Vacuum and mechanical design of ILC DR

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Integration design: usual consideration

field	parameter	implication
Beam dynamics	Beam aperture Impedance/wake field BPM	Vacuum chamber aperture, Shape, material, coatings BPM design
SR power	Power, photon reflectivity	SR power absorber design, cooling
Vacuum design	SR induced gas desorption	Pumping scheme, vacuum chamber material, coatings
Fast ions (in e^- DR)	Gas density specification Ion collection	UHV pumping scheme Mechanical design
Mechanical solutions	Mechanical design, component integration, mechanical stability, etc.	Shape, material, supports, cooling, welding, brazing, feedthroughs, etc.
Cost	Cost optimisation	All systems

Integration design: specific problems in e^+ rings

field	parameter	implication
Ion induced pressure instability	Rapid gas density grow Residual gas ionisation Ion energy, ISD yield	Vacuum design: Requires greater pumping speed and low outgassing walls
E-cloud mitigation	PEY (minimising a number of photoelectrons in beam pipe)	Shape, antechamber, SR absorbers, coatings, low photon reflectivity
	SEY (minimising)	Wall material, Coating, Grooves, electrodes
	Residual gas ionisation	UHV pumping scheme
	Electron simulated gas desorption	Low outgassing walls
Mechanical solutions		More complicate integration
Cost	Guaranteed performance at the lowest cost	Challenging

Vacuum required for ILC DRs

- The need to avoid the fast ion instability leads to very demanding specifications for the vacuum in the electron damping ring [Lanfa Wang, private communication]:
  - < 0.5 nTorr CO in the arc cell,
  - < 2 nTorr CO in the wiggler cell and
  - < 0.1 nTorr CO in the straight section
- In the positron damping ring required vacuum level was not specified and assumed as 1 nTorr (common figure for storage rings)

Ideal vacuum chamber for vacuum design

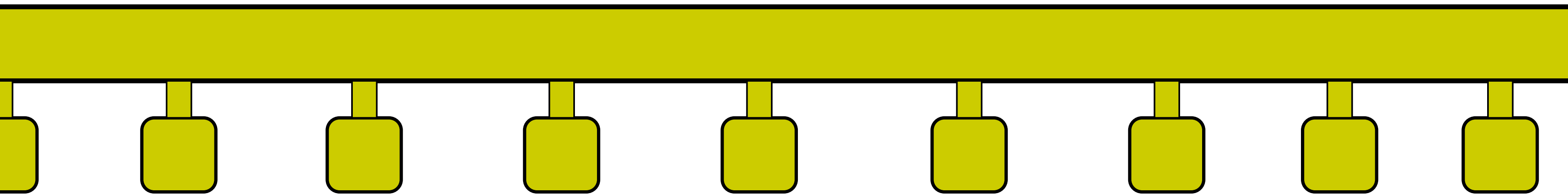
for the electron ring and, where possible, for the positron ring:

- Round or elliptical tube
  - Cheapest from technological point of view
- No antechamber if SR power can absorbed with vacuum chamber wall cooling
  - Beam conditioning is most efficient
  - Easy geometry for NEG coating
- NEG coated
  - Requires less number of pumps with less pumping speed
  - 160°C for NEG coating activation instead of 220-300°C bakeout
  - Choice of vacuum chamber material (stainless steel, copper and aluminium) does not affect vacuum in this case
  - Residual gas CH_4 and H_2 (almost no CO and CO_2)

Pumping scheme along the ILC DR arc

An aluminium tube after bakeout at **220°C** for 24 hrs and 100 Ahr beam conditioning:

- a pump with **S_{eff} = 200 l/s every 5 m**
- H_2, CO and CO_2

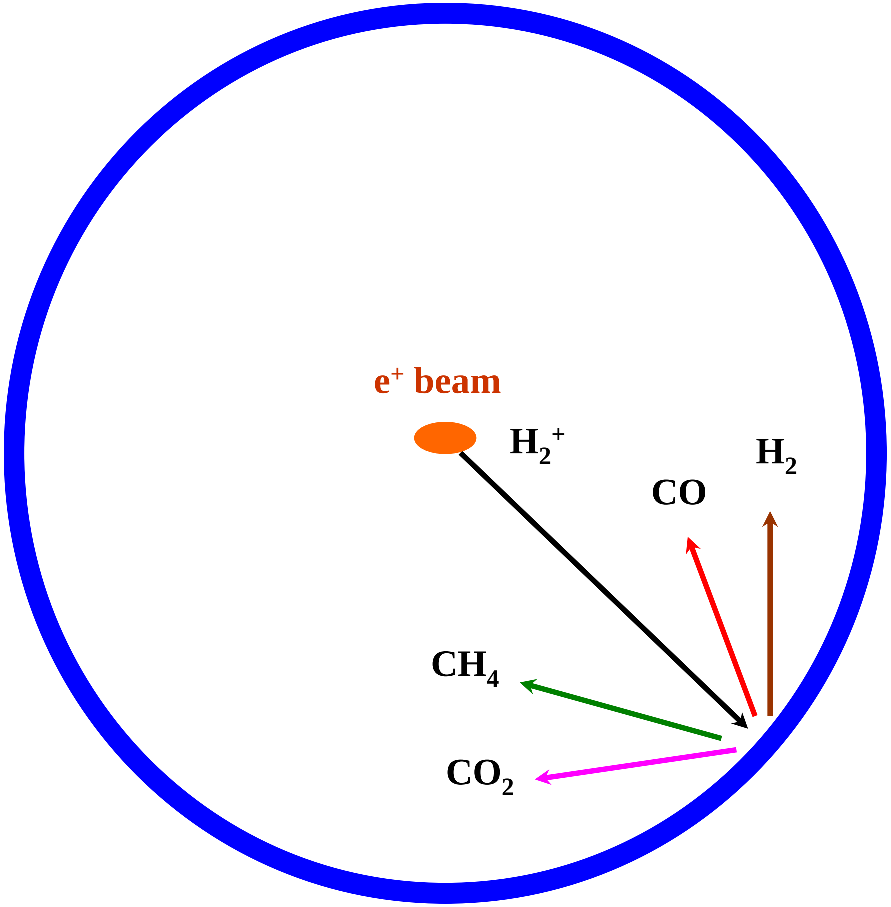


Inside a NEG coated tube after activation at **160°C** for 24 hrs and 100 Ahr beam conditioning: a pump with **S_{eff} = 20 l/s every 30 m**

- H_2 and CH_4

O. Malyshev. Vacuum Systems for the ILC Damping Rings. EUROTeV Report-2006-094.

Ion induced pressure instability in ILC positron DR



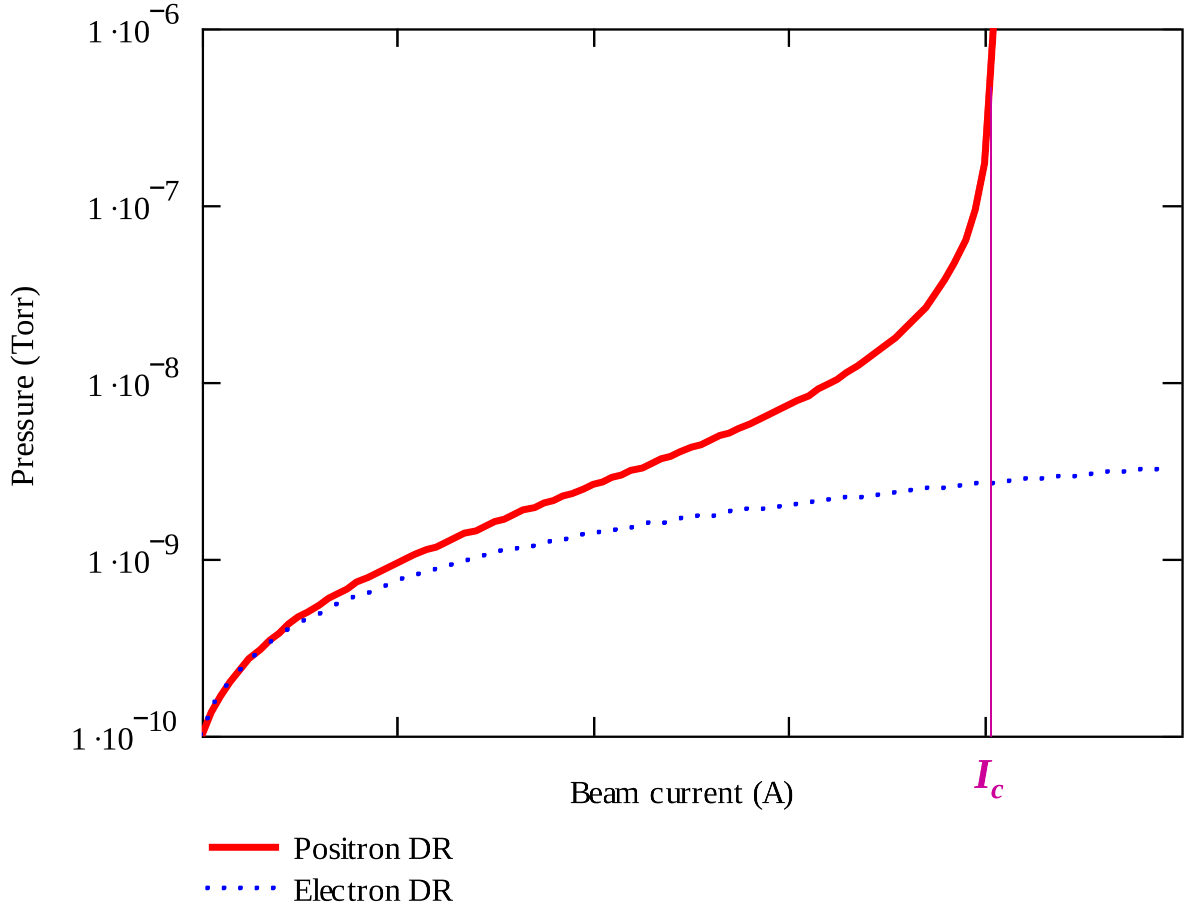
$$P = \frac{Q}{S_{eff} - \chi \frac{\sigma I}{e}}$$

where
Q = gas desorption,
S_{eff} = effective pumping speed,
χ = ion induced desorption yield
σ = ionisation cross section,
I = beam current.

$$\chi = f\left(E_{ion}, M_{ion}, material, bakeout, ...\right)$$

$$E_{ion} = f\left(N_{bunch}, \tau, T, \sigma_x, \sigma_y, ...\right)$$

Critical current



Critical current, I_c, is a current when pressure (or gas density) increases dramatically.

Mathematically, if

$$P = \frac{Q}{S_{eff} - \chi \frac{\sigma I}{e}}$$

when $S_{eff} > \chi \frac{\sigma I}{e}$

Hence $I < I_c$,

where $I_c = \frac{S_{eff} e}{\chi \sigma I}$

The ion stability for different vacuum chamber materials, I_{max}=0.4 A

Vacuum chamber	I_c, (A)	I_c / I_{max}	Domin. gas	Stable or not
Distance between pumps L = 6 m, ID = 50 mm				
316LN	1.0	2.5	CO	Yes
Pure Al	0.5	1.25	CO	No
Ti alloy	1.1	2.8	CO	Yes
Distance between pumps L = 6 m, ID = 60 mm				
316LN	1.24	3.1	CO	Yes
Pure Al	0.64	1.6	CO	No
Ti alloy	1.4	3.5	CO	Yes
Distance between pumps L = 10 m, ID = 50 mm				
316LN	0.47	1.2	CO	No
Pure Al	0.24	0.6	CO	No
Ti alloy	0.53	1.3	CO	No
Distance between pumps L = 40 m, ID = 50 mm				
NEG coated	5	12.5	CH_4	Yes

Pressure instability conclusions:

- Ion energy = ~300 eV, but could be larger for a smaller beam
- For given parameters and large uncertainties, there is a possibility of ion induced pressure increase and even ion induced pressure instability in positron damping ring if pumping is insufficient.
- **Use of NEG coating fully eliminates the probability of the ion induced pressure instability.**

O.B. Malyshev. Study of Ion Induced Pressure Instability in the ILC Positron Damping ring. EUROTeV Report-2008-058.

