LECTURE 25

Collective instabilities;

Rigid beam transverse instability

This is the transverse analog of the Robinson instability

To see how this works, consider a "macroparticle": a point charge of magnitude *Ne*, circulating in a synchrotron. This macroparticle will create a wake field when it passes through an impedance. The macroparticle undergoes betatron oscillations; the wake potentials introduce additional forces into the betatron equations of motion. These additional forces can lead to an instability.

12/4/01

USPAS Lecture 25

1

3

The wake fields generated by the macroparticle can be expressed in terms of a transverse integrated force exerted at the location of the impedance. The transverse integrated force due to a pure harmonic current, with an mth moment, of the form , $I_m(t) = \tilde{I}_m(\omega)\cos(\omega t)$ from Lecture 21, p 25, can be written in terms of the impedance as

$$\vec{F}_{\perp}(t) = ieI_m(t)mr^{m-1} \Big(\hat{r} \cos m\phi - \hat{\phi} \sin m\phi \Big) Z_m^{\perp}(\omega)$$

For m=1, and in the vertical direction, we have

$$\overline{F}_{y}(t) = ieI_{1}(t)Z_{1}^{\perp}(\omega)$$

To use the above equation, we need to know the Fourier spectrum of the dipole moment of the current, which consists of a single circulating macroparticle of charge *Ne*. Let us consider for the moment the monopole current of a macroparticle that is

12/4/01

USPAS Lecture 25

2

not undergoing betatron oscillations. As discussed above in Lecture 23, the current due to the point charge Ne is a series of impulses, which occur at times $t = nT_0$, where n is the turn number, an integer running from $-\infty$ to ∞ . This current can be represented as a sum of Dirac delta-functions

$$I_0(t) = Ne \sum_{n = -\infty}^{\infty} \delta(t - nT_0)$$

in which T_0 is the revolution period.

As explained in Lecture 23, this can be written in terms of harmonics as

$$I_0(t) = \frac{Ne}{T_0} \sum_{p=-\infty}^{\infty} \exp(-ip\,\omega_0 t)$$

Now let us consider the dipole moment of the current. For a particle executing a betatron oscillation, we have $I_1(t) = I_0(t)y(t)$, where y(t) has the form of a betatron oscillation, evaluated at the location of the impedance. Thus

$$y(t) = y_0 \cos(Q_y \omega_0 t) + y_0' \beta_y \sin(Q_y \omega_0 t)$$
$$y'(t) = -\frac{y_0}{\beta_y} \sin(Q_y \omega_0 t) + y_0' \cos(Q_y \omega_0 t)$$

Then we have

12/4/01

$$\begin{split} &I_{1}(t) = I_{0}(t)y(t) = \\ &\frac{Ne}{T_{0}} \Big(y_{0} \cos \Big(Q_{y} \omega_{0} t \Big) + y_{0}' \beta_{y} \sin \Big(Q_{y} \omega_{0} t \Big) \Big) \sum_{p=-\infty}^{\infty} \exp(-ip\omega_{0} t) \\ &= \frac{Ne}{2T_{0}} \sum_{p=-\infty}^{\infty} \Big(y_{0} + iy_{0}' \beta_{y} \Big) \exp\Big(-i \Big(p + Q_{y} \Big) \omega_{0} t \Big) \\ &+ \Big(y_{0} - iy_{0}' \beta_{y} \Big) \exp\Big(-i \Big(p - Q_{y} \Big) \omega_{0} t \Big) \end{split}$$

The integrated force, summed over all harmonics, will then be

12/4/01

USPAS Lecture 25

5

$$\begin{split} \overline{F}_{y}(t) &= \frac{iNe^{2}}{2T_{0}} \sum_{p=-\infty}^{\infty} \left(y_{0} + iy_{0}'\beta_{y} \right) \exp\left(-i\left(p + Q_{y}\right)\omega_{0}t \right) Z_{1}^{\perp} \left(\left(p + Q_{y}\right)\omega_{0} \right) \\ &+ \left(y_{0} - iy_{0}'\beta_{y} \right) \exp\left(-i\left(p - Q_{y}\right)\omega_{0}t \right) Z_{1}^{\perp} \left(\left(p - Q_{y}\right)\omega_{0} \right) \\ &= \frac{iNe^{2}}{2T_{0}} \sum_{p=-\infty}^{\infty} \tilde{y}_{0} \exp\left(-i\left(p + Q_{y}\right)\omega_{0}t \right) Z_{1}^{\perp} \left(\left(p + Q_{y}\right)\omega_{0} \right) \\ &+ \tilde{y}_{0}^{*} \exp\left(-i\left(p - Q_{y}\right)\omega_{0}t \right) Z_{1}^{\perp} \left(\left(p - Q_{y}\right)\omega_{0} \right) \\ &\text{using } \tilde{y} = y + i\beta_{y}y' \end{split}$$

We want to evaluate this on each turn, that is, at $t=nT_0$.

