

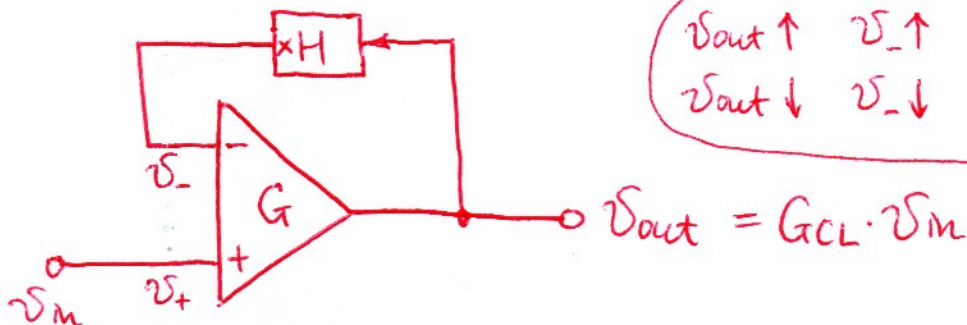
Lecture 10

Negative FeedbackGood amp :

- $R_{in} \gg R_s$ (large input impedance)
- $R_{out} \ll R_L$ (small output imp.)
- $G(\omega) = \text{const}$ (in freq. range of interest)

"Bare" op-amp problems :

- small active range (10's μV)
- large G variations (temp. drifts)
- $G \propto \frac{1}{\omega}$ for $\omega_c \geq 10\text{Hz}$
- R_{out} is fairly large ($R_{out} \sim 80\Omega$)



$v_{out} \uparrow$ $v_- \uparrow$ $v_{out} \downarrow$ } fluct. in v_{out}
 $v_{out} \downarrow$ $v_- \downarrow$ $v_{out} \uparrow$ } with v_{in} fixed
 are reduced

do after defns.

$G = G_{OL} = \text{open-loop gain}$ ("bare" op-amp gain)

$H = \text{transfer fn of feedback loop}$ (e.g. voltage divider)

$G_{CL} = \text{closed loop gain}$

$HG = \text{loop gain}$

$$v_{out} = G(v_+ - v_-) = G(v_{in} - H v_{out}) \Rightarrow \quad (2)$$

$$v_{out}(1+GH) = G v_{in}$$

$$G_{CL} \equiv \frac{v_{out}}{v_{in}} = \frac{G}{1+GH}$$

$|H| < 1$ (passive network)

E.g. choose $|GH| \gg 1$ $G \sim 2 \times 10^5$, $H \sim \frac{1}{100}$

$$\Rightarrow GH \sim 2 \times 10^3$$

$$G_{CL} = \frac{1}{H} \quad \text{for } |GH| \gg 1 \quad (\text{indep. of } G!)$$

- throw away some (most) gain to make a stable circuit, indep. of op-amp fluctuations

Advantages of negative F.B.

① G_{CL} is insensitive to G (G_{OL}) variations

$$\frac{dG_{CL}}{dG} = \frac{d}{dG} \left(\frac{G}{1+GH} \right) = \frac{(1+GH) - H(G)}{(1+GH)^2} = \frac{1}{(1+GH)^2} \ll 1$$

e.g. 741 $G_{typ} \sim 2 \times 10^5$ $G_{min} \sim 2 \times 10^4$

H	G	G_{CL} <small>close to $\frac{1}{H}$</small>	} $\Delta G_{CL} \approx 0.5\%$ for ΔG variation by $\times 10$
1/100	2×10^5	99.95	
"	2×10^4	99.5	
"	2×10^3	95.24	

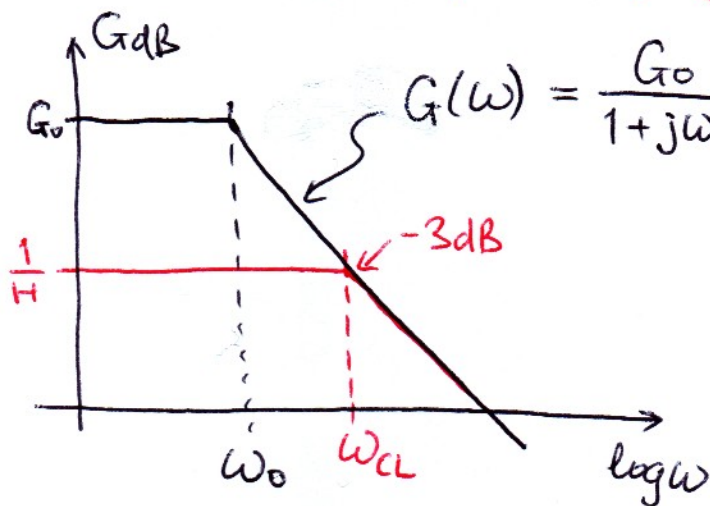
② Larger input range

$$(v_{in})_{active} = \frac{V_{sat+} - V_{sat-}}{G_{CL}} \approx H (V_{sat+} - V_{sat-})$$

e.g. $H \sim \frac{1}{100}$, $\pm 15V$ rails $\Rightarrow (v_{in})_{active} \approx \frac{28V}{100} = 0.28V$