Electron cloud

- Three sources of electrons:
  - Photoelectrons
  - Secondary electrons
  - Gas ionisation

Photoelectrons

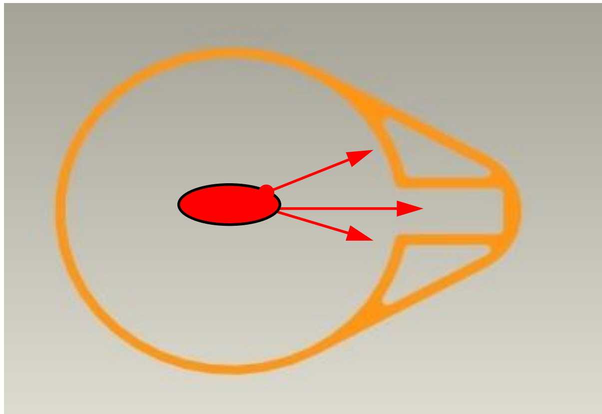
- Photoelectrons:

  PEY = κ F Γ R, where Γ is a total SR flux.

  - A photon flux absorbed in beam chamber can be minimised with an antechamber, F is an antechamber efficiency

  - Lower photon reflectivity, R, helps as well

  - Choice of material, surface treatment, conditioning, coating (ex.: **TiZrV**) allows to reduce photo-electron emission yield, κ



O.B. Malyshev and W. Bruns. ILC DR vacuum design and e-cloud. Proc. of EPAC08, p.673,

and references with in the paper.

PEY for different types of vacuum chamber

Beam pipe	Inside magnets, $B \neq 0$		Downstream straights near the magnet, $B = 0$		
	Tube	Antechamber	Tube	Solenoid	Antechamber
Estimated achievable PEY					
Dipole SR	$3\cdot10^{-4}$– 0.065	$\mathbf{3\cdot10^{-6}}$– $6.5\cdot10^{-3}$	0.01–0.1	0.01–0.1	10^{-4}– 0.01
Wiggler SR	$3\cdot10^{-3}$ – 0.65	$\mathbf{3\cdot10^{-5}}$– $6.5\cdot10^{-2}$	0.1–1	0.1–1	10^{-3}– 0.1
Required maximum PEY from e-cloud modelling					
Dipole	$\sim10^{-4}$		?		
Wiggler	$\sim10^{-4}$		?		

Secondary electrons

- Secondary electron yields, e-cloud and mitigation techniques are intensively studied in many places, see all other talks on this session.
- Secondary electron
  - Choice of material (intrinsic SEY for flat and dense surface)
  - Surface treatment to modify surface micro-structure (air bake, anodisation, ion bombardment, etc.)
  - Low SEY coatings: material *and* its surface micro-structure: **TiZrV or TiN or Amorphous C coatings**
  - Geometrical electron traps (ex.: grooves)
  - Field suppression:
    - Magnetic material coatings
    - Biased electrodes
    - Solenoid field

Gas ionisation

- Ionisation cross section of heavy molecules is higher:
  - $\sigma(CO_2)=12\,\sigma(H_2)$
- Ionisation in ILC DR can be neglected when CO pressure is below 10^{-8} Torr
  - Surface treatment and conditioning
  - Low outgassing coating (ex.: **TiZrV** coating)
  - Better pumping (ex.: **TiZrV** coating or more pumps)

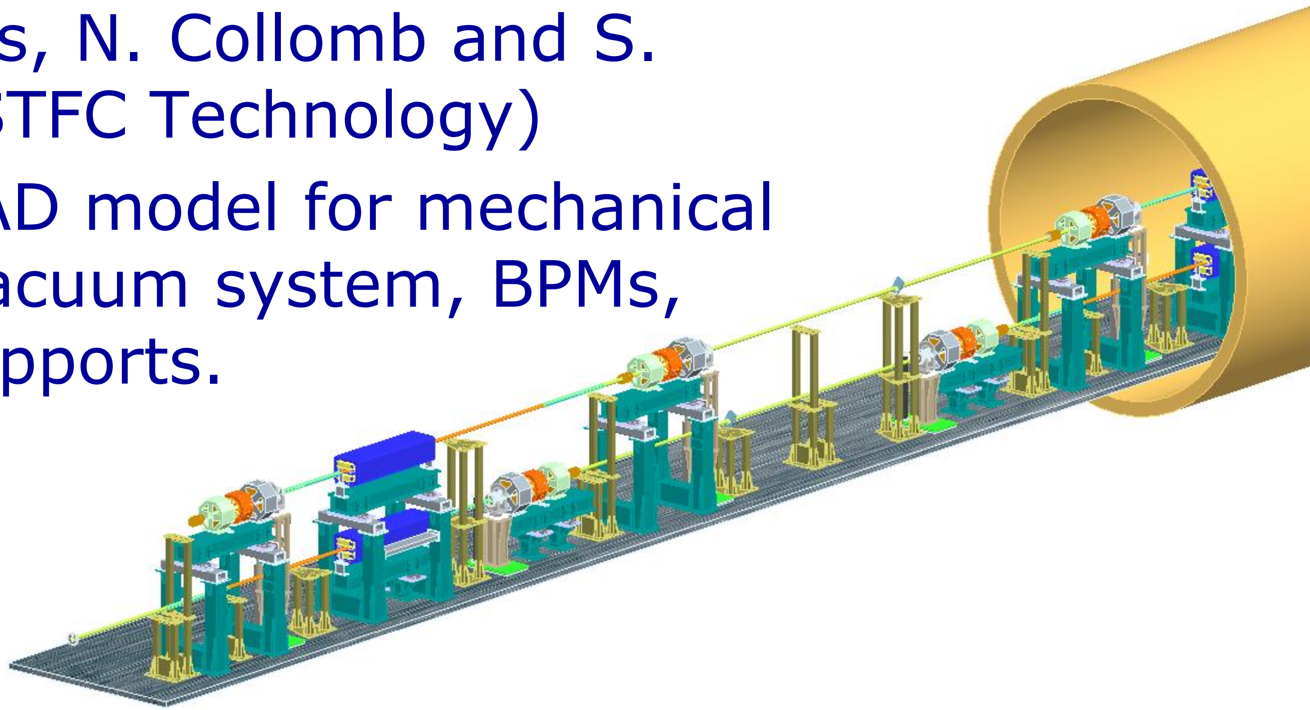
O.B. Malyshev and W. Bruns. ILC DR vacuum design and e-cloud. Proc. of EPAC08, p.673.

Selecting an e-cloud mitigation

- A complex solution required:
  - Good solution against Photo-electrons or Secondary electrons might lead to higher gas density and higher gas ionisation, and vice versa, best pumping solution might compromise PEY and SEY mitigation.
  - NEG coating is the best choice for UHV systems.
  - NEG coating + grooves might be sufficient in many places
  - Using other coatings and other mitigation techniques increases a cost of DR and should be only used where it is essential.

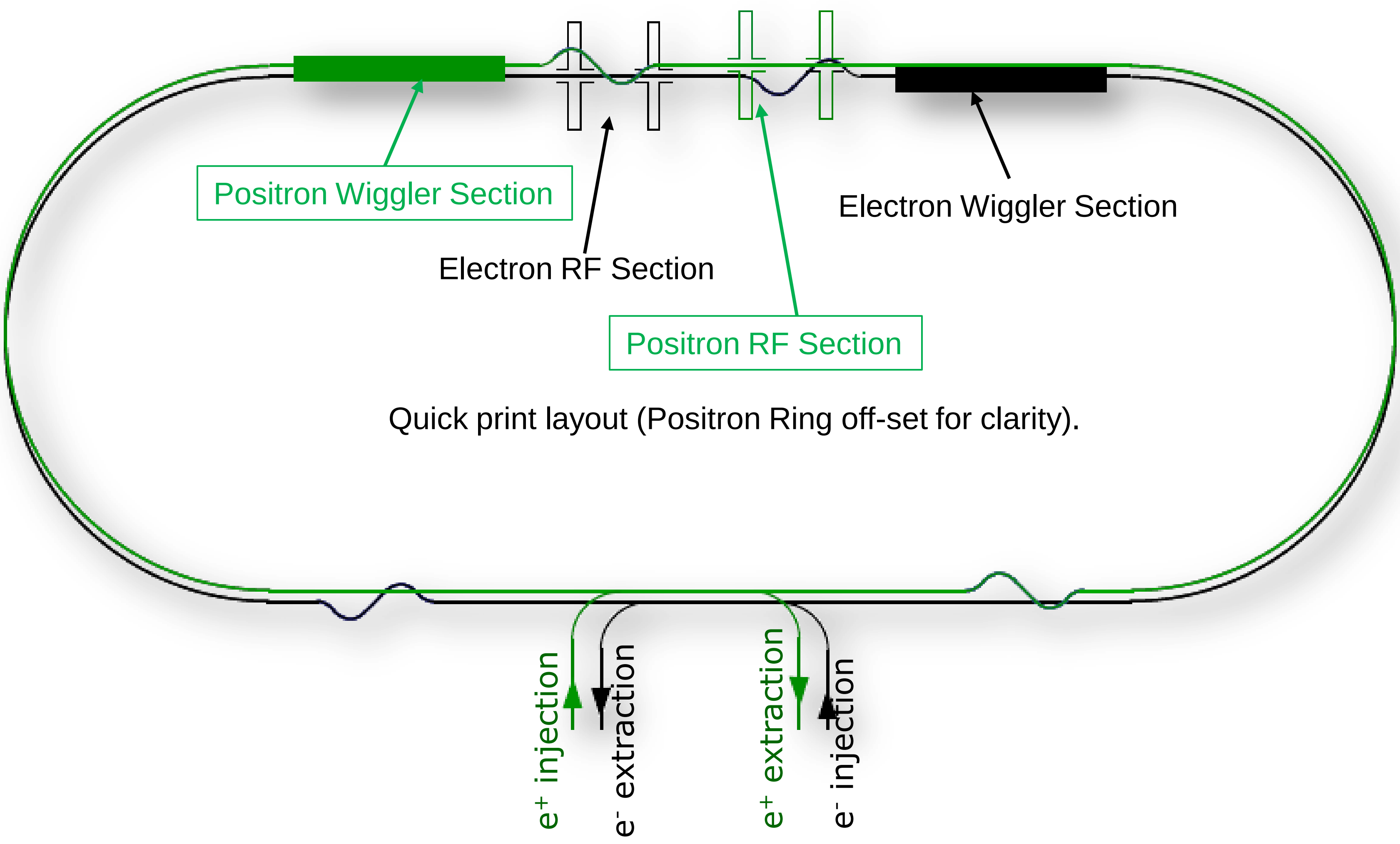
Engineering Model

- Work by J. Lucas, N. Collomb and S. Postlethwaite (STFC Technology)
- Developing a CAD model for mechanical integration of vacuum system, BPMs, magnets and supports.

