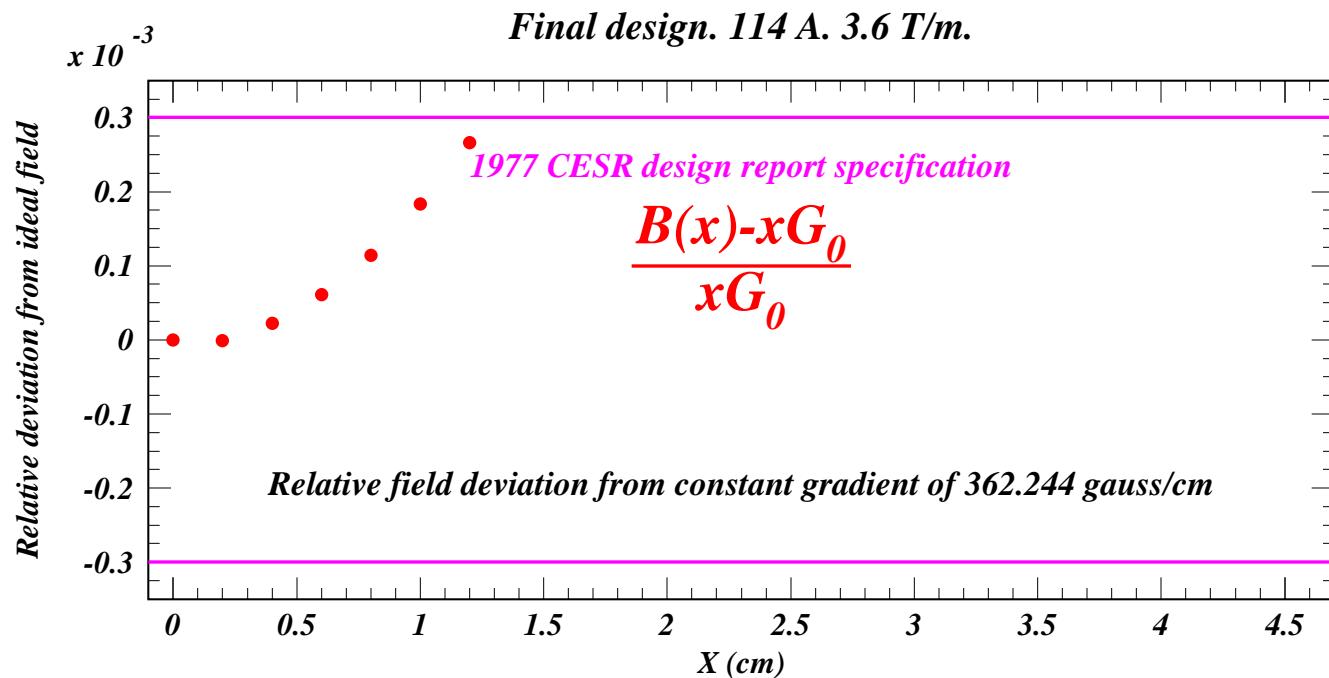
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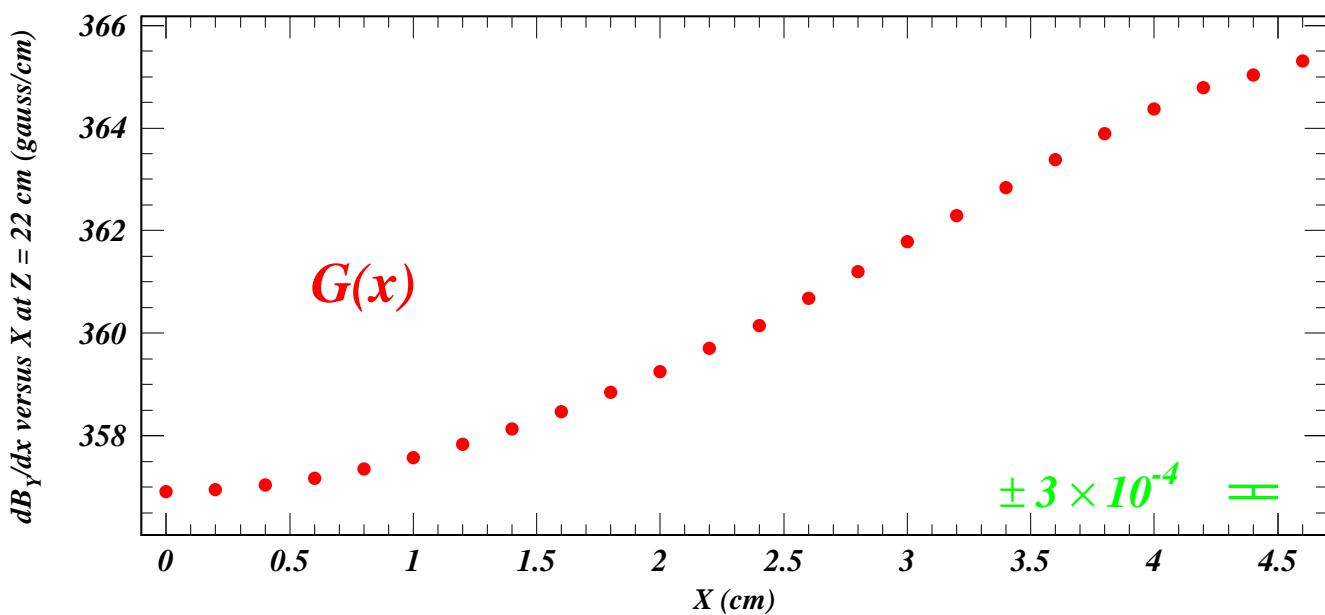
