



CESR Sextupole Calibration (II)

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Machine Studies Meeting

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Update from 19 Aug 21

CBN 78-1

**Sextupole Magnetic Measurements
(D. Larson, L. Roberts and R. Talman)**

Parameter table (bore radius 47.24 mm, $L_{\text{pole}}=248$ mm, $L_{\text{mag}}=272$ mm)

Sextupole, vertical corrector strengths versus excitation current

$$S L = 1.18 \text{ m}^{-2} \text{ at } 13.2 \text{ A and } 10 \text{ GeV}$$

CON 95-6

**CESR Sextupole Upgrade
A. Mikhailichenko**

Motivation: improved field uniformity to accommodate pretzel orbits ($x_{\text{beam}} = \pm 2$ cm)

Hall probe measurements ($\delta B \simeq 10$ G, poletip field $B \simeq 1000$ G)

for one sextupole **before and three sextupoles **after** cutting 7.4 ± 0.2 mm from pole tip**

Multipole expansion for measured field values

CBN 98-2

**Sextupole for CESR
A. Mikhailichenko**

Mermaid 3D FE model matched to field measurements of CBN 95-6

Modeled $L_{\text{mag}} = 278$ mm (Bmad lattice element not updated from 272 mm)

Multipole expansion of modeled field integrals

$$\int B_Y(x, z) dz \text{ (kG cm)} = 1.06533 x^2 + 4.023e-6 x^8 - 2.278e-10 x^{14} \text{ (10 A, 160 A-turns)}$$



CBN 98-2

Table of Mermaid Field Integrals

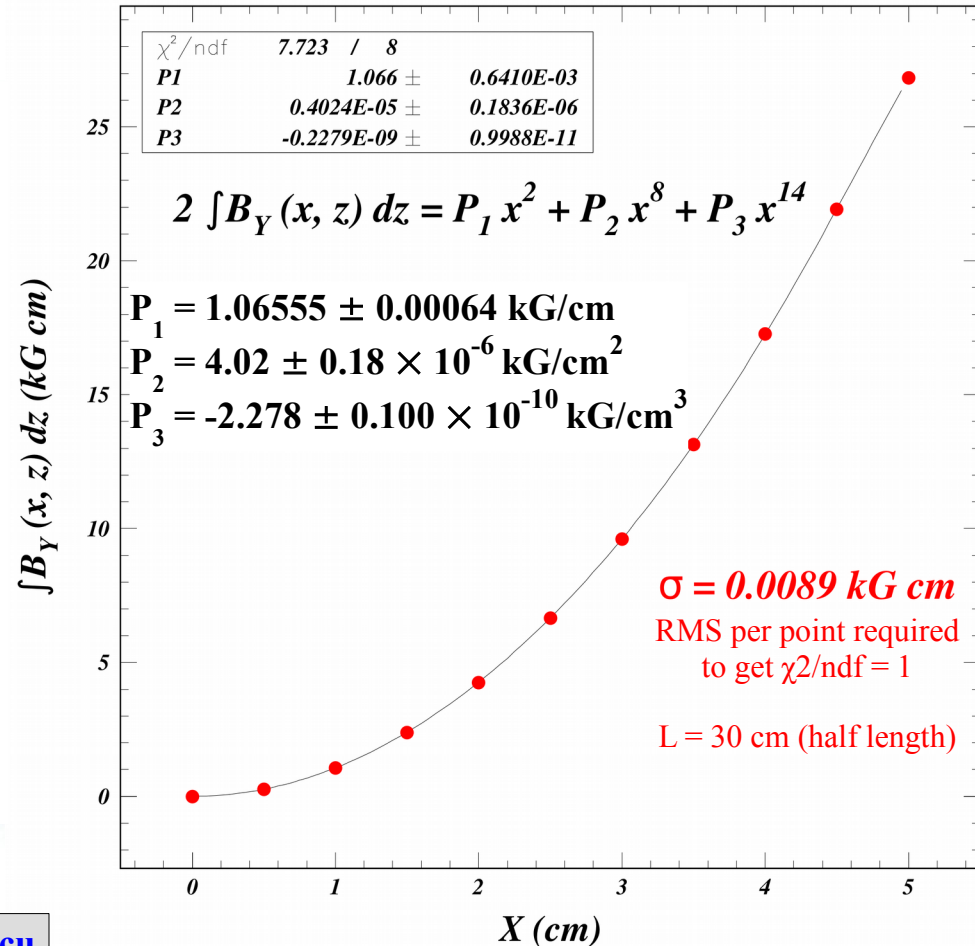
$x, \text{ cm}$	$I_{\text{half lens}}(x) = \int_0^{30\text{cm}} B_y(x,s) ds, \text{ kG} \cdot \text{cm}$
0.0	0.0
0.5	0.1272
1.0	0.5265
1.5	1.1934
2.0	2.1277
2.5	3.3305
3.0	4.8079
3.5	6.5698
4.0	8.6291
4.5	10.9647
5.0	13.410