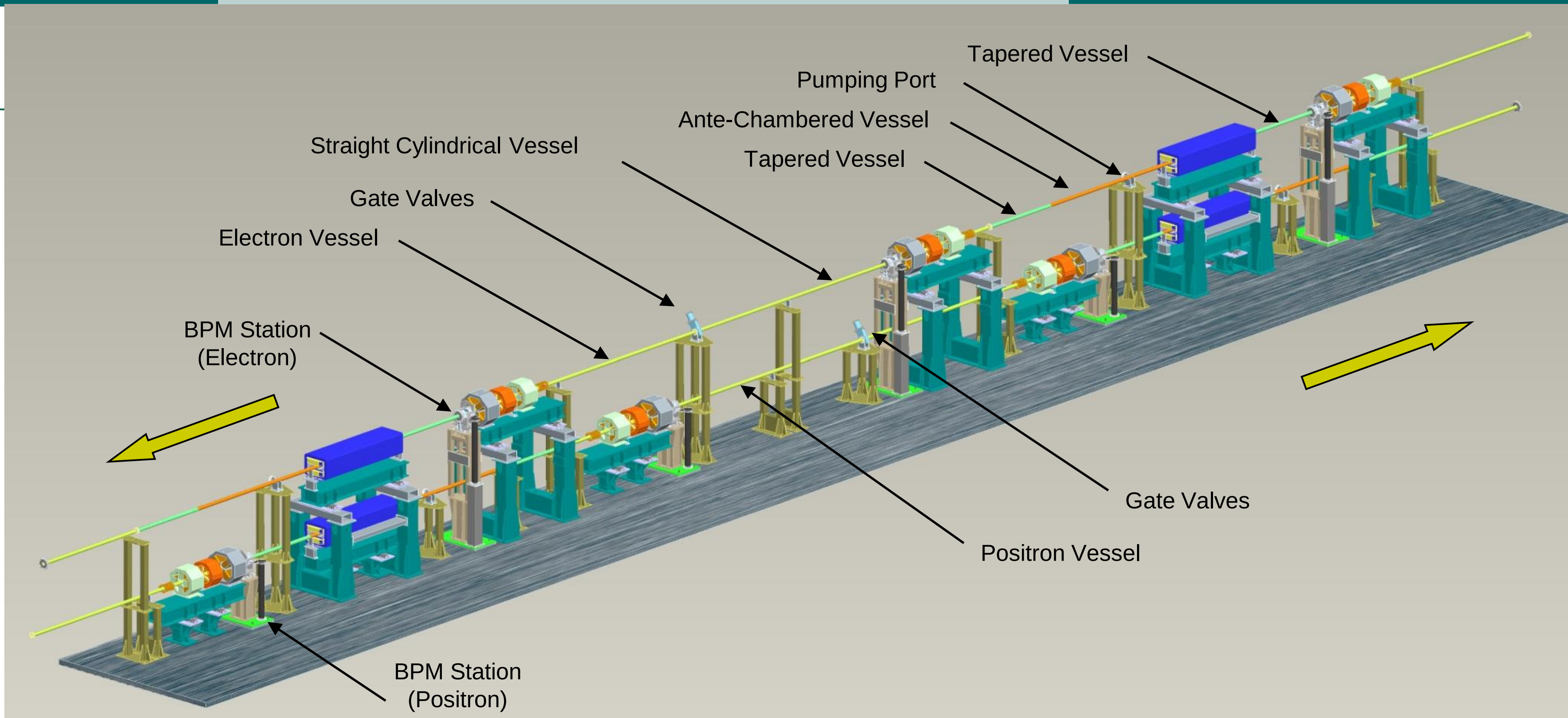


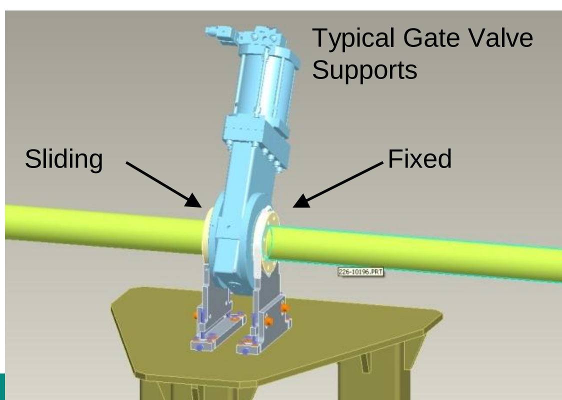
- Goals:
  - to demonstrate engineering feasibility of both the Electron & Positron Damping Ring Periodic Arc Cells;
  - to provide a basis for further design and beam
  - dynamics studies and costing of vacuum, magnets, conventional facilities, etc.

DC04 Overall Layout (simplified)



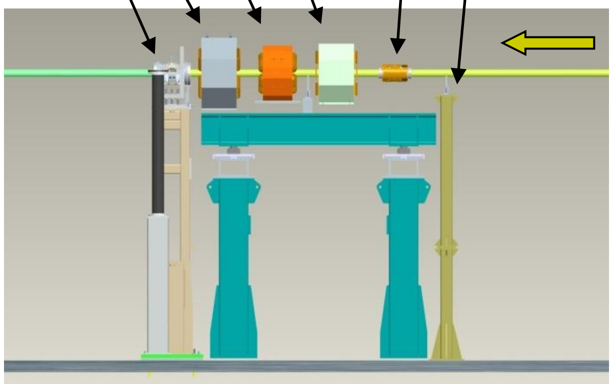
Arc Cell Components



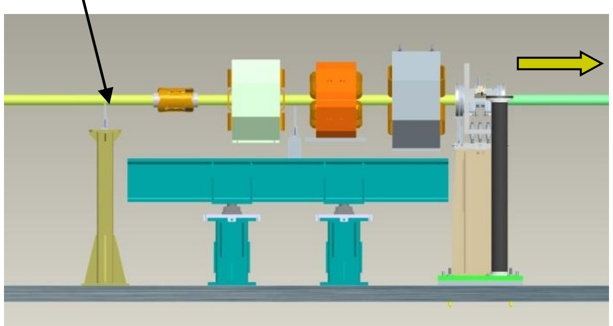


- Work has focused on developing the model for a Single Arc Cell (Linear)
- One Gate Valve per 5 Arc Cells
- Gate Valve supports consist of one fixed and one sliding
- Bellows allow for 4.5 mm/meter thermal expansion (NEG activation at 160-180°C).

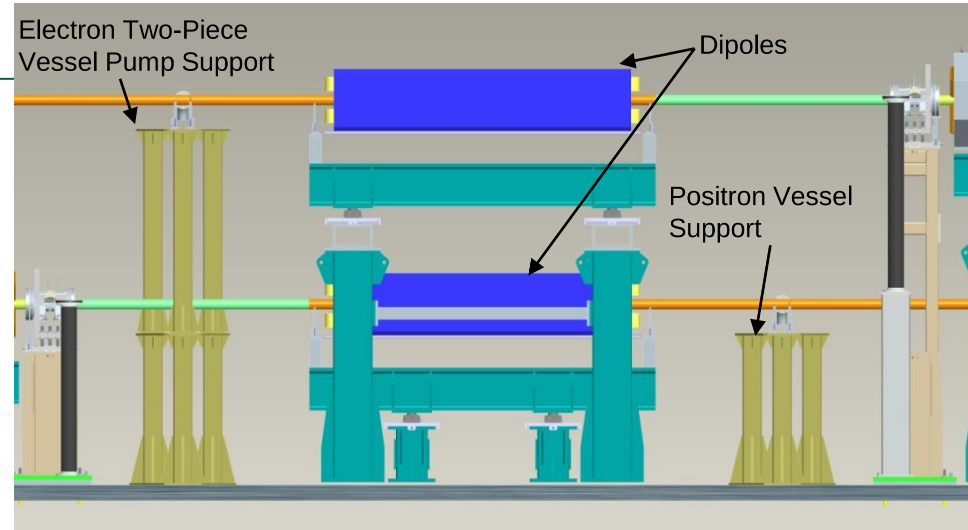
Arc Cell Components Cont'd



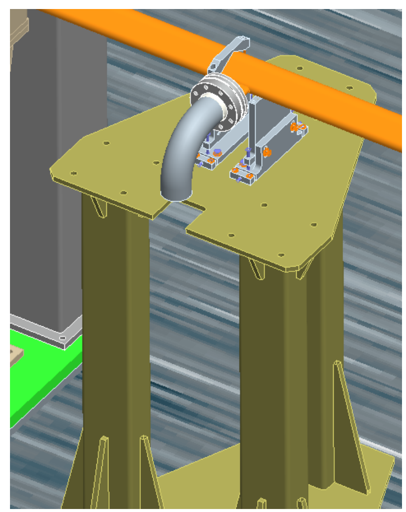
Magnet & Supports – (Electron)

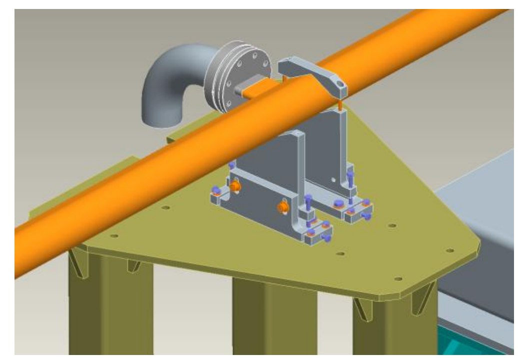


Magnet & Supports



Dipoles & Supports



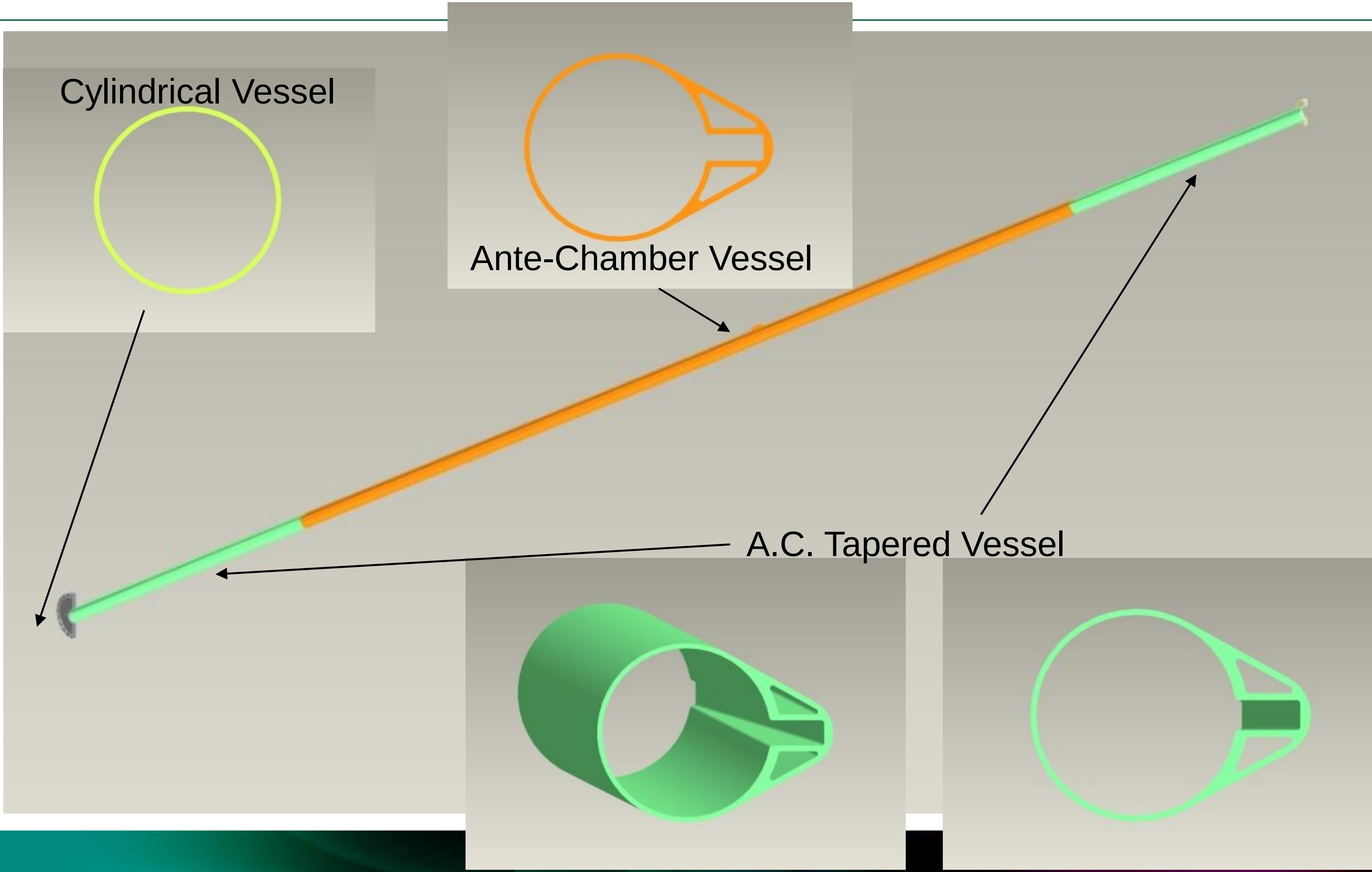


Vessel Pumping Supports

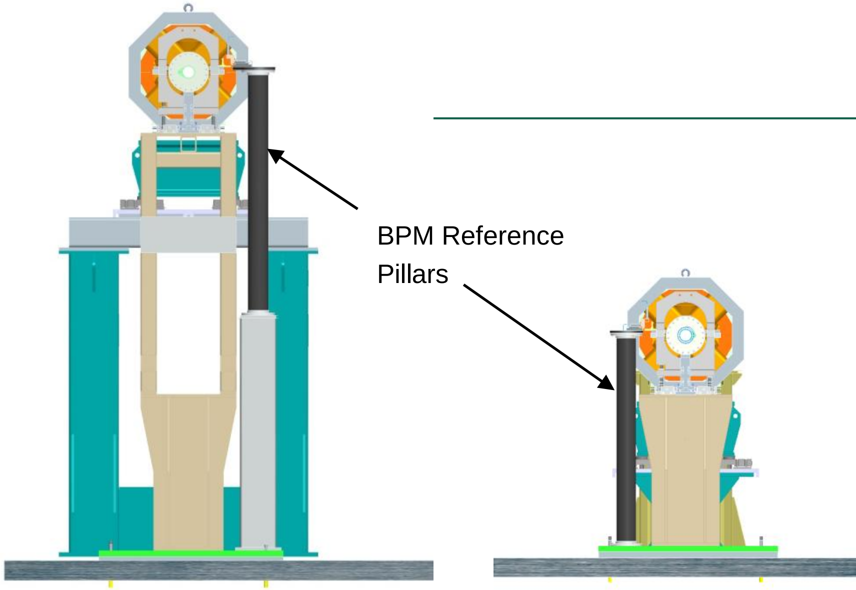
Vacuum system: key features

- Vacuum chamber mostly consists of straight cylindrical tube.
  - Internal diameter 60 mm, wall thickness 2 mm.
- Antechamber and cooling provided in dipoles and a few meters downstream.
  - Intended to reduce build-up of electron cloud by reducing the number of photons in the beam chamber.
  - Dipole chamber will consist of extruded vessel with antechamber, welded to machined "taper" sections.
  - A pumping port is included in antechamber downstream of dipole.
- All vacuum chambers are NEG coated