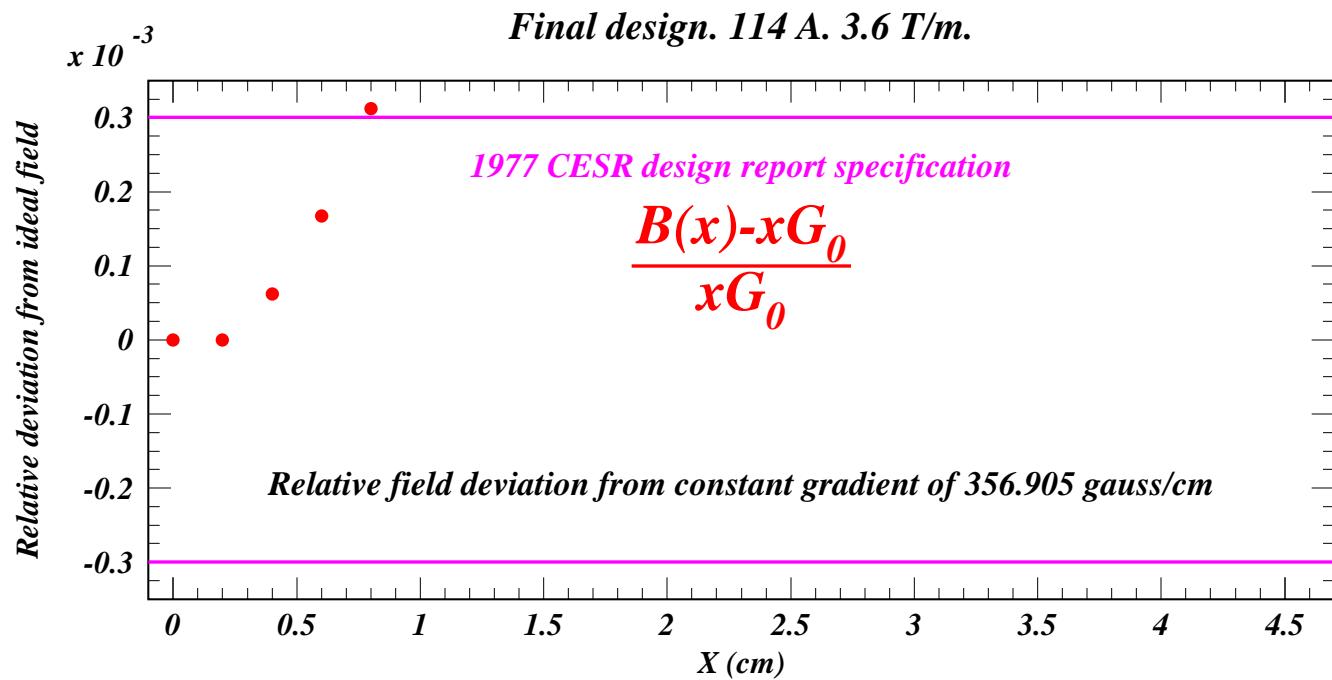
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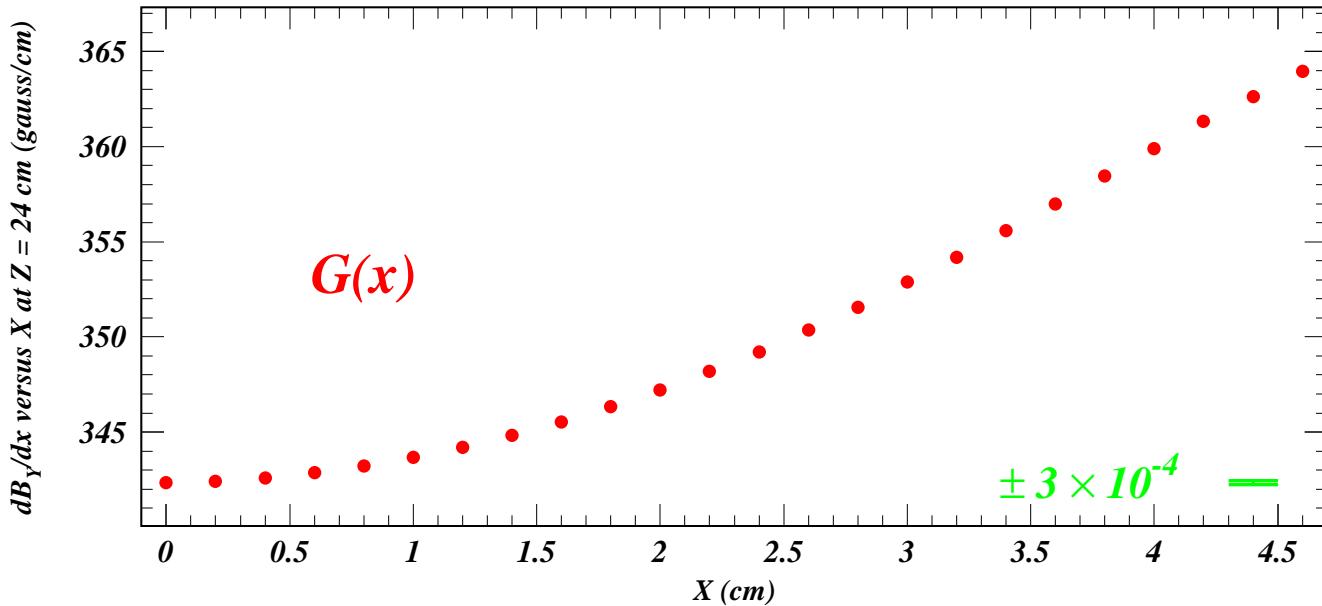