$$\int B_Y dz = 1.06533 x^2 + 4.023e-6 x^8 - 2.278e-10 x^{14}$$

$$\Delta K_2 L = (10.6533 \text{ Tm}) (0.3/6) (1/10 \text{ A}) (12.5 \text{ A}/16\text{k cu}) \Delta \text{cu}$$

$$L_{\text{eff}} = 0.272 \text{ m (Bmad lattice)}$$

$$\Delta K_2 (\text{m}^{-3}) = 1.530e-4 \Delta \text{cu}$$

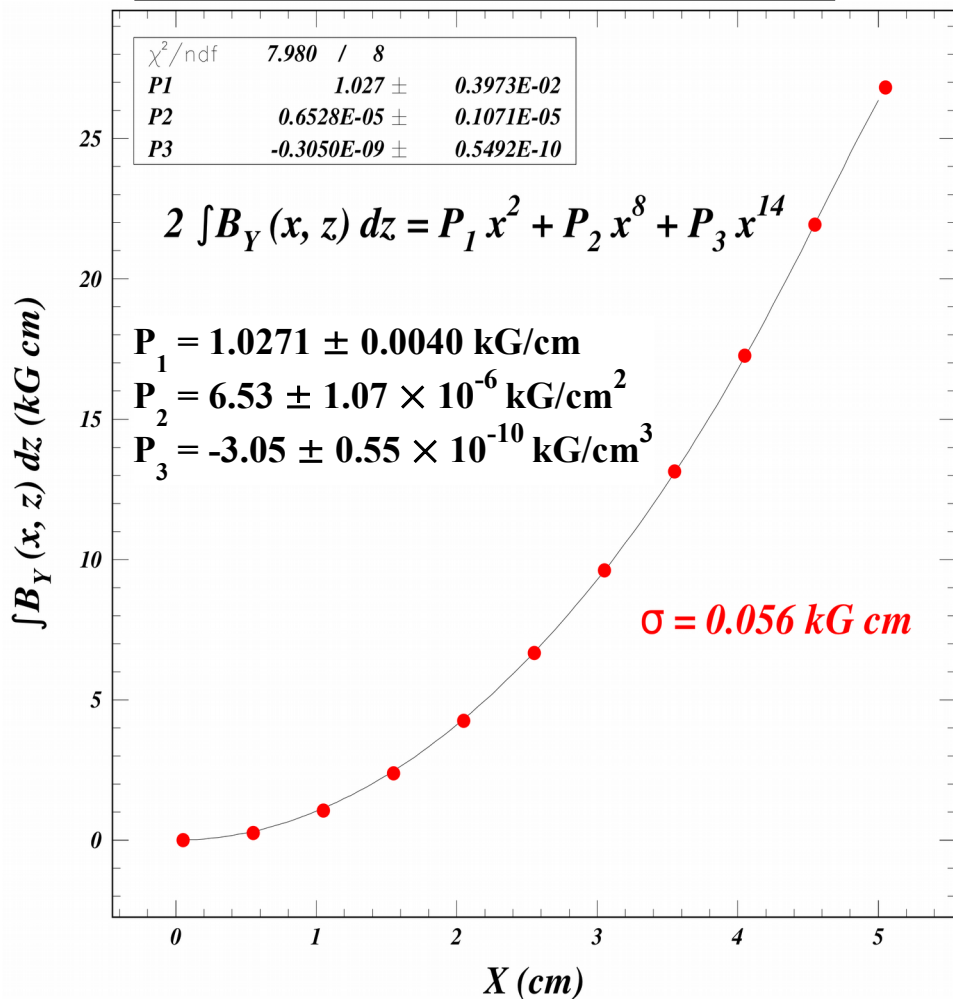


Good fit which reproduces AM result.

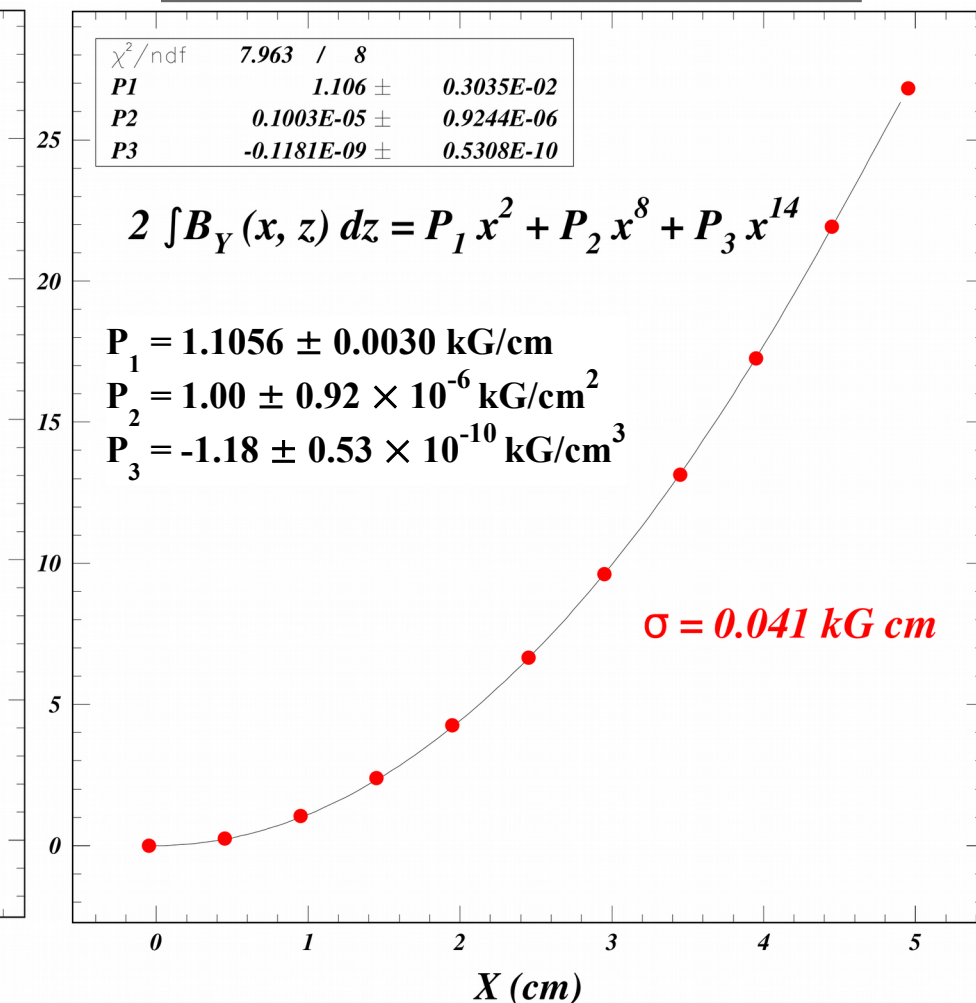
Jitter is about 0.3 Gauss.