③ Flat freq. response of gain (G_{CL})

③



$$G(\omega) = \frac{G_0}{1+j\omega/\omega_0} \quad \text{"bare" op-amp gain}$$

$$G_{CL} = \frac{1}{H} \frac{GH}{1+GH} = \frac{1}{H} \frac{1}{1+\frac{1}{GH}}$$

ω_{CL} = corner freq.
when $|\frac{1}{GH}| \sim 1$

if $\omega \gg \omega_0$, $G \sim \frac{G_0}{j\omega/\omega_0}$, \Rightarrow

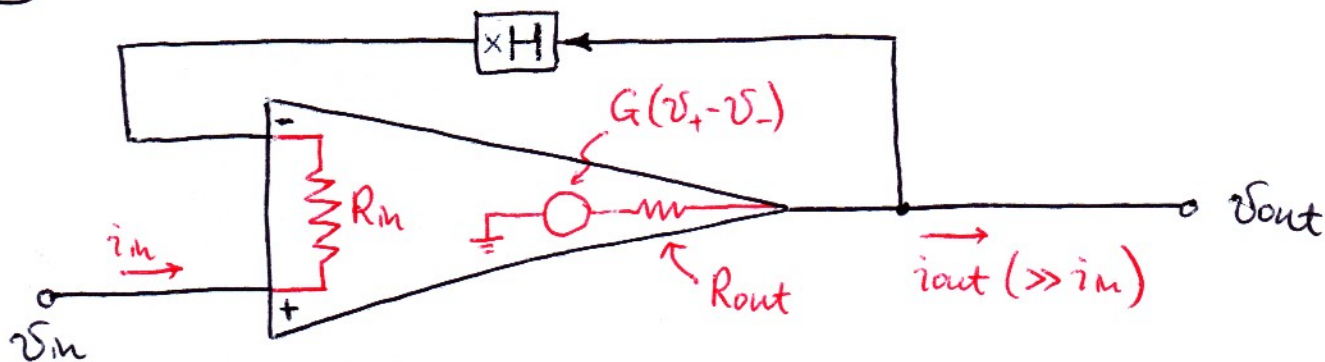
$$\omega_{CL} \approx \omega_0 G_0 H$$

$\omega_{CL} \cdot G_{CL} = \omega_0 G_0 = \text{const}$
"gain-bandwidth product" rule

E.g. 741 $G_0 \sim 2 \times 10^5$, $f_0 \sim 10 \text{ Hz}$ $\Rightarrow G_0 \cdot f_0 = 2 \times 10^6 \text{ Hz}$

Let $G_{CL} = \frac{1}{H} = 100$, $\Rightarrow f_{CL} = 20 \text{ kHz}$

④ Increased input impedance



$$i_{in} R_{in} = v_+ - v_- = v_{in} - H v_{out} = v_{in} - H \frac{G}{1+GH} v_{in} = \frac{v_{in}}{1+GH}$$

$$R_{in,CL} \equiv \frac{v_{in}}{i_{in}} = R_{in} (1+GH)$$

E.g. 741, $G \sim 2 \times 10^5$, $R_{in} \sim 1 \text{ M}\Omega$

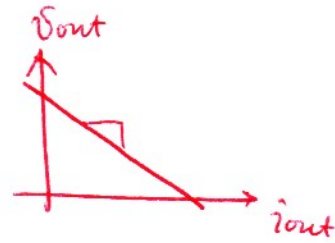
$H \sim \frac{1}{100}$, $\Rightarrow R_{in,CL} \sim 2 \text{ G}\Omega$

⑤ decreased output impedance

④

$$v_{out} = G(v_{in} - H v_{out}) - i_{out} \cdot R_{out}$$

$$v_{out} = \underbrace{\frac{G}{1+GH} v_{in}}_{\text{same as before}} - \underbrace{i_{out} \frac{R_{out}}{1+GH}}_{\text{due to loading}}$$



$$R_{out,CL} = \frac{R_{out}}{1+GH}$$

e.g. $G \approx 2 \times 10^5$, $H \approx \frac{1}{100}$, $R_{out} \approx 80 \Omega$

$R_{out,CL} \approx 0.04 \Omega$
(ideal volt. source)

Rules for analyzing negative F.B. circuits

- 1) current rule: inputs of op-amp draw no current
- 2) voltage rule: $v_{diff} = v_+ - v_- \sim 0$ (very small unless saturates)
 $v_+ \approx v_-$