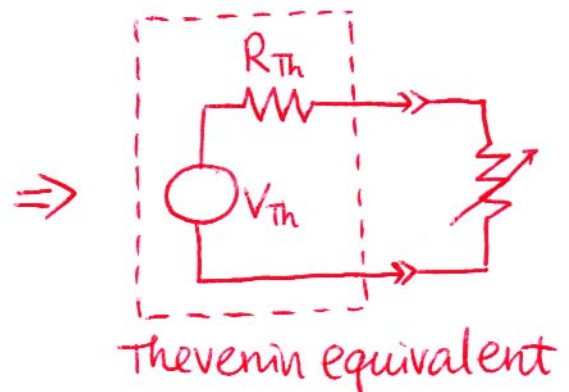
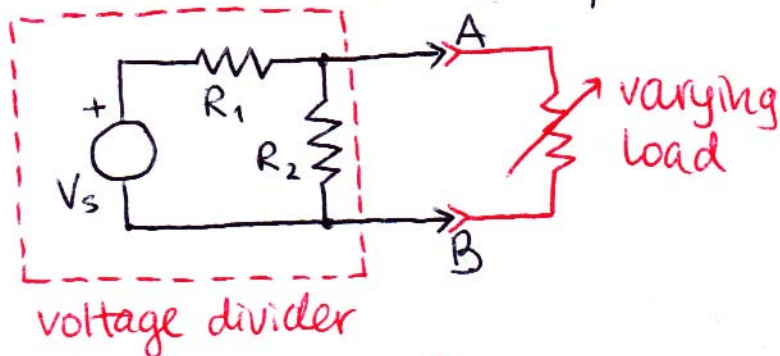


Lecture 3

Thevenin th. - example



$$V_{Th} = V_{o.c.} = V_s \frac{R_2}{R_1 + R_2} ; I_{s.c.} = \frac{V_s}{R_1} \Rightarrow$$

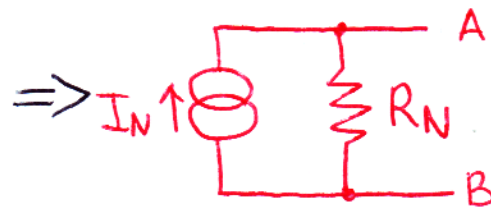
$$R_{Th} = \frac{V_{Th}}{I_{s.c.}} = \frac{V_s R_2}{R_1 + R_2} \frac{R_1}{V_s} = \frac{R_1 R_2}{R_1 + R_2} = R_1 \parallel R_2$$

Useful trick: to find R_{Th} , short all volt. sources and open all curr. sources. R_{Th} is resistance by looking inside the two terminals.

Norton equivalent

same as Thevenin but \Rightarrow

$$I_N = I_{s.c.} , R_N = \frac{V_{o.c.}}{I_N}$$



Q: R_N vs R_{Th} ? same

Q: which one to use, Nor or Th?

if $R_N = R_{Th} \ll R_L$  \Rightarrow use Th

if $R_N = R_{Th} \gg R_L$  \Rightarrow use N

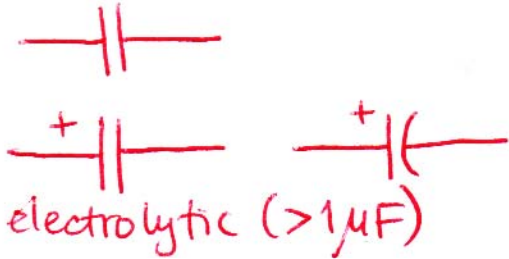
Linear time-dep. elements

(2)

Linear if KVL & KCL contain terms $\propto I, V, \frac{dI}{dt}, \frac{d^2V}{dt^2}, \text{etc.}$
but never $I^2, IV, \left(\frac{dV}{dt}\right)^2, \text{etc.}$