X displaced by 0.5 mm



X displaced by -0.5 mm



Calibration factor changes by $\pm 4\%$ for ± 0.5 mm measurement displacement.



! There are two types of sextupoles, unmodified and modified.

! 4000 cu => 12.5 A

! Unmodified: see CBN 78-1 (31E/W, 32E/W)

!SI = 1.18 /m² @13.2 A, 10 GeV

! = 2.11 /m² @4000 cu, 5.29 GeV

!S = 1.94e-3 /cu-m³ @5.29 GeV

! => 515 cu = 1 /m³ @5.29 GeV

! Dimat has another factor of two => 1030 cu-m³

! Modified: see CBN 98/02

!IBy = 1.06553 kG/cm x² + ... @10 A

!S = 1/2 ec/E(d²B/dx²) by definition

!SI = (3e8m/s / 5.29e9V)*10.6553T/m @10 A, 5.29 GeV

!S = 2.777 /m³ @12.5 A, 5.29 GeV

! => 1440.4 cu-m³ @5.29 GeV

!

! dk2_dcu normalized to 5.29 GeV

\$ALL_CALIB

dk2_dcu_all = 1.736e-4 = 1.530 e-4 * 6.00 / 5.29 (modified)

The comments for the chopper calibration have not been changed since the upgrade from 4k cu range to 32k cu range, but the values for the sextupole calibration dk2_dcu have been updated.

Dimat is a code used prior to Bmad.

The S value in CBN 78-1 is apparently defined as Bmad’s K_2L .

The S value in CBN 98-2 is apparently defined as Bmad’s $K_2/2$.



! There are two types of sextupoles, unmodified and modified.
! See CON 96-5 for field measurements of both types.

! Chopper resolution $dcu/dI = 32000 \text{ cu} / 12.5 \text{ A}$
! Sextupole length $L=0.272 \text{ m}$

! Unmodified (31/32 W/E): see CBN 78-1 (NB: "S"=K2)

$$SL = 1.18 \text{ m}^{-2} @ 13.2 \text{ A}, 10 \text{ GeV}$$

$$= 2.11 \text{ m}^{-2} @ 12.5 \text{ A}, 5.29 \text{ GeV}$$

$$K2 = S = SL/L = 7.757 \text{ m}^{-3} @ 12.5 \text{ A}, 5.29 \text{ GeV}$$

$$\Rightarrow dK2/dcu = 2.424E-4 \text{ m}^{-3}/cu @ 5.29 \text{ GeV}$$

$$\Rightarrow dcu/dK2 = 4125 \text{ cu}/\text{m}^{-3} @ 5.29 \text{ GeV}$$

! Modified: see CBN 98/02

$$\text{Int By } dz = 1.06553 \text{ kG/cm } x^2 + \dots @ 10 \text{ A}$$

$$S = 1/2 ec/E(d^2B/dx^2) \text{ by definition}$$

$$SL = (3e8\text{m/s} / 5.29e9\text{V}) * 10.6553\text{T/m} @ 10 \text{ A}, 5.29 \text{ GeV}$$

$$S = SL/L = 2.777 \text{ m}^{-3} @ 12.5 \text{ A}, 5.29 \text{ GeV}$$

$$\Rightarrow dS/dcu = 8.678E-5 \text{ m}^{-3} /cu @ 5.29 \text{ GeV}$$

$$\Rightarrow dcu/dS = 11523 \text{ cu}/\text{m}^{-3} @ 5.29 \text{ GeV}$$

$$K2 = 2S = 5.554 \text{ m}^{-3} @ 12.5 \text{ A}, 5.29 \text{ GeV}$$

$$\Rightarrow dK2/dcu = 1.736E-4 \text{ m}^{-3}/cu @ 5.29 \text{ GeV}$$

$$\Rightarrow dcu/dK2 = 5762 \text{ cu}/\text{m}^{-3} @ 5.29 \text{ GeV}$$

!!
! $dk2_dcu$ normalized to 5.29 GeV

\$ALL_CALIB

$$dk2_dcu_all = 1.736e-4$$

Update the chopper resolution.