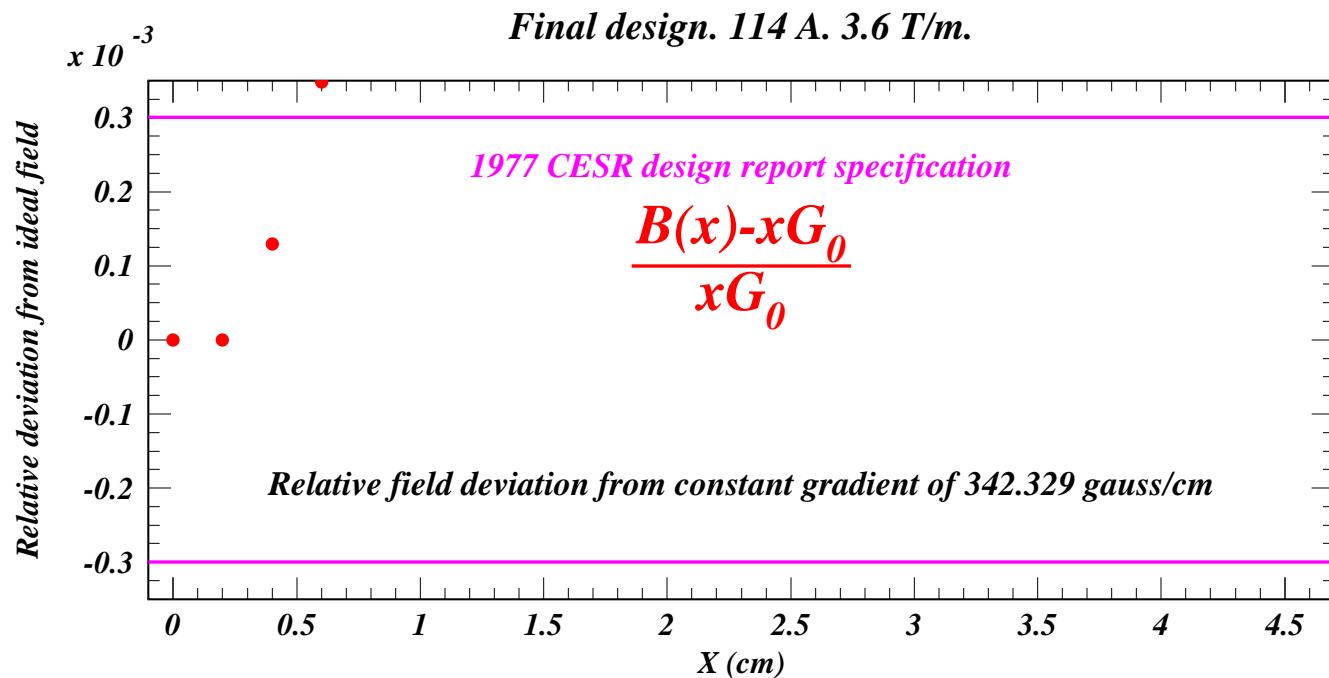
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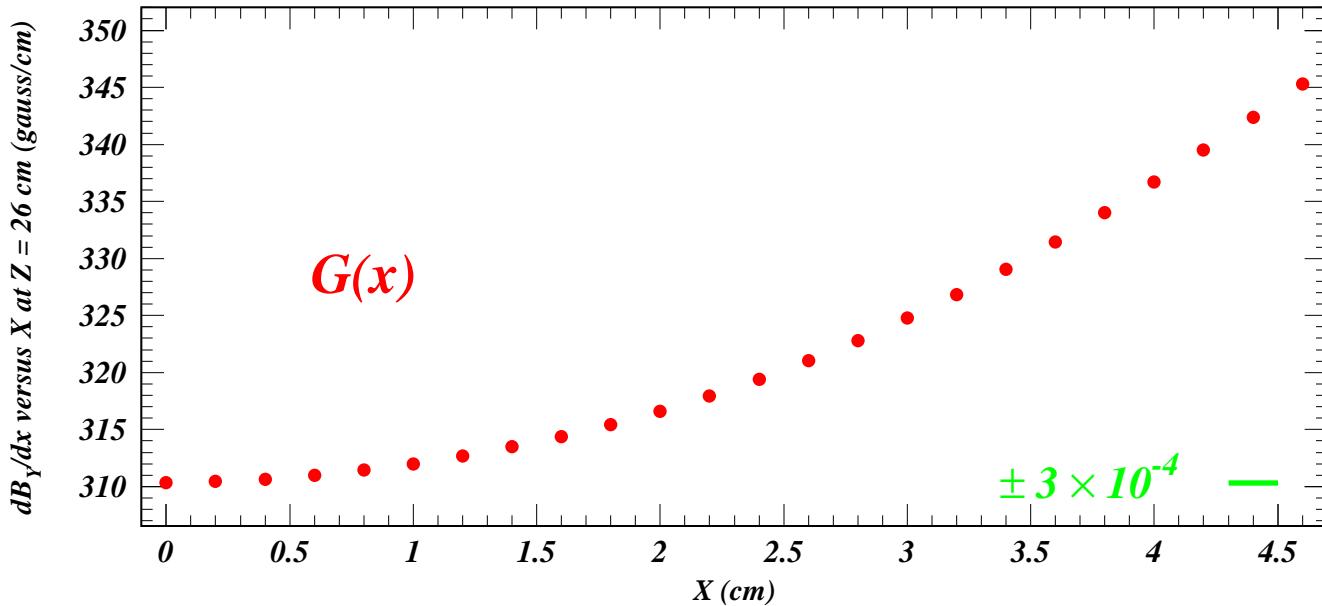