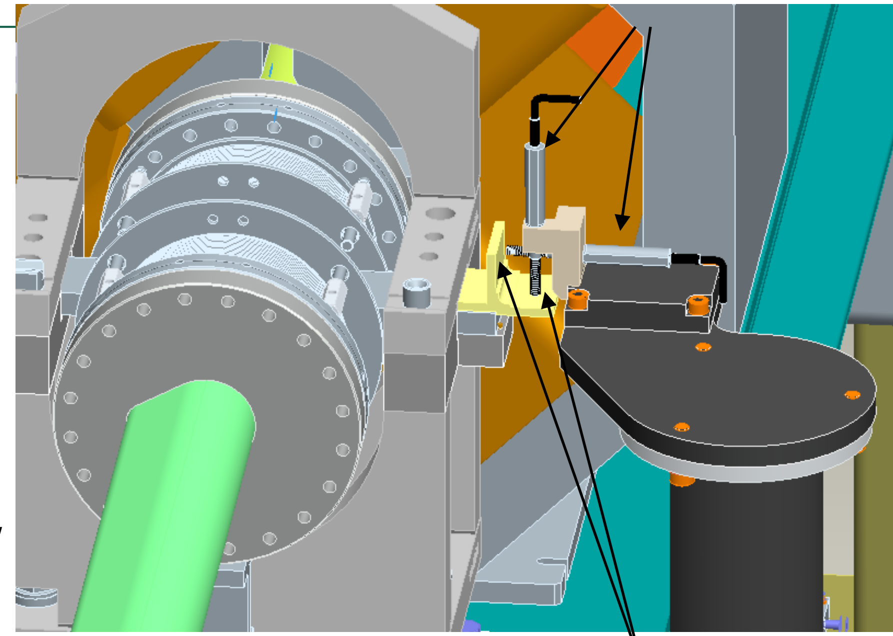
Vacuum Vessel Profiles



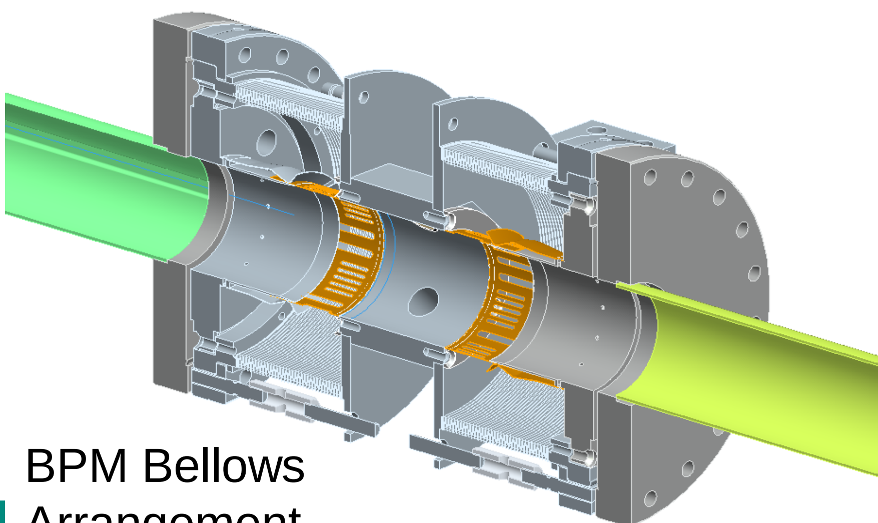
Vacuum Vessel BPM Stations



Electron End View   Positron End View



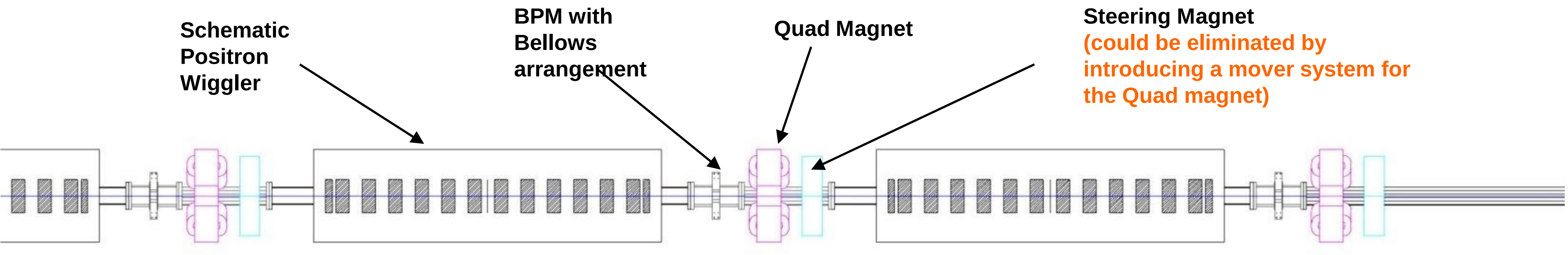
Position Encoders



BPM Bellows Arrangement

- Fitted on all BPM Blocks
- Reference Pillar provides reference points for the beam orbit.
- Position Encoders monitor any motion of BPMs from thermal or mech effects

DC04 Wiggler Section



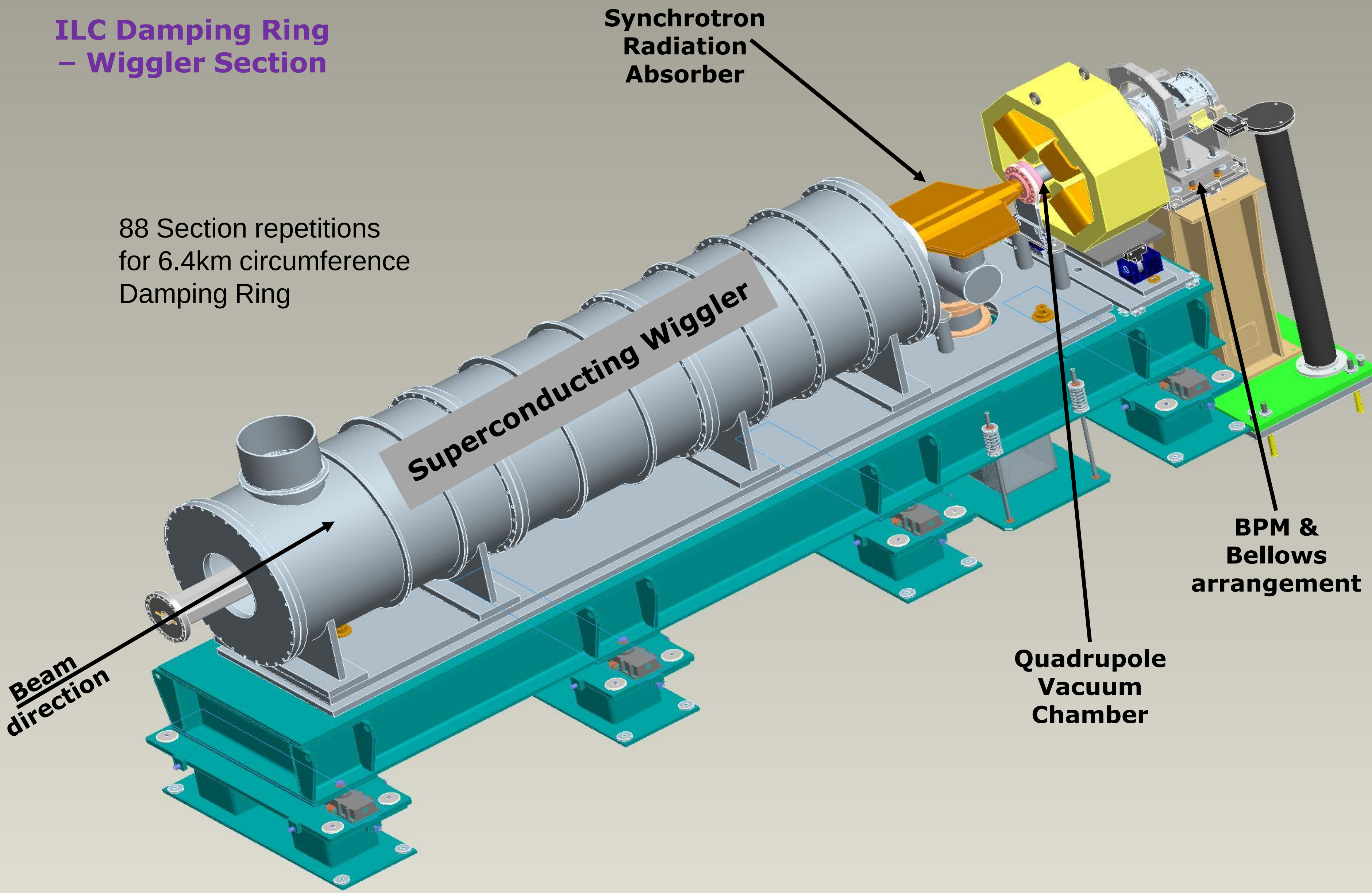
Challenges in a wiggler section design:

- SR power absorption – up to ~40 kW per wiggler
  - Power dissipation calculation by K. Zolotarev (BINP)
- Minimising a number of SR photons hitting beam chamber inside a wiggler to provide low PEY
  - Antechamber and shadow
- Grooved top and bottom and TiN coating to provide low SEY
- Sufficient pimping (NEG strips + SIPs)
- Impedance calculation by M. Korostelev (CI and Liverpool University)

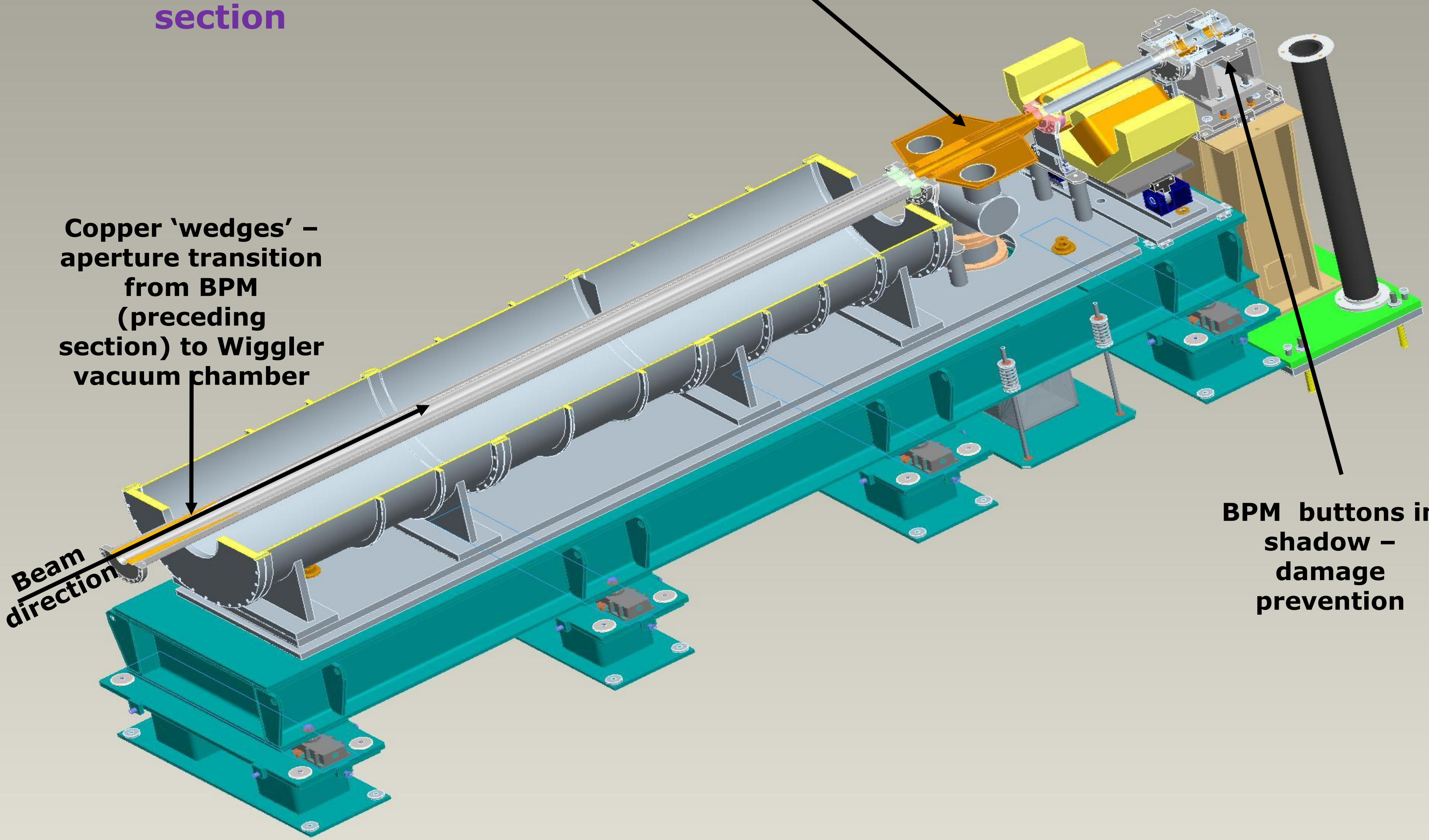
Big thank to Cornell and LBNL for their information on the CESR-TA wiggler design.