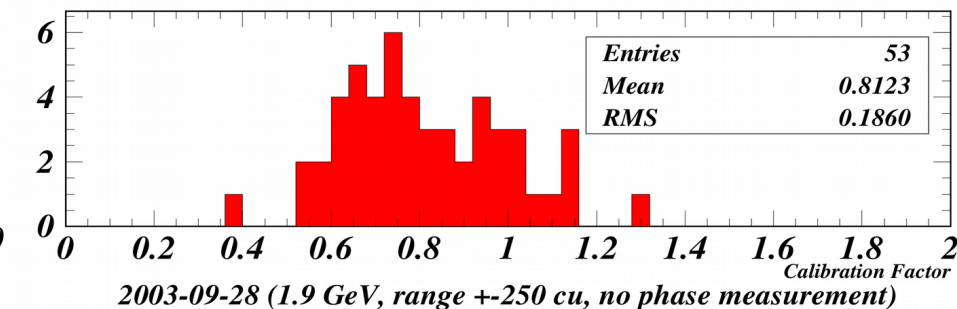
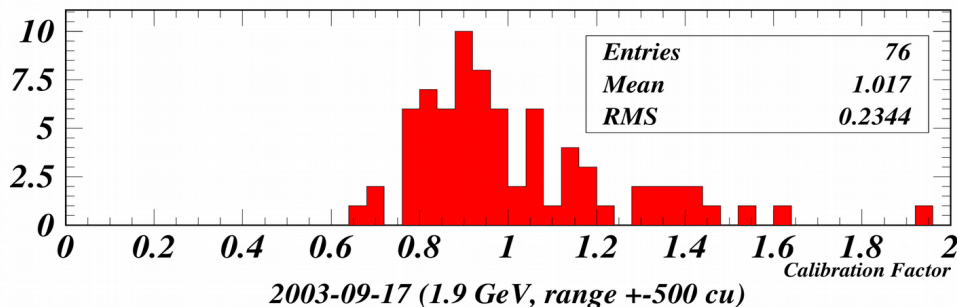
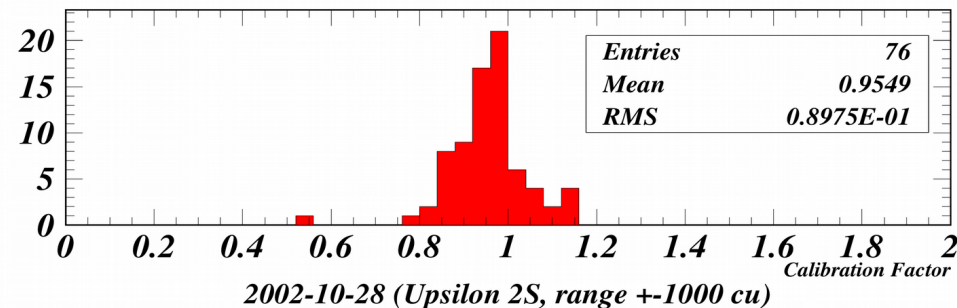