(4) Capacitor

stores en. in
elect. field



2 parallel plates
separated by
insulator

$$Q = CV, \quad C = \frac{Q}{V} = \frac{\text{coul.}}{\text{volt.}}$$

[C] = farads


$$C_{\text{Total}} = \left(\sum \frac{1}{C_k} \right)^{-1} \quad \text{series} \quad \left. \vphantom{C_{\text{Total}}} \right\} \text{opposite to } R$$
$$= \sum C_k \quad \text{parallel}$$

$$V = \frac{Q}{C}, \quad \Rightarrow \quad \frac{dV}{dt} = \frac{1}{C} \underbrace{\frac{dQ}{dt}}_{\text{curr.}} = \frac{I}{C}$$

$$\boxed{\frac{dV}{dt} = \frac{I}{C}}$$

Q: can V_c change abruptly? no, b/c unphys. $I_c \rightarrow \infty$

(5) Inductors


stores energy
in magn. field

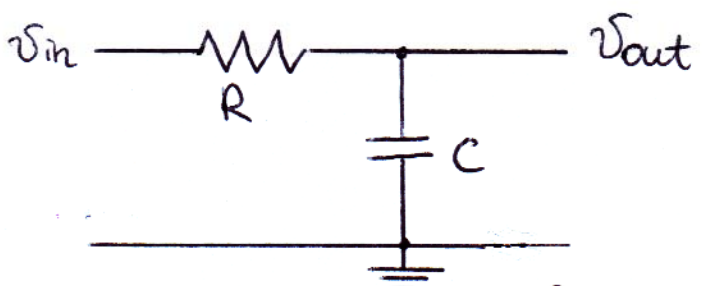
$$\boxed{V = L \frac{dI}{dt}}$$

$$[L] = \frac{V \cdot s}{A} = \text{henries}$$

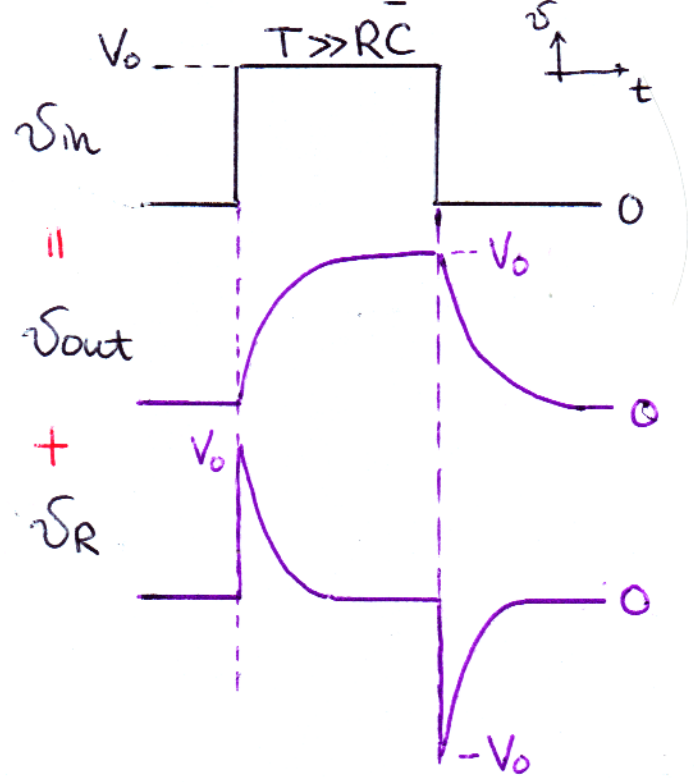
$$L_{TOTAL} = \sum L_k \text{ series} \\ = \left(\sum L_k^{-1} \right)^{-1} \text{ parallel} \quad \left. \vphantom{\sum L_k} \right\} \text{ like } R$$

Bulky \approx MHz, not routinely used (often can do the same with R & C)

Low - Pass filter (pass low speed signal)



$$V_{in} - V_{out} = V_R, \quad V_C = V_{out} \\ i_R = i_C. \quad V_R = i_R \cdot R, \quad i_C = C \frac{dV_C}{dt} \\ \frac{V_{in} - V_{out}}{R} = C \frac{dV_{out}}{dt} \quad \text{Diff. eqn.}$$



For voltage step $V_I \rightarrow V_F$, the soln.

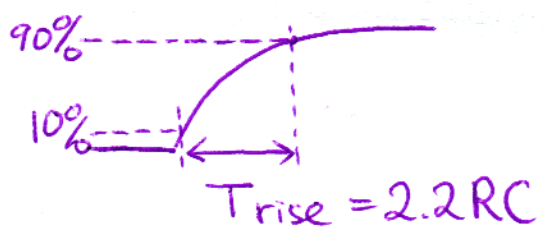
$$V_{out} = V_F + (V_I - V_F) e^{-\frac{t}{\tau}}$$

with $\tau = RC$

check that the formula works at $t=0$ and $t \rightarrow \infty$.