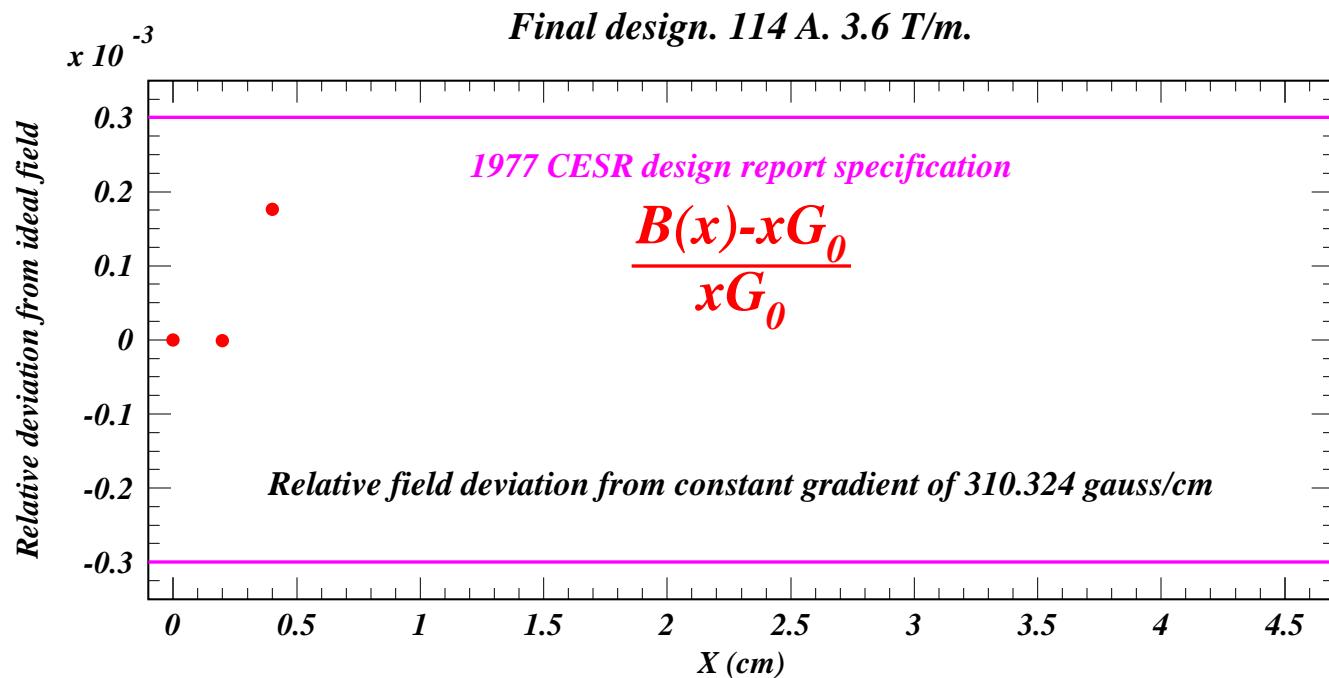
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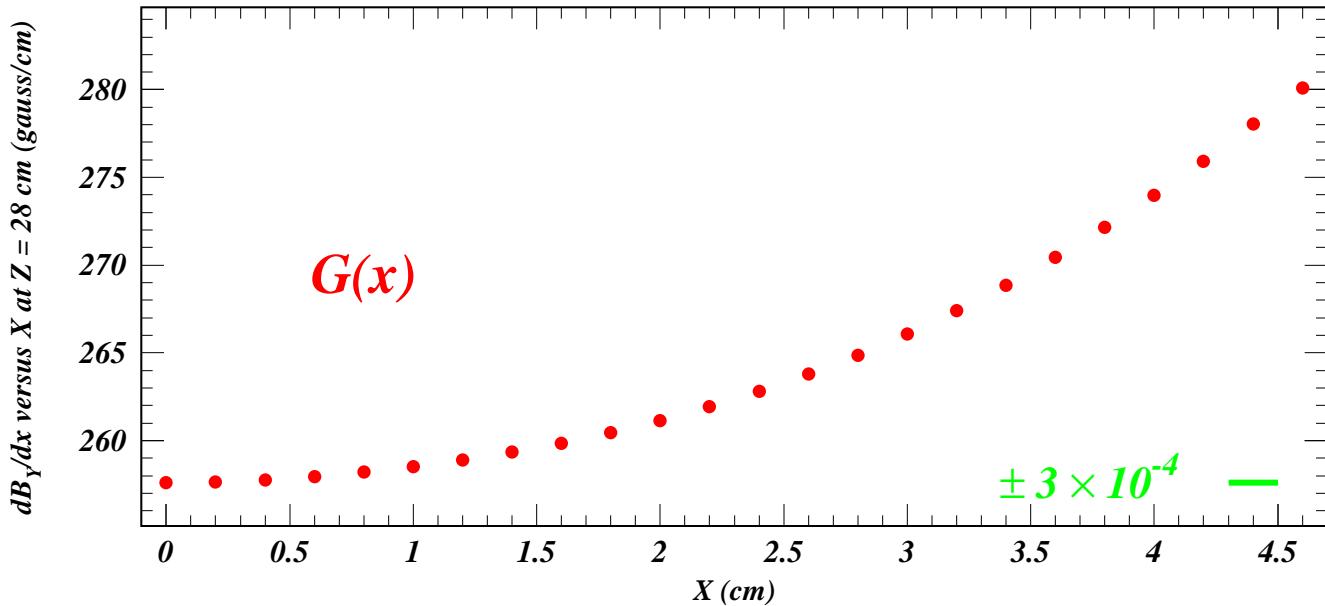
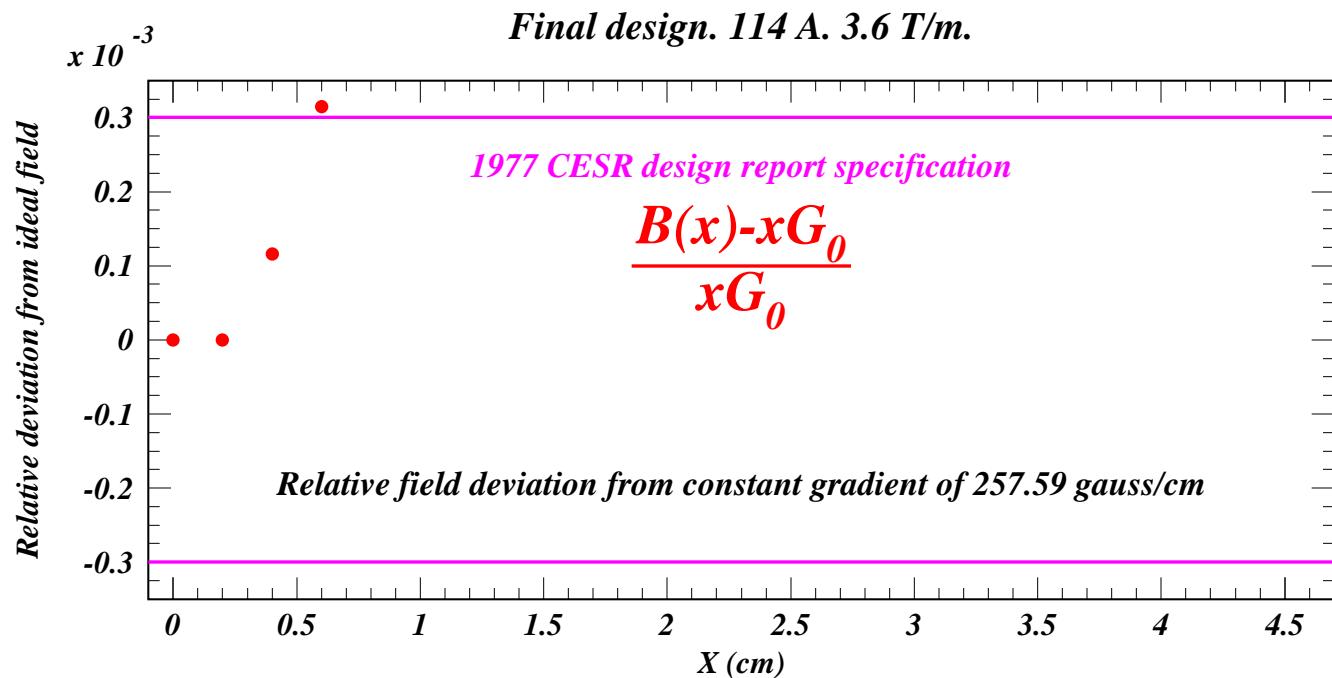