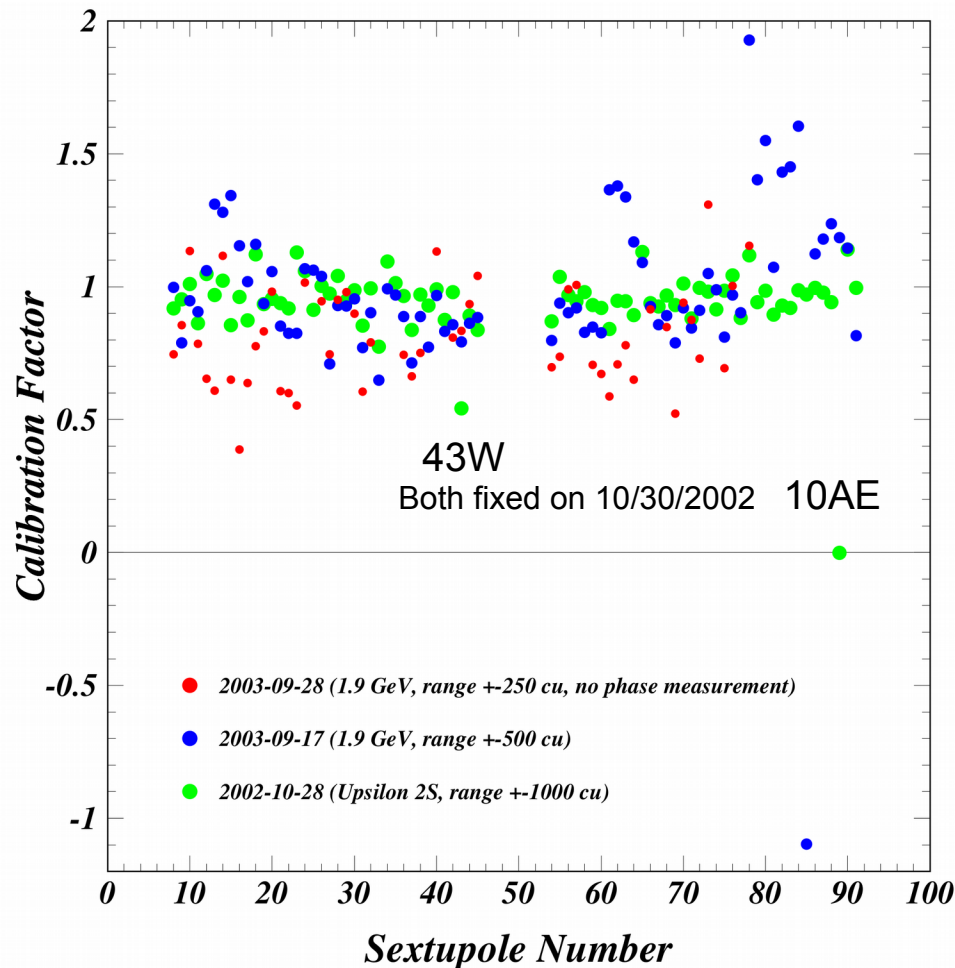
Add reference to CON 96-05 where Hall probe measurements for both types of sextupole are available.

