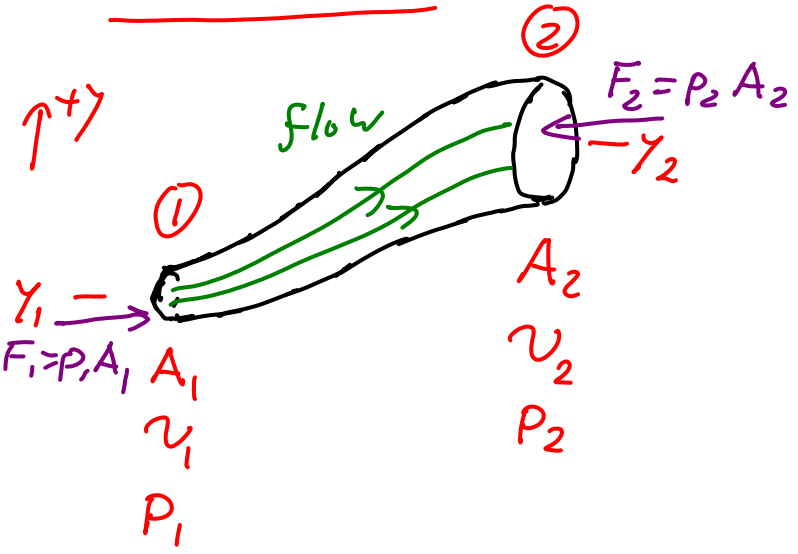


Recap: Ideal Fluids in Motion

• Ideal Fluid: no fluid friction; $\rho = \text{const}$; laminar flow

• Ideal Flow:



- Volume flow rate: $R = \frac{\Delta \text{Volume passing}}{\Delta t} = A v$
x-sectional area
↓
speed of flow \uparrow
- Continuity: $R_1 = R_2 \Rightarrow A_1 v_1 = A_2 v_2$
- Bernoulli's equation for ideal flow

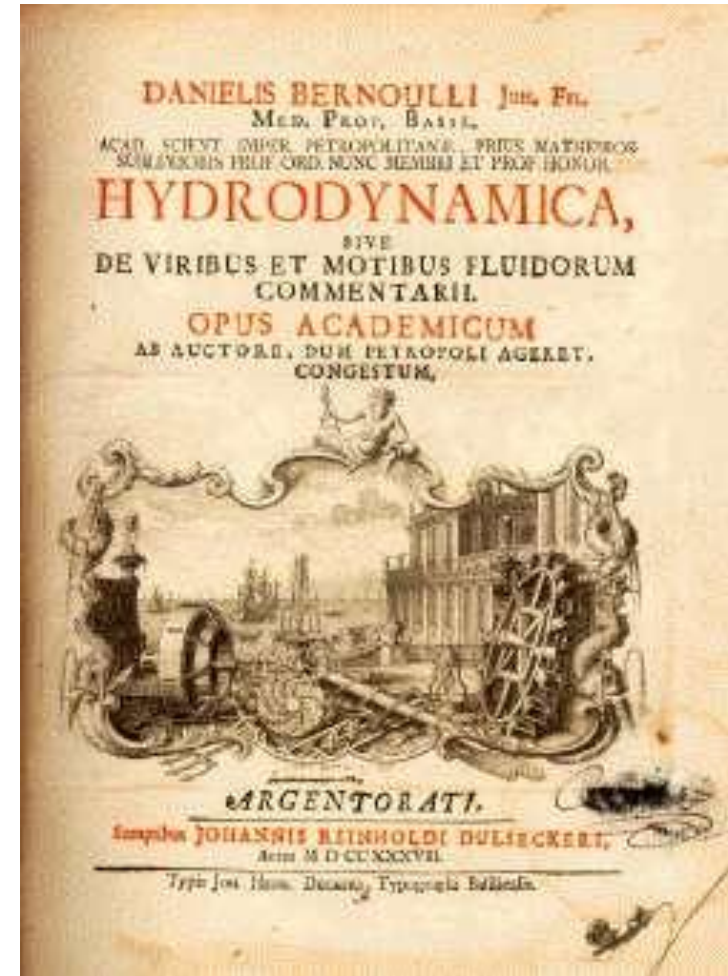
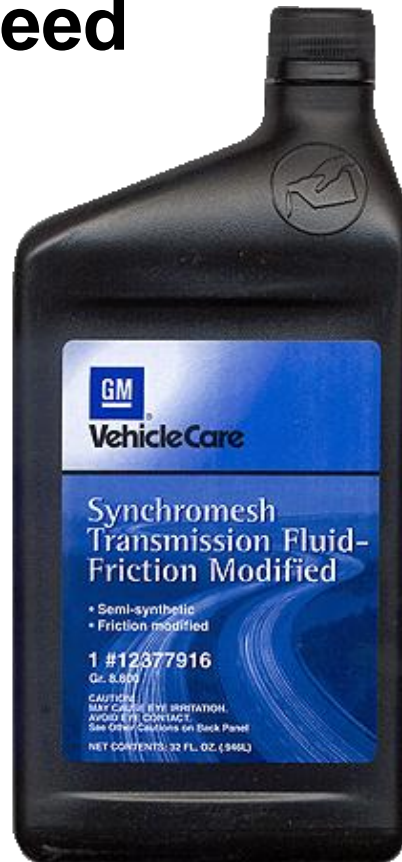
Work on fluid by $\Delta P = \Delta U_g + \Delta K$