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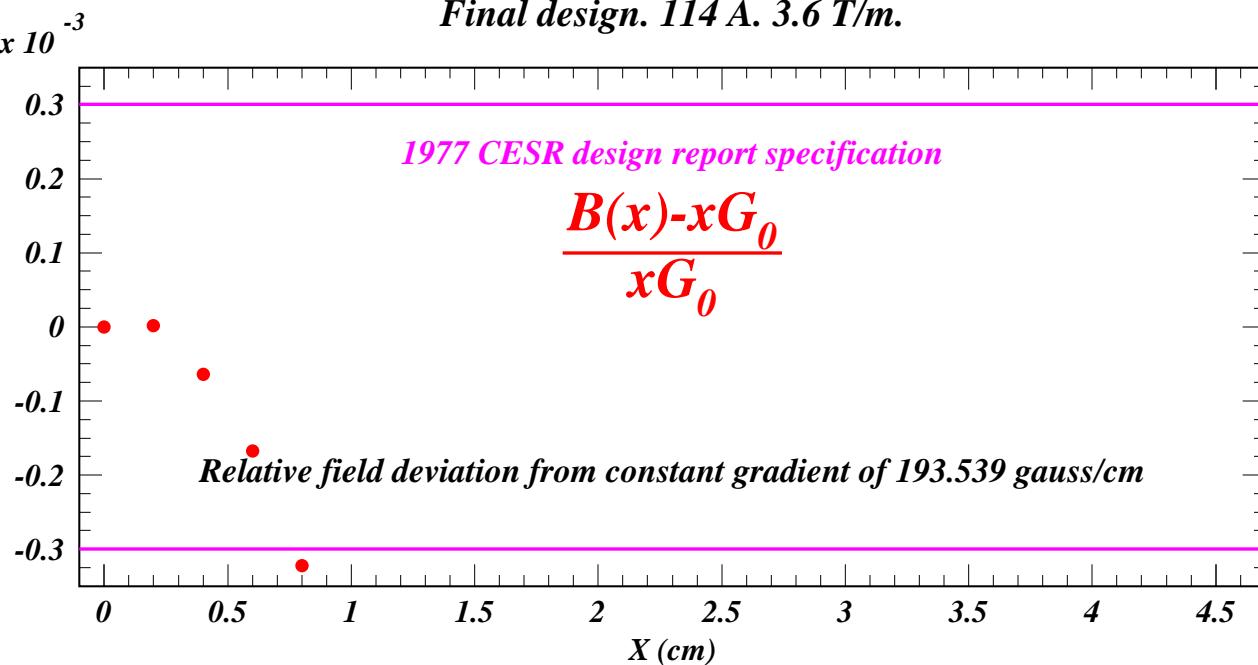
Final design. 114 A. 3.6 T/m.