Make equations explicit.

Adapt units to the quantity they describe (personal preference?)

Make explicit that CBN 78-1 and CBN 98-2 use different conventions for S.

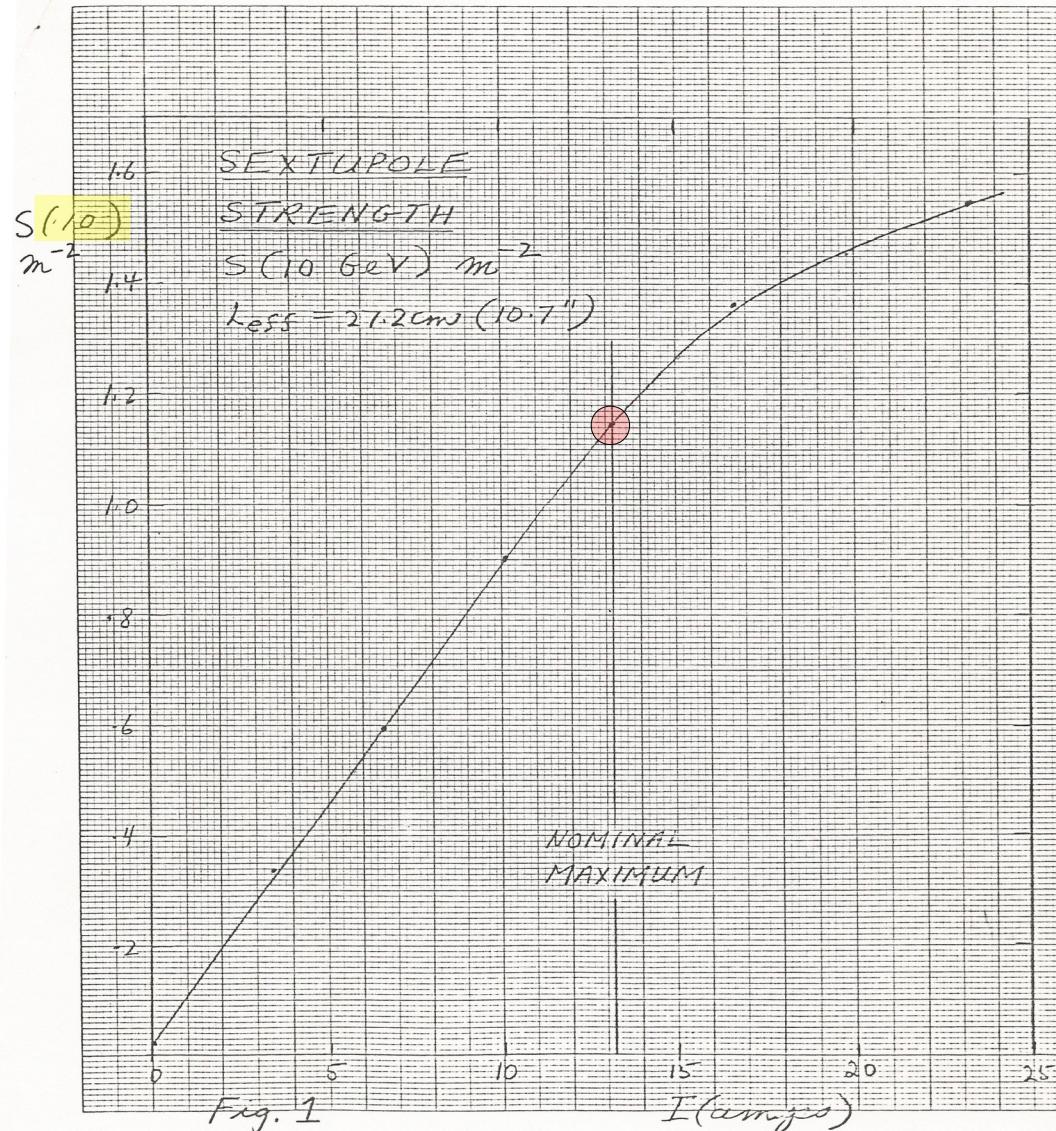
Calibration factors $dk2_dcu$ are unchanged.



The measured calibration factors are accurate to much better than a factor of two.

They vary by 7% for the October 2002 measurements at 5.012 GeV.

Contribution from measurement accuracy at 3.125 A (1000 cu then, 4000 cu now) unknown.



“ $S = 1.18 \text{ m}^{-2}$ for 13.2 A at 10 GeV”

This is the integrated strength SL.

According to the definition

$$SL = 0.5 (0.3/10) L (d^2B_Y/dx^2)$$

$$L (d^2B_Y/dx^2) = 2 (10/0.3) SL = 78.6 \text{ T/m}$$

$$\text{So } B_Y = 78.6/2/0.272 x^2 = 144 x^2$$

However, the measurement of the unmodified sextupole in CON 96-05 found

$$B_Y = 66.5 x^2 \text{ for } 13.2 \text{ A.}$$

The discrepancy is resolved at the level of 8% if we suppose CBN 78-1 measured $K_2 L$ instead of SL.