ILC Damping Ring – Wiggler Section

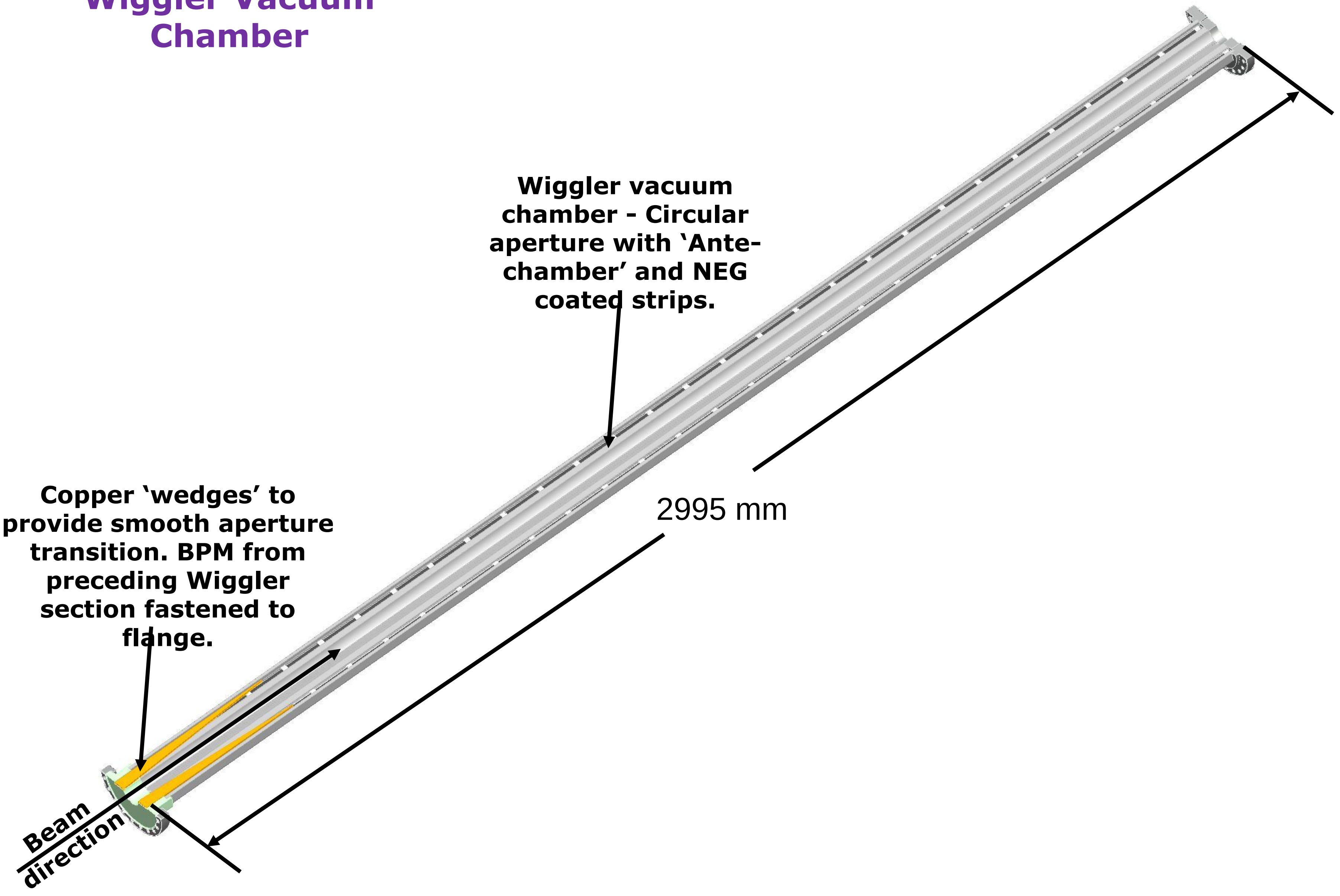
88 Section repetitions for 6.4km circumference Damping Ring



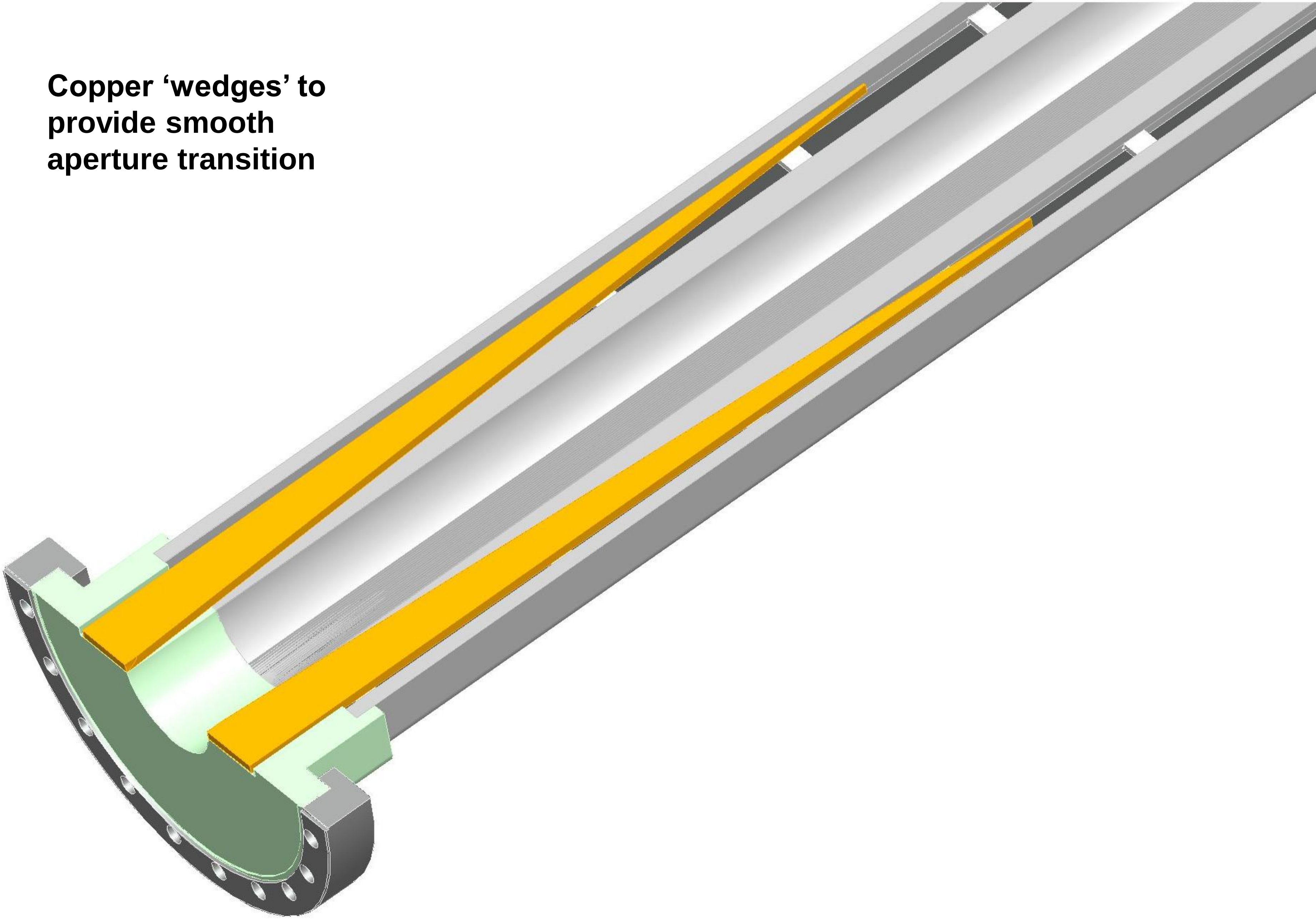
ILC Damping Ring - Wiggler Section - Vacuum Chamber cross-section



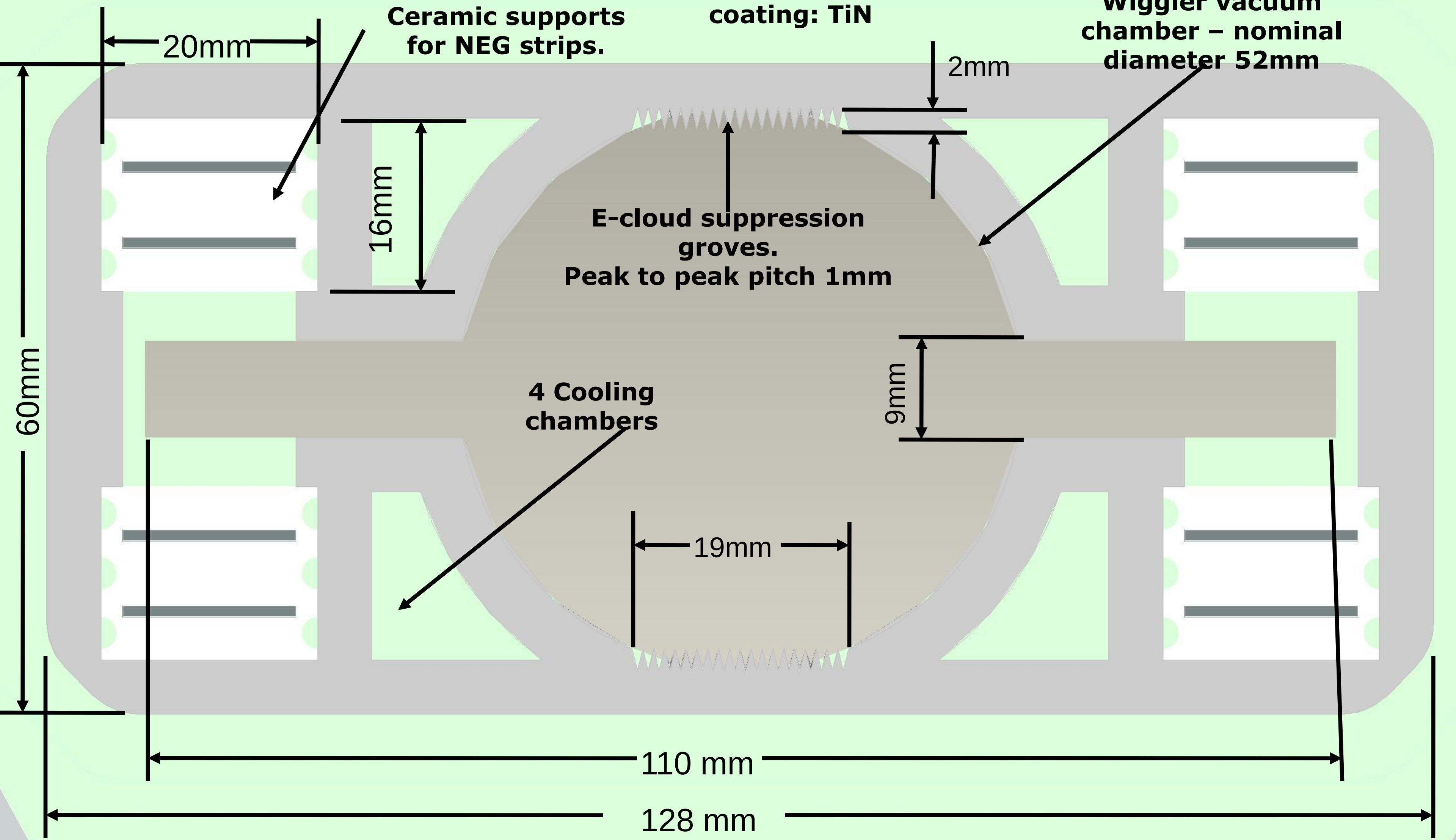
ILC Damping Ring – Wiggler Vacuum Chamber