1977 CESR design report specification

$$\frac{B(x)-xG_0}{xG_0}$$

Relative field deviation from constant gradient of 193.539 gauss/cm

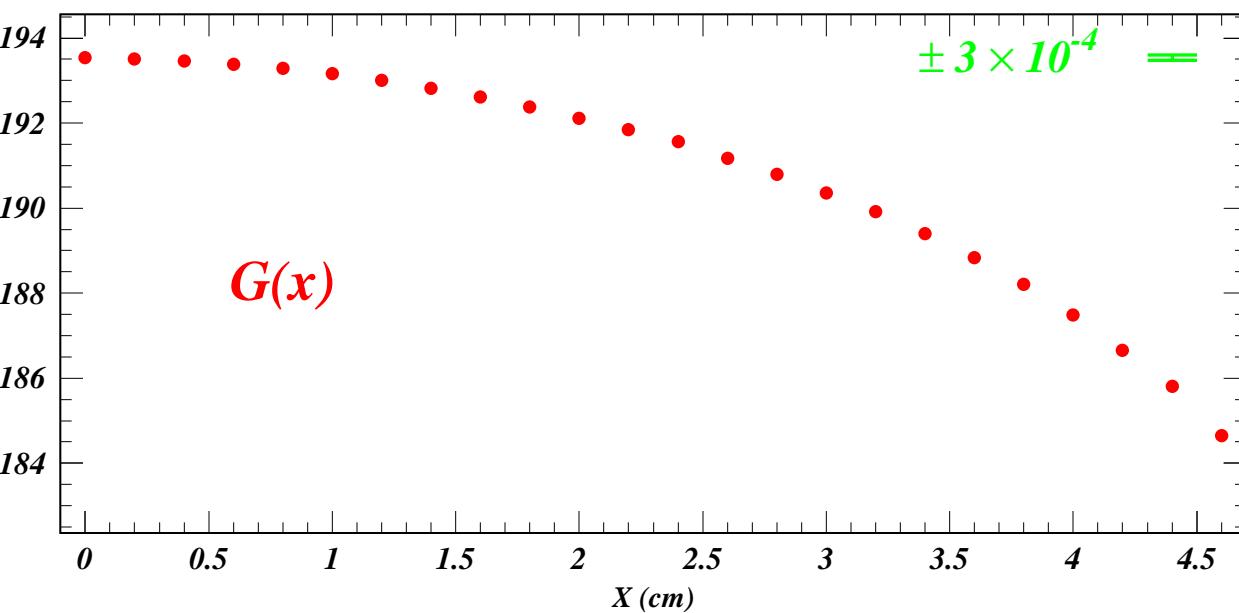
Relative deviation from ideal field



dB_y/dx versus X at $Z = 30$ cm (gauss/cm)