$$\Rightarrow \underbrace{P_1}_{\text{work by } F_1} + \underbrace{\rho g y_1}_{U_g/\Delta V} + \underbrace{\frac{1}{2} \rho v_1^2}_{K/\Delta V} = P_2 + \rho g y_2 + \frac{1}{2} \rho v_2^2$$

\Rightarrow for flow at const. height: where v is big, p is small!

Today:

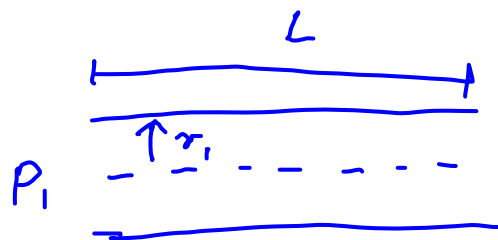
- Fluid friction
- Viscous flow through tube
- Viscous and turbulent drag
- Terminal speed



When blood flows through a blood vessel, it experiences **viscous drag, i.e. friction forces**.

Two **blood vessels of equal length** are connected in parallel so that they have **same pressure drop Δp** . The radius of the first vessel is r_1 . Due to formation of atherosclerotic plaques, the radius r_2 of the second vessel has been **reduced by 50%**.

What is the **ratio R_2/R_1 of the volume flow rates** in the two vessels?

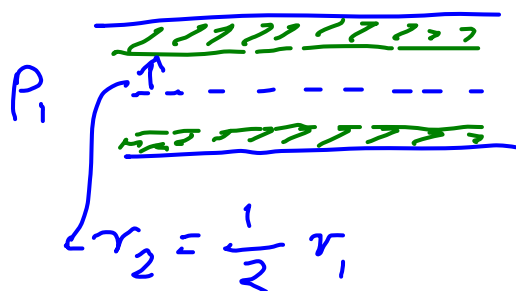


flow \rightarrow

volume flow rate:

$$R = \frac{\Delta P \pi}{L 8\eta} r^4$$

const



flow \rightarrow

$$\Rightarrow R \propto r^4$$

$$\Rightarrow \frac{R_2}{R_1} = \left(\frac{r_2}{r_1}\right)^4 = \left(\frac{1}{2}\right)^4$$

$$R_2/R_1 = ?$$

A. 1

B. 1/2

C. 1/4

D. 1/8

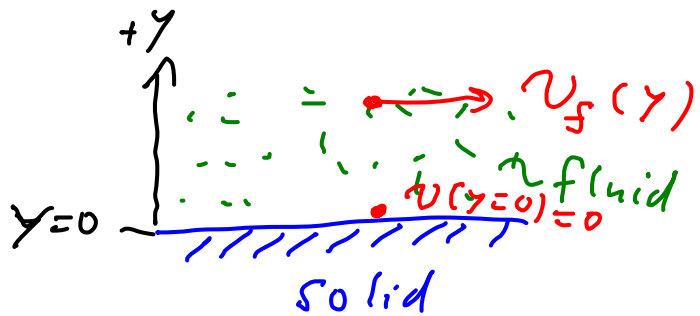
E. 1/16

→ Fluid Friction:

• Recall: Solid on Solid friction:

- f_s, f_k oppose relative motion of the surfaces in contact!