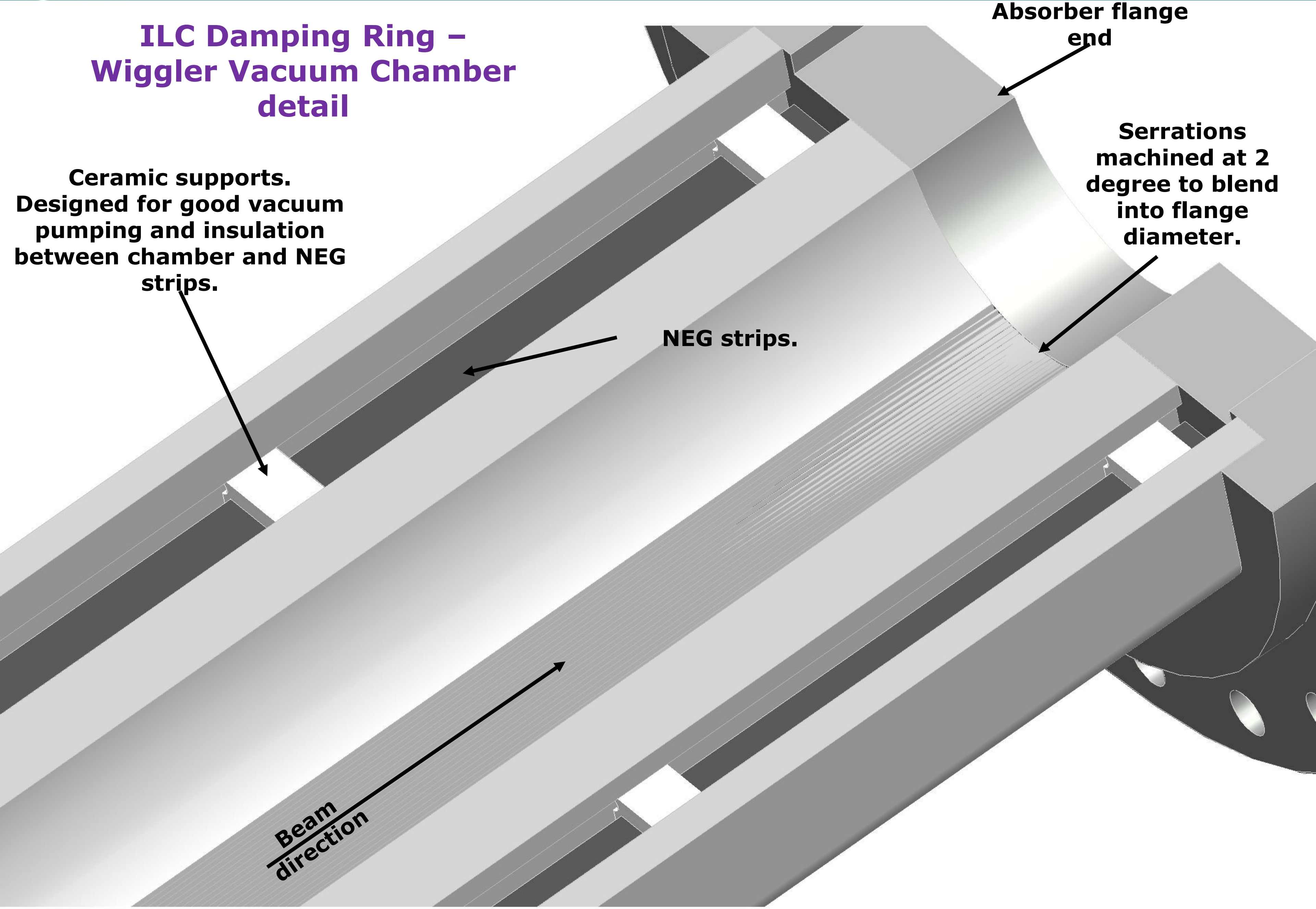
Copper ‘wedges’ to provide smooth aperture transition

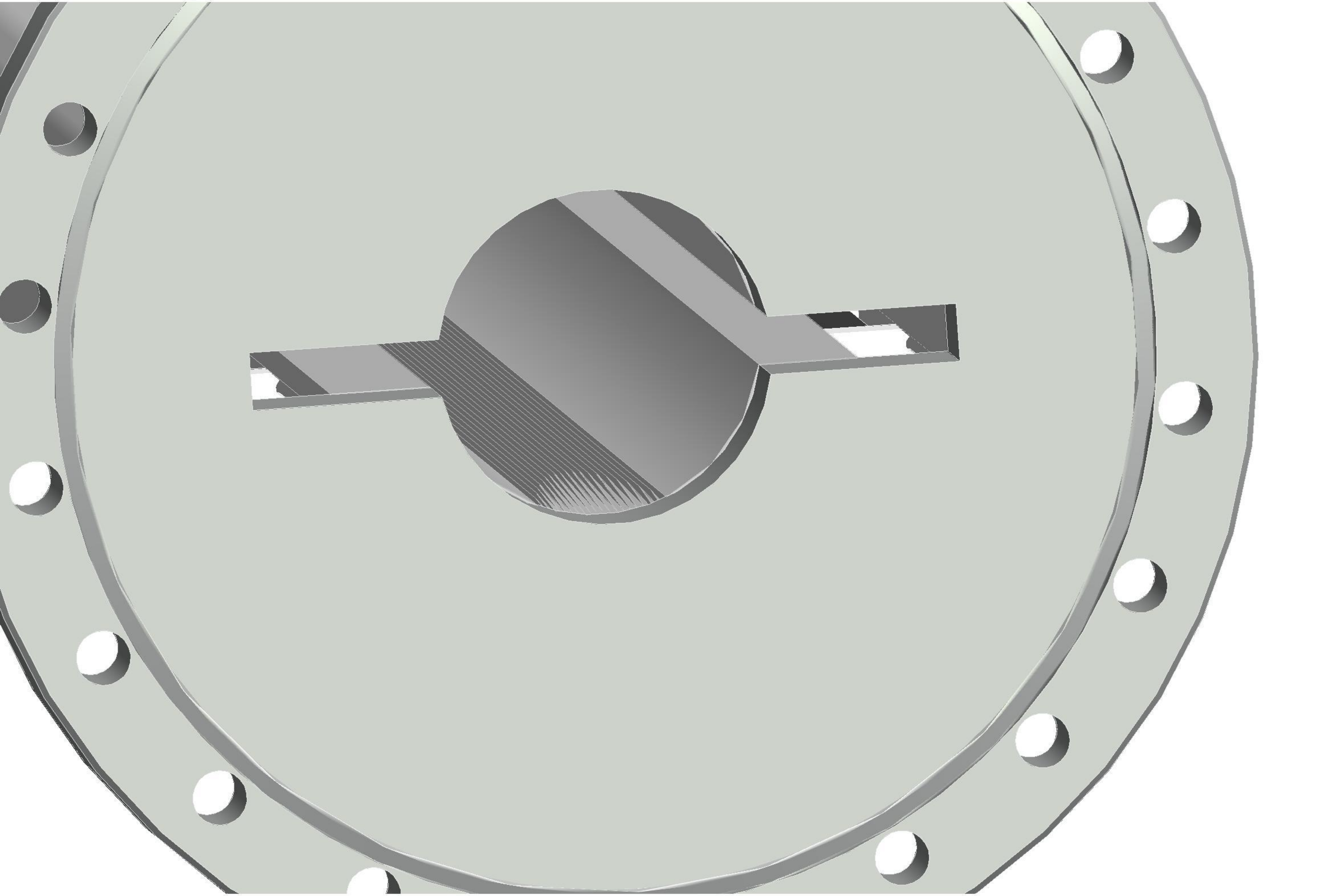


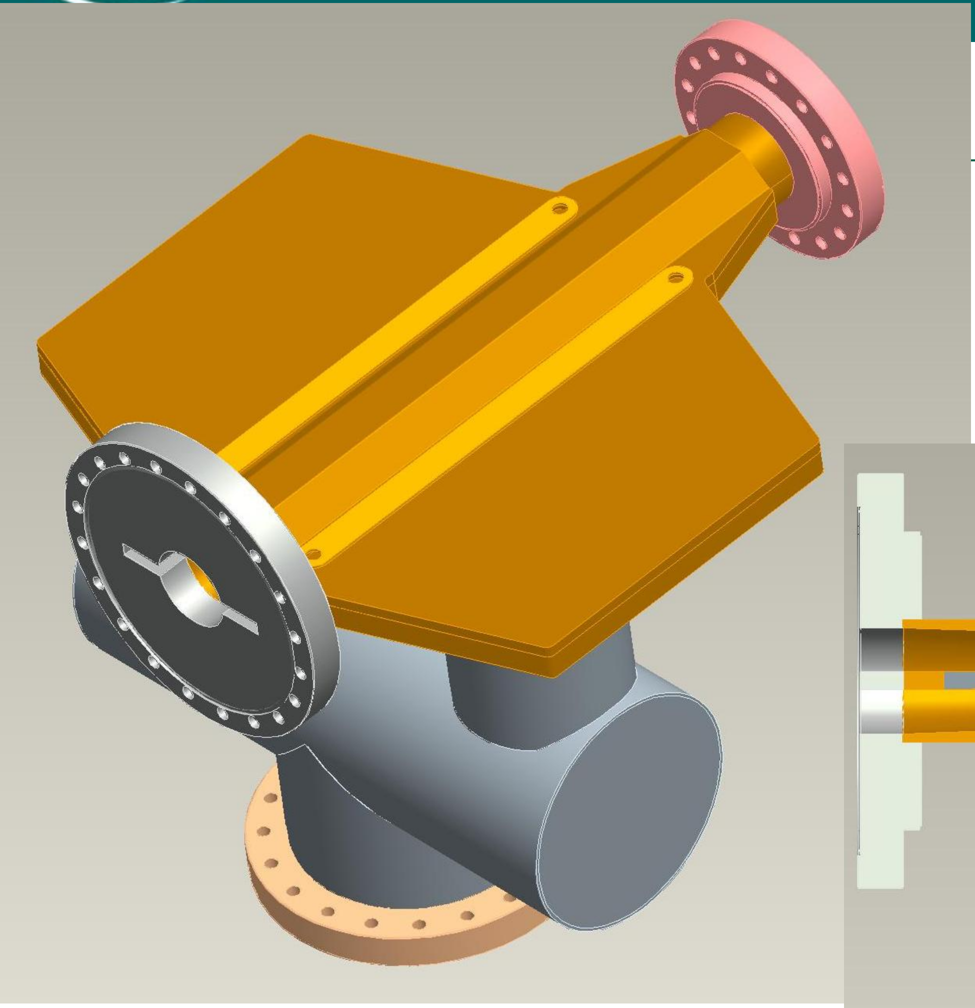
ILC Damping Ring – Wiggler Vacuum Chamber detail