$G(x)$

$\pm 3 \times 10^{-4}$ —



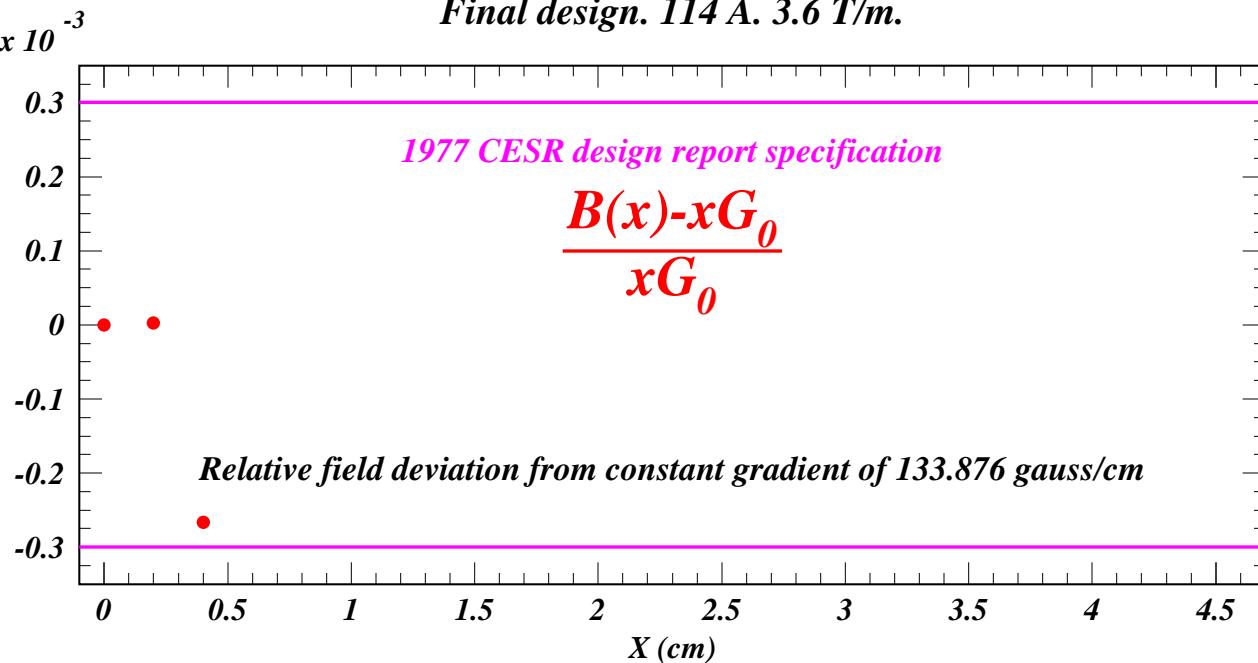
16/09/28 10.26

Final design. 114 A. 3.6 T/m.

1977 CESR design report specification

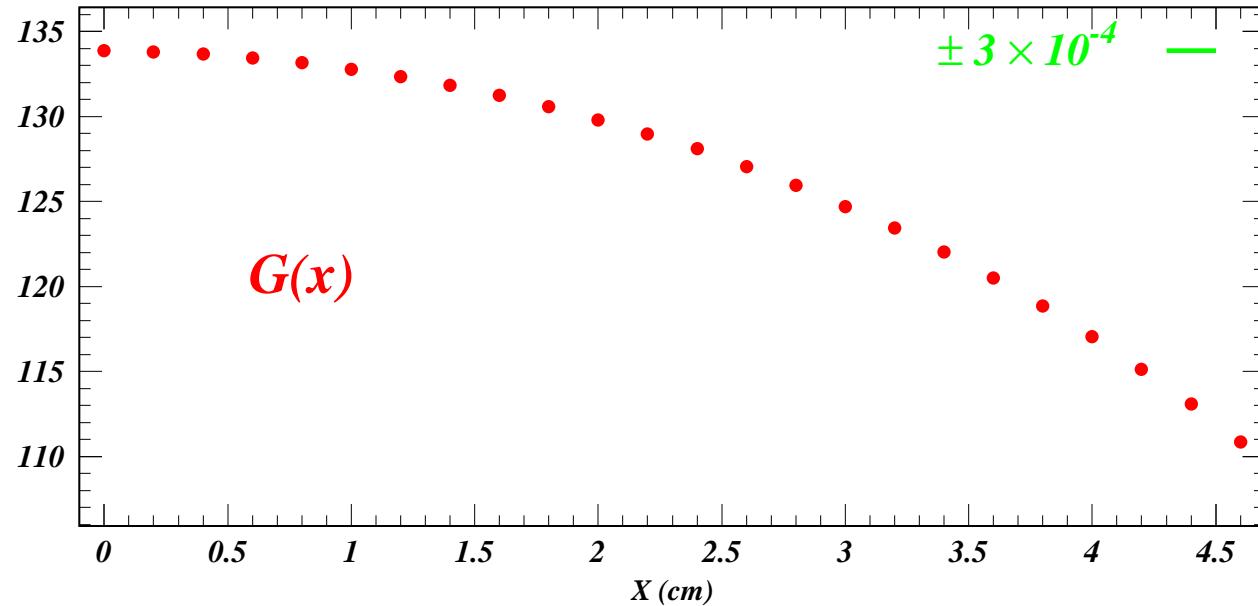
$$\frac{B(x)-xG_0}{xG_0}$$

Relative deviation from ideal field



Relative field deviation from constant gradient of 133.876 gauss/cm

dB_y/dx versus $X = 32$ cm (gauss/cm)