12/4/01

USPAS Lecture 25

6

$$\overline{F}_{y}(nT_{0}) = \overline{F}_{y,n} = \frac{iNe^{2}}{2T_{0}} \left(\exp(-i2\pi Q_{y}n)\tilde{y}_{0} \sum_{p=-\infty}^{\infty} Z_{1}^{\perp}((p+Q_{y})\omega_{0}) + \exp(i2\pi Q_{y}n)\tilde{y}_{0}^{*} \sum_{p=-\infty}^{\infty} Z_{1}^{\perp}((p-Q_{y})\omega_{0}) \right)$$

Then, we can use the symmetry property

$$Z_1^{\perp}(\omega) = -Z_1^{\perp *}(-\omega).$$

So that

$$\sum_{p=-\infty}^{\infty} Z_1^{\perp} \left(\left(p - Q_y \right) \omega_0 \right) = - \sum_{p=-\infty}^{\infty} Z_1^{\perp *} \left(\left(p + Q_y \right) \omega_0 \right)$$

and we have

$$\overline{F}_{y,n} = \frac{iNe^2}{2T_0} \begin{bmatrix} \tilde{y}(n) \sum_{p=-\infty}^{\infty} Z_1^{\perp} ((p+Q_y)\omega_0) \\ -\tilde{y}^*(n) \sum_{p=-\infty}^{\infty} Z_1^{\perp *} ((p+Q_y)\omega_0) \end{bmatrix}$$

This can be written as

$$\overline{F}_{y,n} = -\frac{Ne^2}{T_0} \times$$

$$\left(y(n)\sum_{p=-\infty}^{\infty}\operatorname{Im}\left[Z_{1}^{\perp}\left(\left(p+Q_{y}\right)\omega_{0}\right)\right]+\beta_{y}y'(n)\sum_{p=-\infty}^{\infty}\operatorname{Re}\left[Z_{1}^{\perp}\left(\left(p+Q_{y}\right)\omega_{0}\right)\right]\right)$$

We now insert this into the betatron equations of motion. The unperturbed betatron equations, written in terms of turn number, have the form

12/4/01

USPAS Lecture 25

7

12/4/01

USPAS Lecture 25

8

$$\frac{dy'}{dn} = -2\pi Q_y \frac{y(n)}{\beta_y} \quad \frac{dy}{dn} = 2\pi Q_y \beta_y y'(n)$$

The effect of the integrated force is to produce a change in y' given by $\Delta y' = \frac{\overline{F}_{y,n}}{pv} = \frac{\overline{F}_{y,n}}{m_0 c^2 \gamma}$. Hence the equation of motion becomes

$$\frac{dy'}{dn} = -2\pi Q_y \frac{y(n)}{\beta_y} - \frac{Ne^2}{m_0 c^2 \gamma T_0} \left(Ay(n) + B\beta_y y'(n) \right)$$

$$A = \sum_{p=-\infty}^{\infty} \operatorname{Im} \left[Z_{1}^{\perp} \left(\left(p + Q_{y} \right) \omega_{0} \right) \right] \quad B = \sum_{p=-\infty}^{\infty} \operatorname{Re} \left[Z_{1}^{\perp} \left(\left(p + Q_{y} \right) \omega_{0} \right) \right]$$
 and so

12/4/01

USPAS Lecture 25

9

$$\begin{split} &\frac{d^{2}y}{dn^{2}} = 2\pi Q_{y}\beta_{y}\frac{dy'(n)}{dn} \\ &= -\Big(2\pi Q_{y}\Big)^{2}y(n) - \frac{2\pi Q_{y}\beta_{y}Ne^{2}}{m_{0}c^{2}\gamma T_{0}}\Big(Ay(n) + B\beta_{y}y'(n)\Big) \\ &= -\Big(\Big(2\pi Q_{y}\Big)^{2} + \frac{2\pi Q_{y}\beta_{y}Ne^{2}}{m_{0}c^{2}\gamma T_{0}}A\Big)y(n) - \frac{\beta_{y}Ne^{2}}{m_{0}c^{2}\gamma T_{0}}B\frac{dy}{dn} \end{split}$$