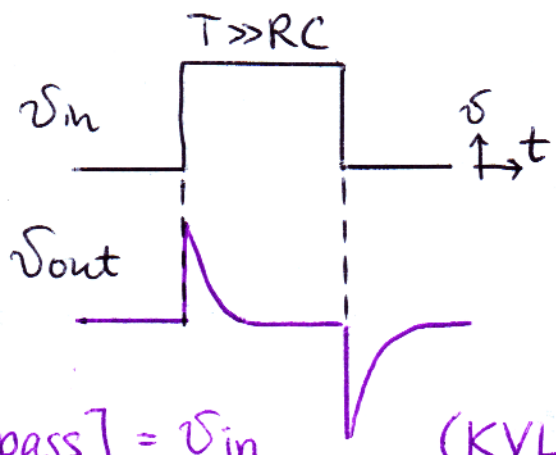
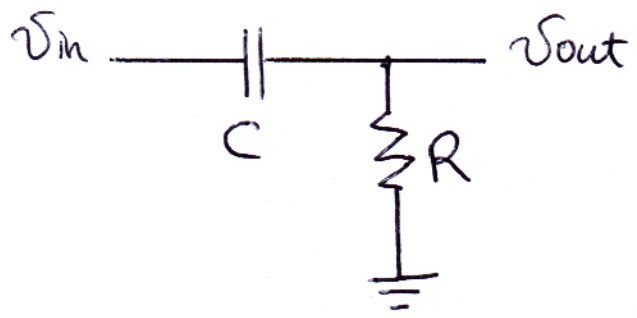
$i_R = \frac{V_R}{R} \rightarrow$ current flows only during switching
(efficient battery-driven devices don't like high f)

Piece of trivia: V_C vs t after step in voltage



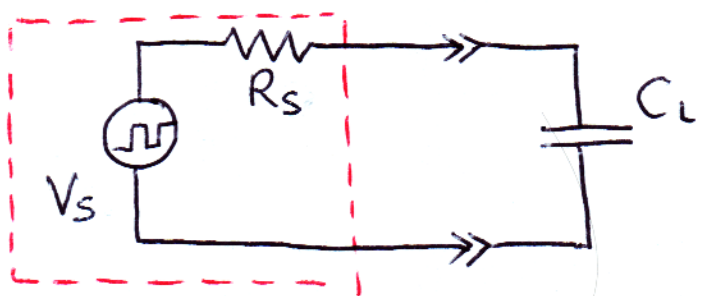
how scope finds Trise

High-pass filter (swap R & C positions)



$[V_{out \text{ hi pass}}] + [V_{out \text{ lo pass}}] = V_{in}$ (KVL)

Exp I-10



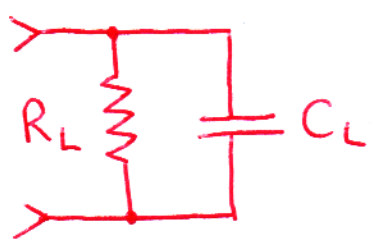
Function generator produces \square , \wedge , \sim
drives capacitive load C_L
e.g. piezzo, MOSFETs

input if $T \ll R_s C_L \Rightarrow$ output

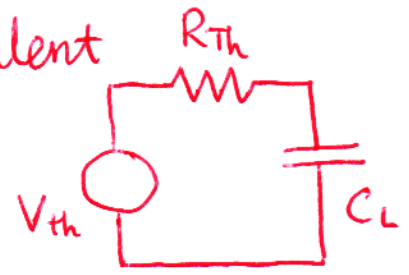
'Fake' large R_i by adding large R to f -generator. *not what you intended*

Need to transmit shape. How?

Soln.



Thev. equivalent



New $\tau = R_{Th} C_L$ can be made $\tau \ll T$.

$$R_{Th} = \frac{R_s R_L}{R_s + R_L}, \quad V_{Th} = V_s \frac{R_L}{R_s + R_L}$$

Shape transmitted! (But now V_{Th} can be $V_{Th} \ll V_s$)