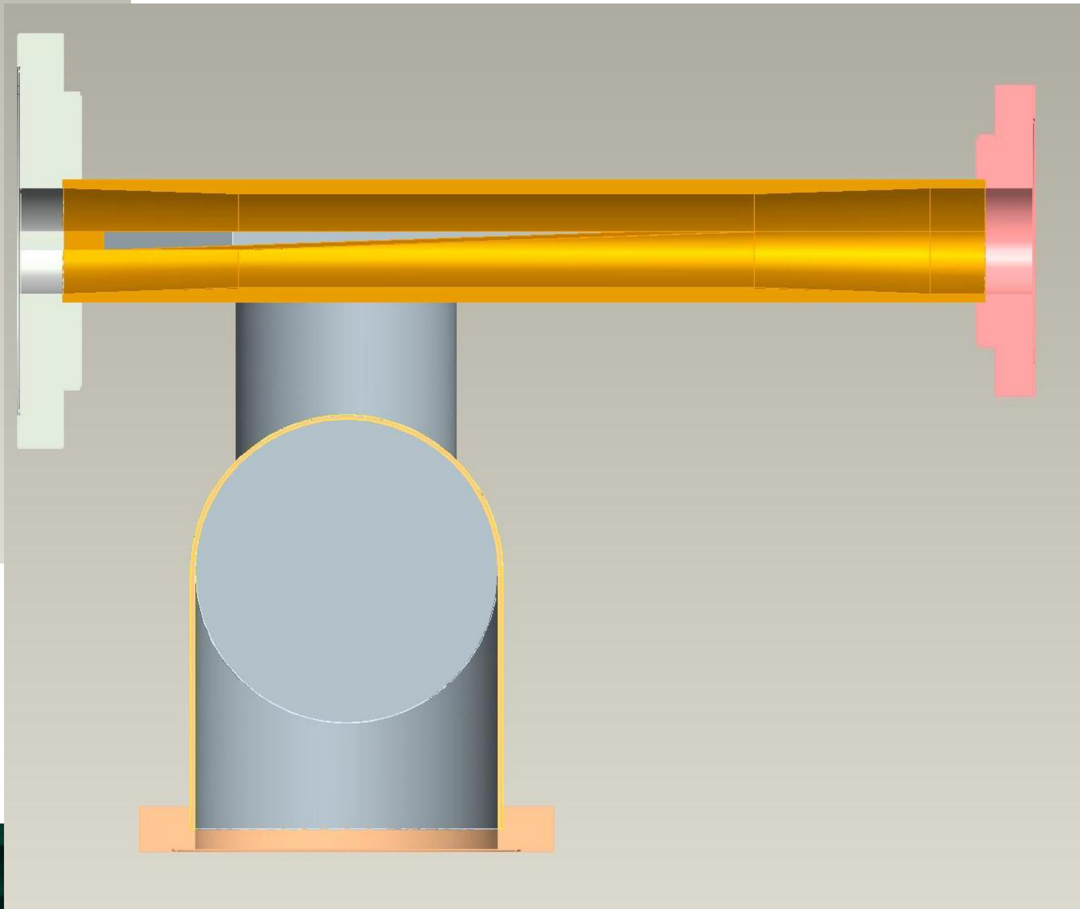
ILC Damping Ring – Wiggler Vacuum Chamber detail



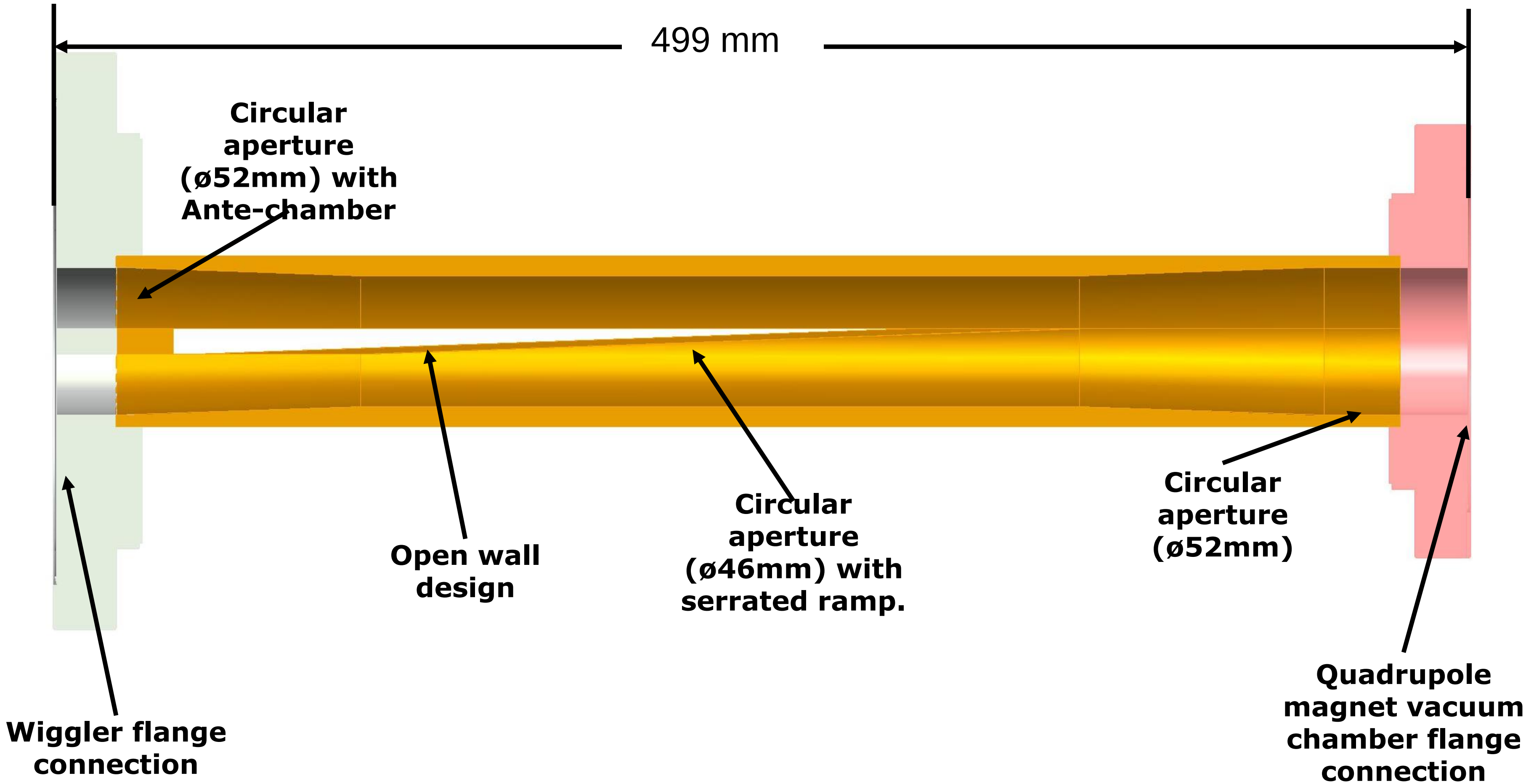




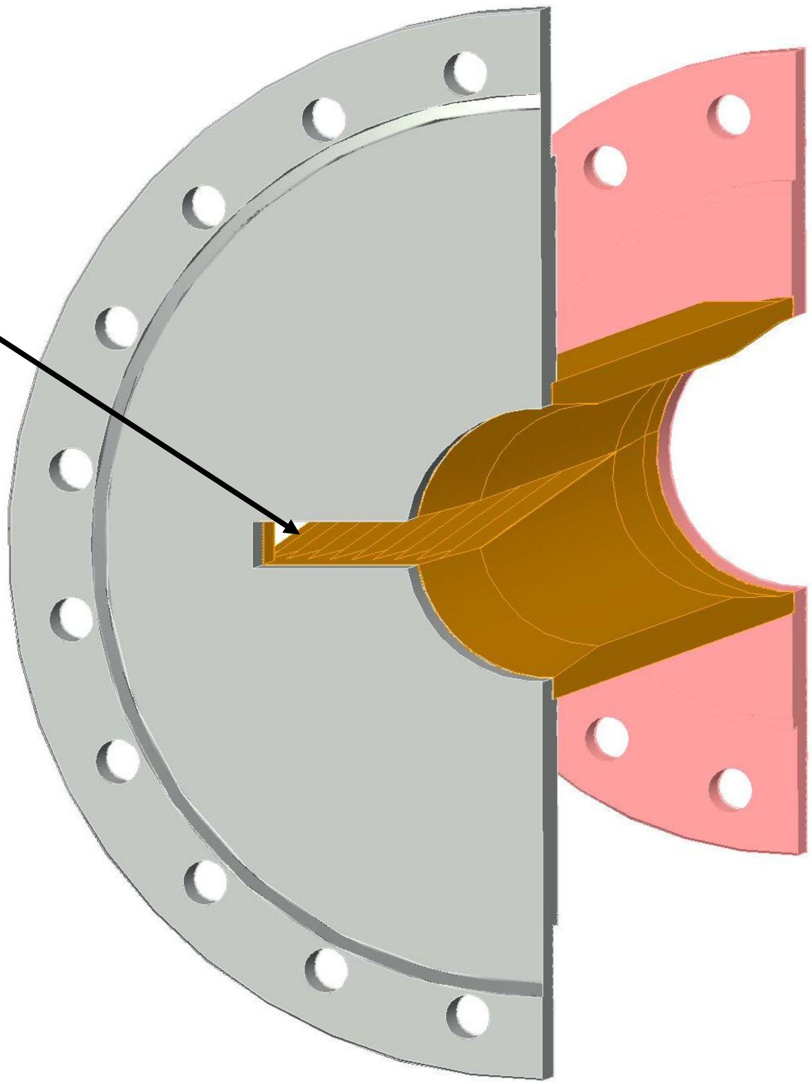
ILC Damping Ring – SR Absorber detail



ILC Damping Ring – SR Absorber detail

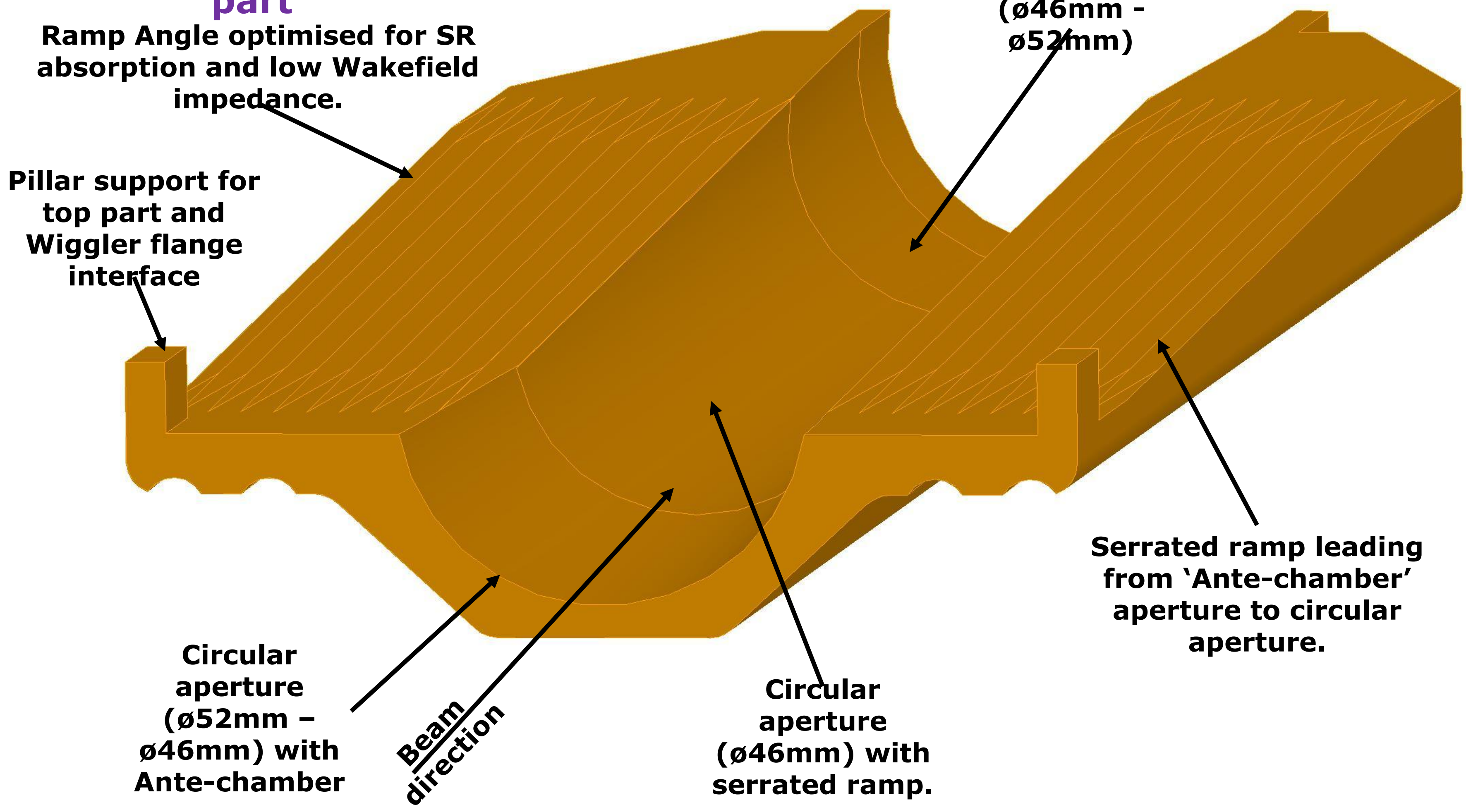


The ramped (or sow tooth) absorber geometry was originally invented at BINP for SR absorbers designed for Siberia-2 LS (Russia)