The A coefficient is associated with a tune shift; the B coefficient can cause damping or an instability. This equation has the general form

$$\frac{d^2y}{dn^2} = -2\alpha \frac{dy}{dn} - \left(2\pi Q_y'\right)^2 y$$

12/4/01

USPAS Lecture 25

10

which is the equation of a damped harmonic oscillator, with a solution (for $\alpha << 2\pi Q_{\nu}'$)

$$y(n) \propto \exp(-\alpha + 2\pi i Q_y') n$$

By comparing with the equation above, we see that the damping rate (per turn) is

$$\alpha = \frac{\beta_y N e^2}{2m_0 c^2 \gamma T_0} B = \frac{\beta_y N e^2}{2m_0 c^2 \gamma T_0} \sum_{p = -\infty}^{\infty} \text{Re} \left[Z_1^{\perp} ((p + Q_y) \omega_0) \right]$$

and the frequency is given by

$$(2\pi Q_y')^2 = (2\pi Q_y)^2 + \frac{2\pi Q_y \beta_y N e^2}{m_0 c^2 \gamma T_0} A$$

Using

$$2\pi Q_y' = \sqrt{\left(2\pi Q_y\right)^2 + \Delta} = 2\pi Q_y \sqrt{1 + \frac{\Delta}{\left(2\pi Q_y\right)^2}} \approx 2\pi Q_y + \frac{\Delta}{4\pi Q_y}$$

$$\Rightarrow \delta Q_y = \frac{\Delta}{8\pi^2 Q_y}$$

we get

$$\delta Q_{y} = \frac{\beta_{y} N e^{2}}{4\pi m_{0} c^{2} \gamma T_{0}} A = \frac{\beta_{y} N e^{2}}{4\pi m_{0} c^{2} \gamma T_{0}} \sum_{p=-\infty}^{\infty} \text{Im} \left[Z_{1}^{\perp} \left(\left(p + Q_{y} \right) \omega_{0} \right) \right]$$

Example: the transverse resistive wall instability. The impedance is (Lecture 19, p 23)

$$\begin{split} Z_{1}^{\perp}(\omega) &= C \frac{1 - i \operatorname{sgn}(\omega)}{\omega \pi b^{3}} \sqrt{\frac{|\omega| \mu c^{2}}{2\sigma}} \\ \sum_{p = -\infty}^{\infty} \operatorname{Re} \Big[Z_{1}^{\perp} \Big(\Big(p + Q_{y} \Big) \omega_{0} \Big) \Big] &= \frac{C}{\pi b^{3}} \sqrt{\frac{\mu c^{2}}{2\omega_{0}\sigma}} \sum_{p = -\infty}^{\infty} \frac{\sqrt{|p + Q_{y}|}}{p + Q_{y}} \\ &= \frac{C}{\pi b^{3}} \sqrt{\frac{\mu c^{2}}{\omega_{0}\sigma}} f\Big(\Delta_{\beta} \Big), \quad f\Big(\Delta_{\beta} \Big) &= \frac{1}{\sqrt{2}} \sum_{p = -\infty}^{\infty} \frac{\sqrt{|p + \Delta_{\beta}|}}{p + \Delta_{\beta}}, \quad Q_{y} = n + \Delta_{\beta} \end{split}$$

in which n is the integral part of the tune.

The damping rate per turn is

$$\alpha = \frac{\beta_y N e^2 c^2}{2\pi b^3 \gamma m_0 c^2} \sqrt{\frac{\mu}{\omega_0 \sigma}} f(\Delta_\beta)$$

The function

$$f(\Delta_{\beta}) = \frac{1}{\sqrt{2}} \sum_{p=-\infty}^{\infty} \frac{\sqrt{|p+\Delta_{\beta}|}}{p+\Delta_{\beta}} = \frac{1}{\sqrt{2}} \left(\frac{\Delta_{\beta}}{|\Delta_{\beta}|^{3/2}} + \zeta\left(\frac{1}{2}, 1+\Delta_{\beta}\right) - \zeta\left(\frac{1}{2}, 1-\Delta_{\beta}\right) \right)$$

 $(\zeta(a,b))$ is the zeta function) is shown below

12/4/01

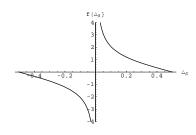
USPAS Lecture 25

13

12/4/01

USPAS Lecture 25

14



For damping, we need to have $\alpha>0$, that is, $f(\Delta_{\beta})>0$, which requires $\Delta_{\beta}>0$ Since $\Delta_{\beta}=Q_y-n$, to damp the transverse resistive wall instability, the fractional part of the machine tune should be below the half-integer, that is, in the range $0<\Delta_{\beta}<0.5$

For CESR parameters: Q_y =9.58, Δ_{β} =-0.42, $f(\Delta_{\beta})$ =-0.27, β_y =20 m, N=2x10¹¹, b=2.5 cm, γ =10⁴, T_0 =2.5 μ s, σ =3.5x10⁷ Ω^{-1} m⁻¹ (aluminum), we find a growth time of $\frac{T_0}{\alpha}$ = -0.67 s. (not a very strong instability).

12/4/01

USPAS Lecture 25

15

12/4/01

USPAS Lecture 25

16