$G(x)$

$\pm 3 \times 10^{-4}$

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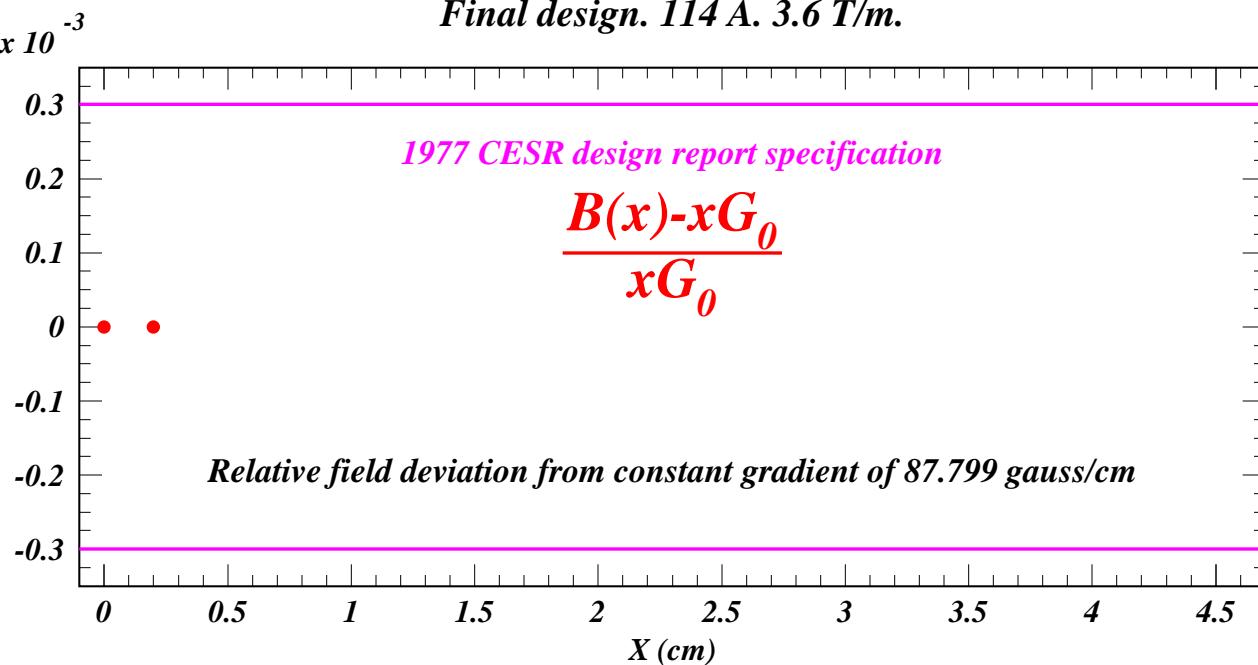
Final design. 114 A. 3.6 T/m.

1977 CESR design report specification

$$\frac{B(x)-xG_0}{xG_0}$$

Relative field deviation from constant gradient of 87.799 gauss/cm

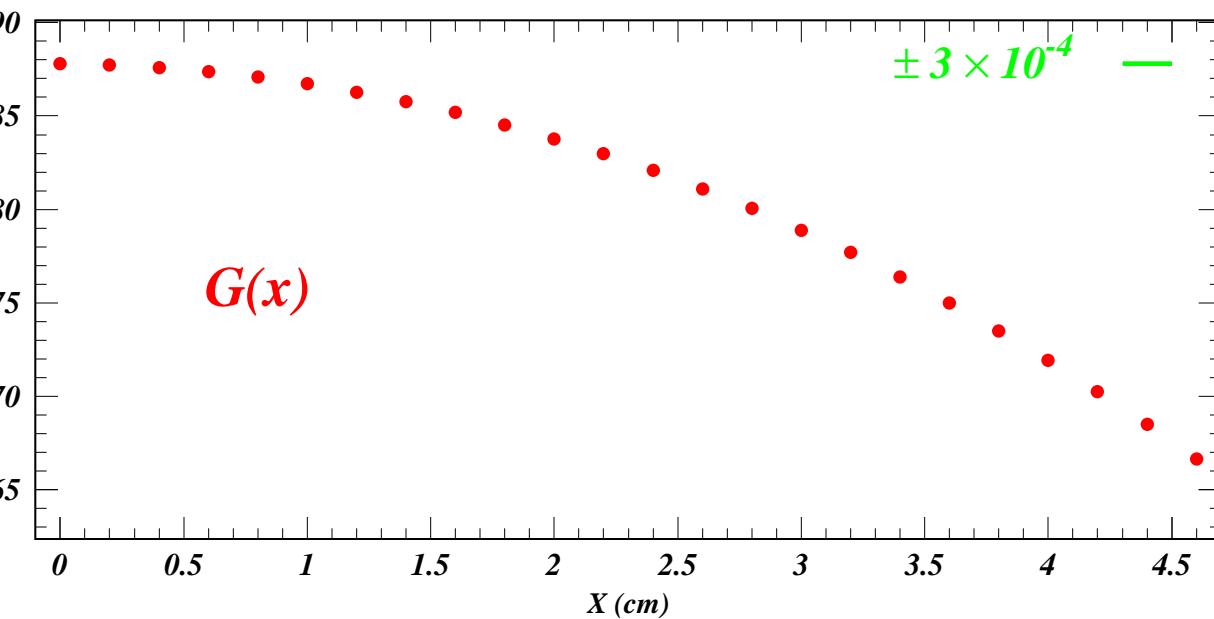
Relative deviation from ideal field



dB_y/dx versus X at $Z = 34$ cm (gauss/cm)

$G(x)$

$\pm 3 \times 10^{-4}$



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Final design. 114 A. 3.6 T/m.