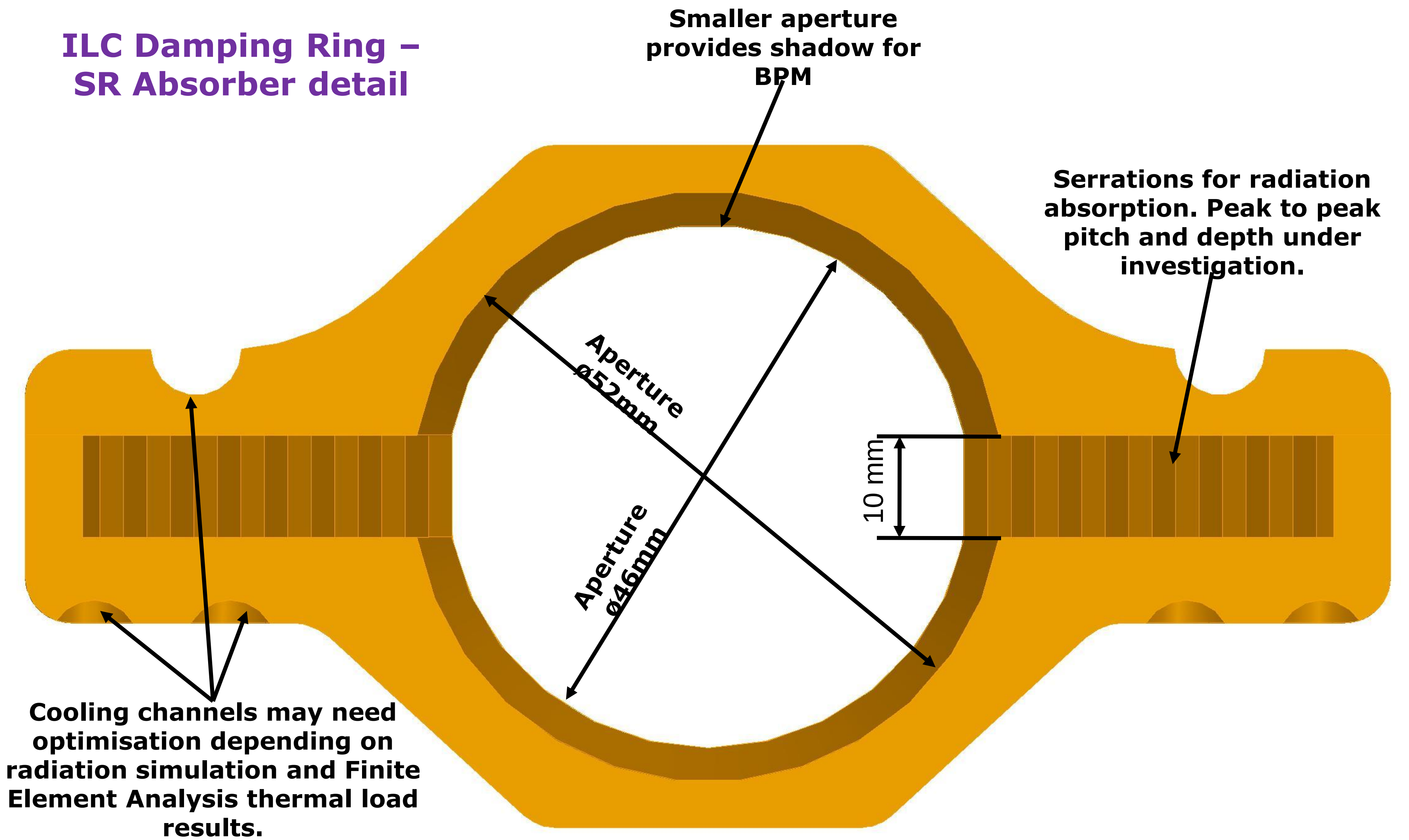


This geometry was also used for a crotch absorber in the Diamond LS (UK)

ILC Damping Ring – SR Absorber detail Bottom manufactured part

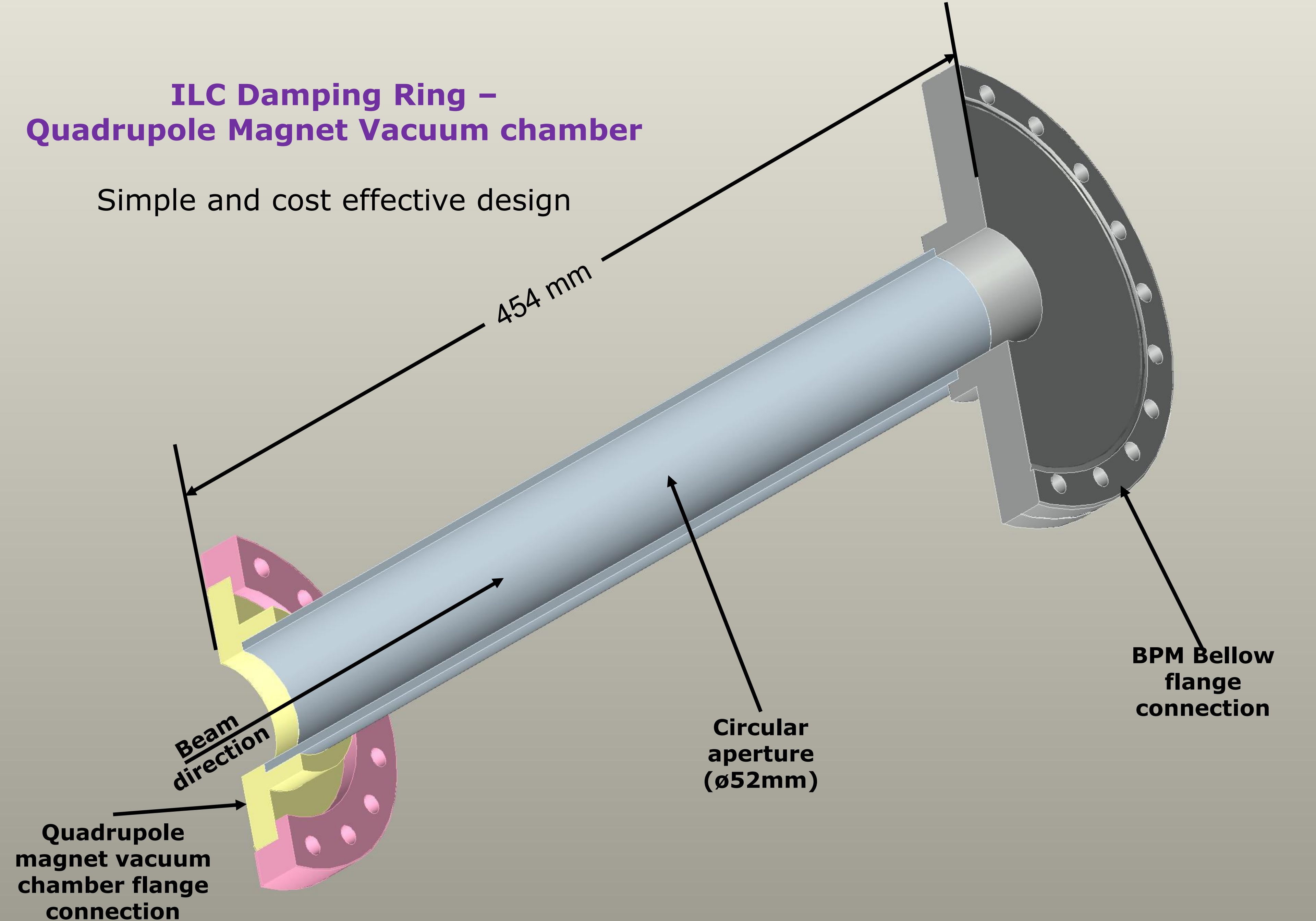


ILC Damping Ring – SR Absorber detail

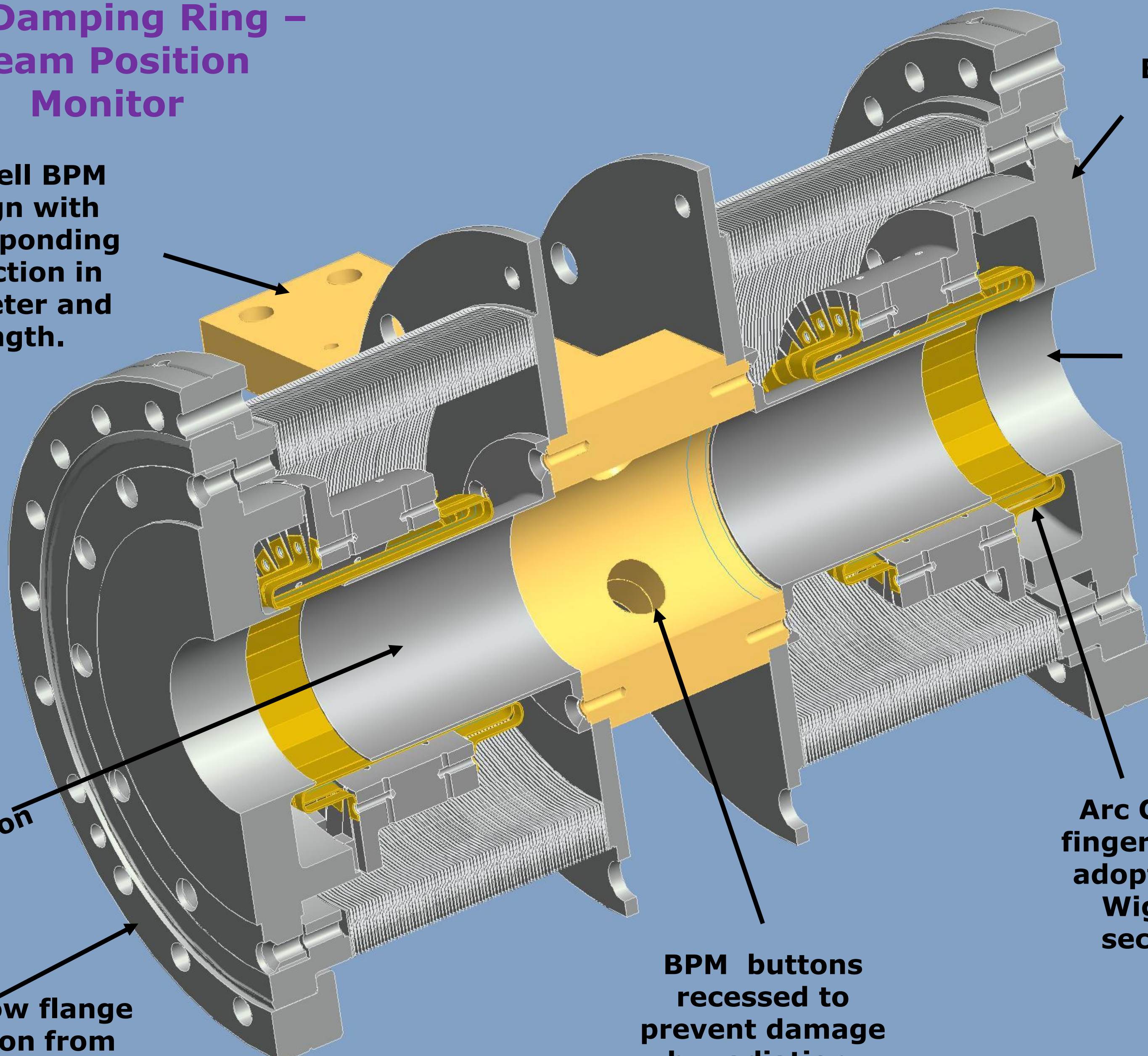


ILC Damping Ring – Quadrupole Magnet Vacuum chamber

Simple and cost effective design



ILC Damping Ring – Beam Position Monitor



Conclusions

- Mechanical design of ILC DR vacuum vessel includes requirements from
  - Impedance, e-cloud, power absorption and vacuum models
  - Low cost
- Drawing of vacuum vessel of ILC DR are available to be used for the next run of modelling.
  - Impedance and wake field calculation
  - e-cloud modelling
  - Vacuum system design
- Although the design is made for 6.4-km ring, most of the components could be used for 3.2-km rings models.