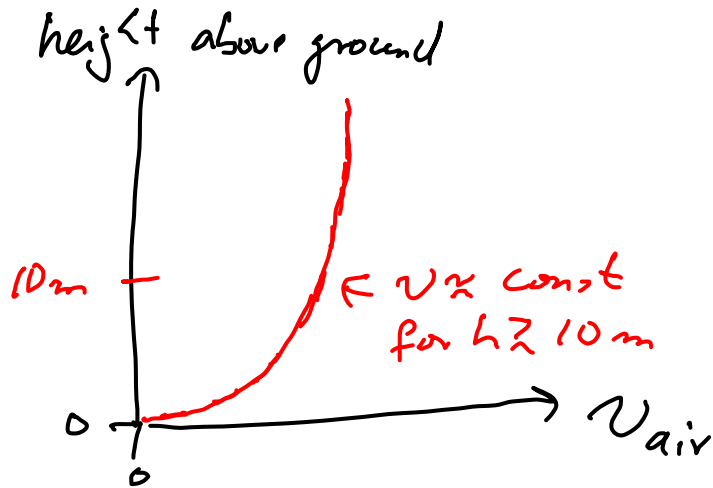
• Fluid-Solid Friction:



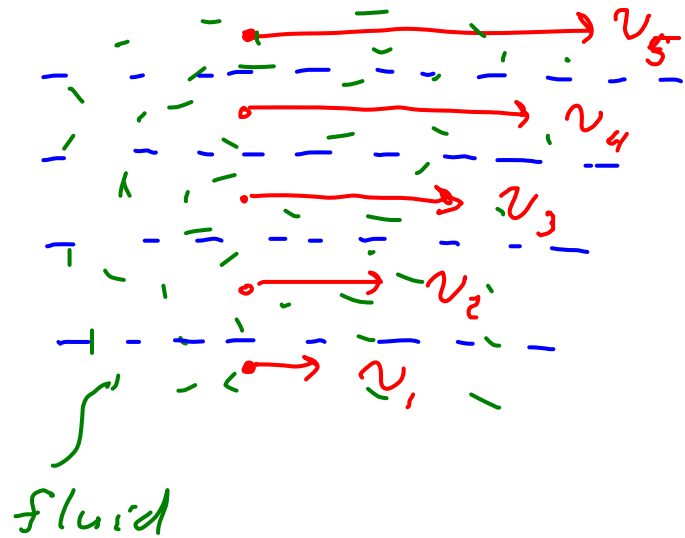
- $v_f = v_f(y)$ depends on height above solid surface
- $v_{fluid}(y=0) = 0$ at $y=0$ (i.e. at fluid-solid interface) relative to surface (no relative motion at surface)

- Examples:

- rain drops on car windshield
- air near earth's surface

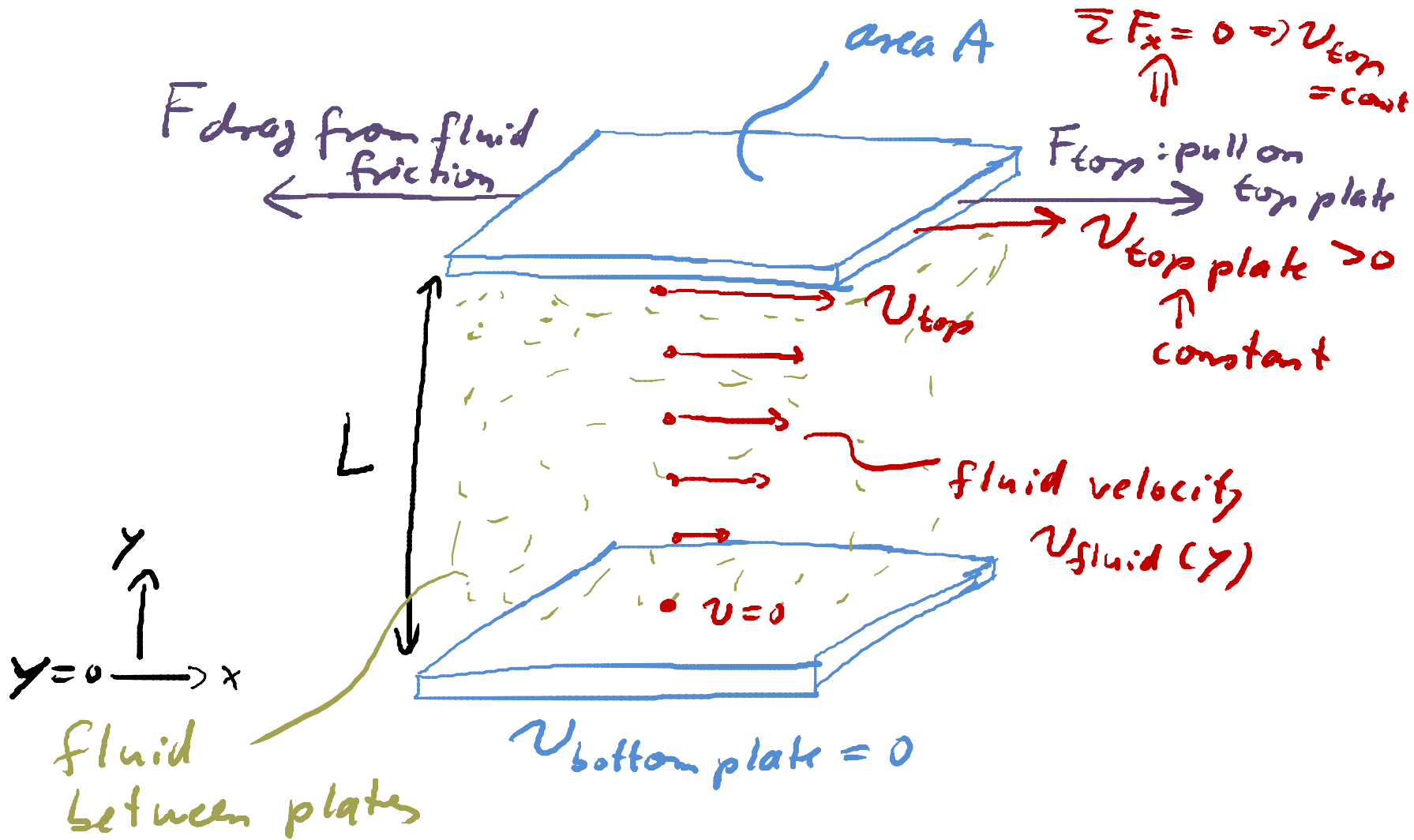


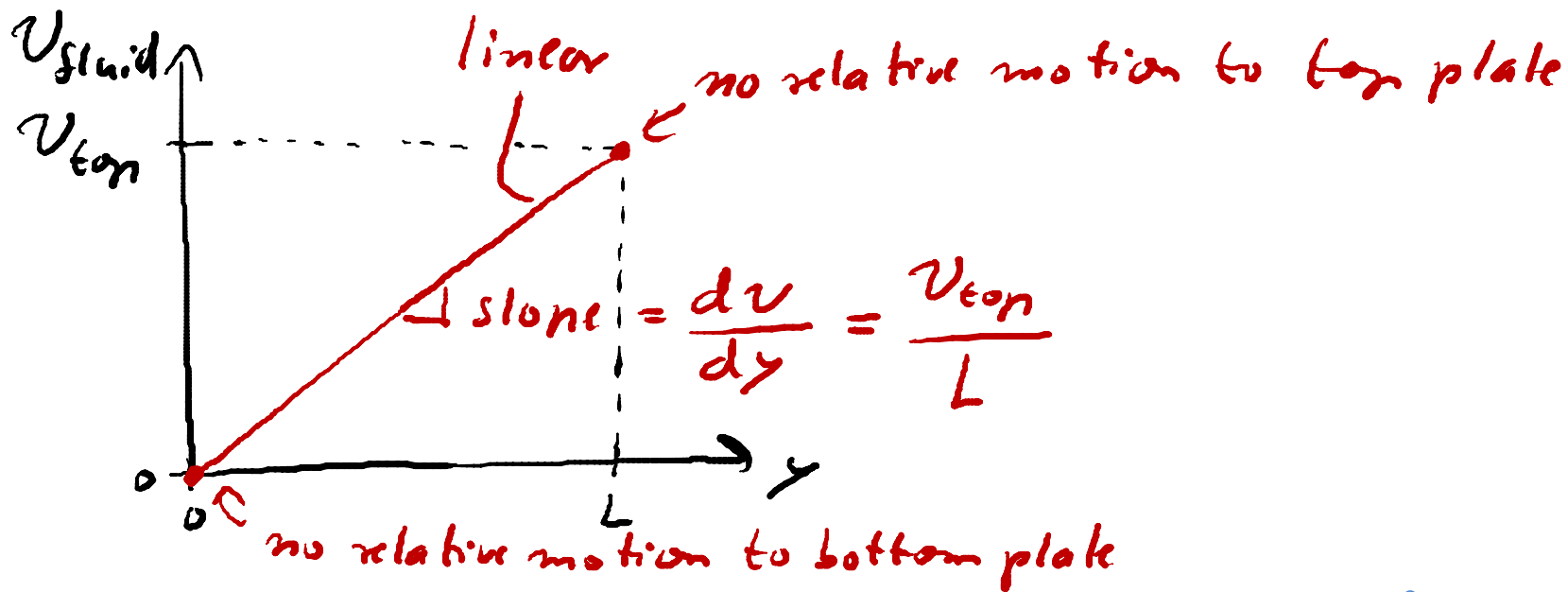
- Fluid-Fluid Friction:



- friction forces (drag) between "layers" at different speeds
 - Fluid friction opposes relative motion of adjacent fluid "layers"
- ⇒ viscosity $\eta = \text{"eta"}$

→ specific geometry:





$|F_{\text{fluid drag}}| \propto A \frac{v_{top}}{L}$

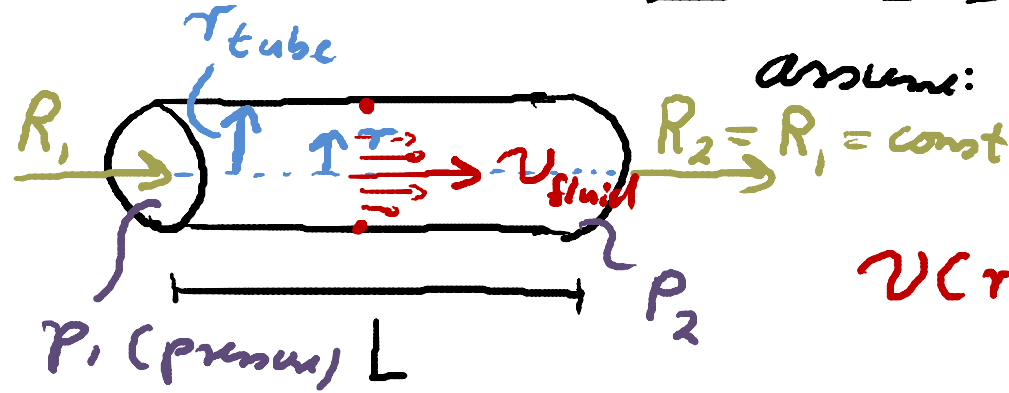
\uparrow large speed \Rightarrow more force
 \uparrow layer A \Rightarrow more force
 \leftarrow smaller L \Rightarrow more force

$$\frac{v_{top}}{L} = \frac{dv}{dy}$$

$$\Rightarrow F_{\text{fluid drag}} = \eta A \frac{dv}{dy}$$

$\eta = \text{viscosity}$ $[\eta] = \frac{\text{kg}}{\text{m}\cdot\text{s}} = \text{Pa}\cdot\text{s}$
 $\eta_{\text{water}} = 10^{-3} \text{ Pa}\cdot\text{s}$ $\eta_{\text{air}} = 1.8 \cdot 10^{-5} \text{ Pa}\cdot\text{s}$

→ Viscous, laminar flow through tube (const. height)



assume: $y = \text{const}$, $A = \text{const}$

fluid speed in the tube:

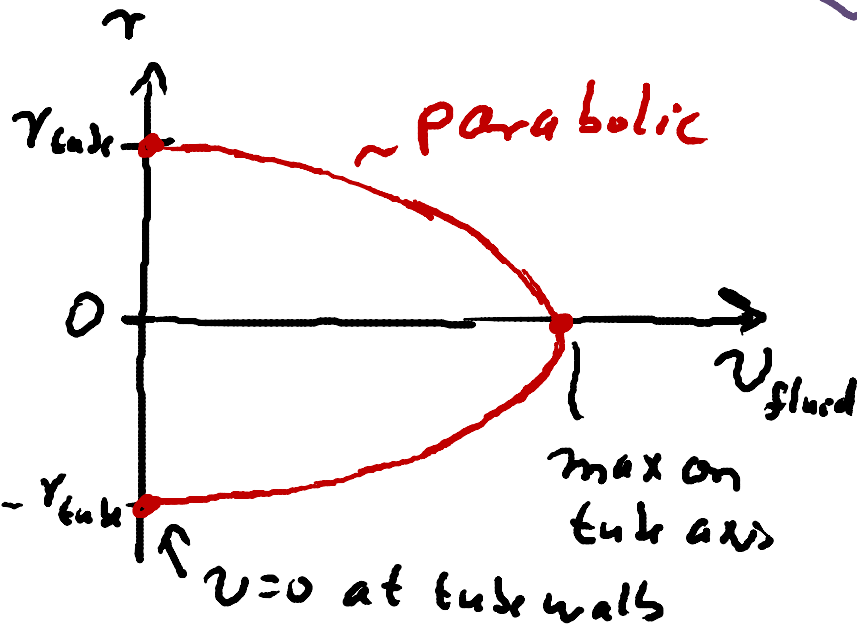
$$v(r) = \frac{1}{4} \frac{1}{\eta} \frac{\Delta P}{L} (r_{\text{tube}}^2 - r^2)$$

radial distance from tube axis

need $\Delta P = P_1 - P_2 > 0$

work by pressure difference required to provide energy lost by friction and to maintain constant flow!

Note: Bernoulli's equation only for ideal fluids, i.e. no friction! ($\eta = 0$)



⇒ Volume flow rate for tube:

$$\underline{\underline{R}} = \text{Area} \cdot v_{\text{avg}} = \pi r_{\text{tube}}^2 \cdot v_{\text{avg}}$$

← average of flow speed over cross-sectional area of tube

$$= \underbrace{\pi r_{\text{tube}}^2}_{\text{from area}} \cdot \frac{1}{8} \frac{1}{\eta} \frac{\Delta P}{L} \underbrace{r_{\text{tube}}^2}_{\text{from } v_{\text{fluid}}} \propto r_{\text{tube}}^4$$

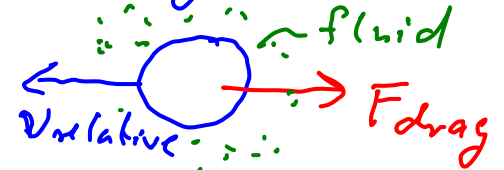
$$\Rightarrow R_{\text{tube}} = \frac{\pi}{8\eta} \frac{\Delta P}{L_{\text{tube}}} r_{\text{tube}}^4$$

Poiseuille's equation

- for laminar, viscous flow only!
- ~ obeyed in human circulatory system

→ Fluid drag on Moving Objects:

Two regimes (extreme cases):



Turbulent drag regime

- high velocities, large objects, small η

$$F_{\text{drag, turb}} = \frac{1}{2} C \rho_{\text{fluid}} A_{\text{obj}} v^2$$

⇒ for sphere: $C = \frac{1}{2}$

⇒

$$F_{\text{drag, turb, sphere}} = \frac{1}{4} \rho_{\text{fluid}} \underbrace{\pi r_{\text{sp}}^2}_{A_{\text{sp}} = \pi r_{\text{sp}}^2} v^2$$

↑
radius of sphere

Viscous drag (laminar flow) regime

- low velocities, small objects, large η

$$F_{\text{drag, visc}} \propto \eta v$$

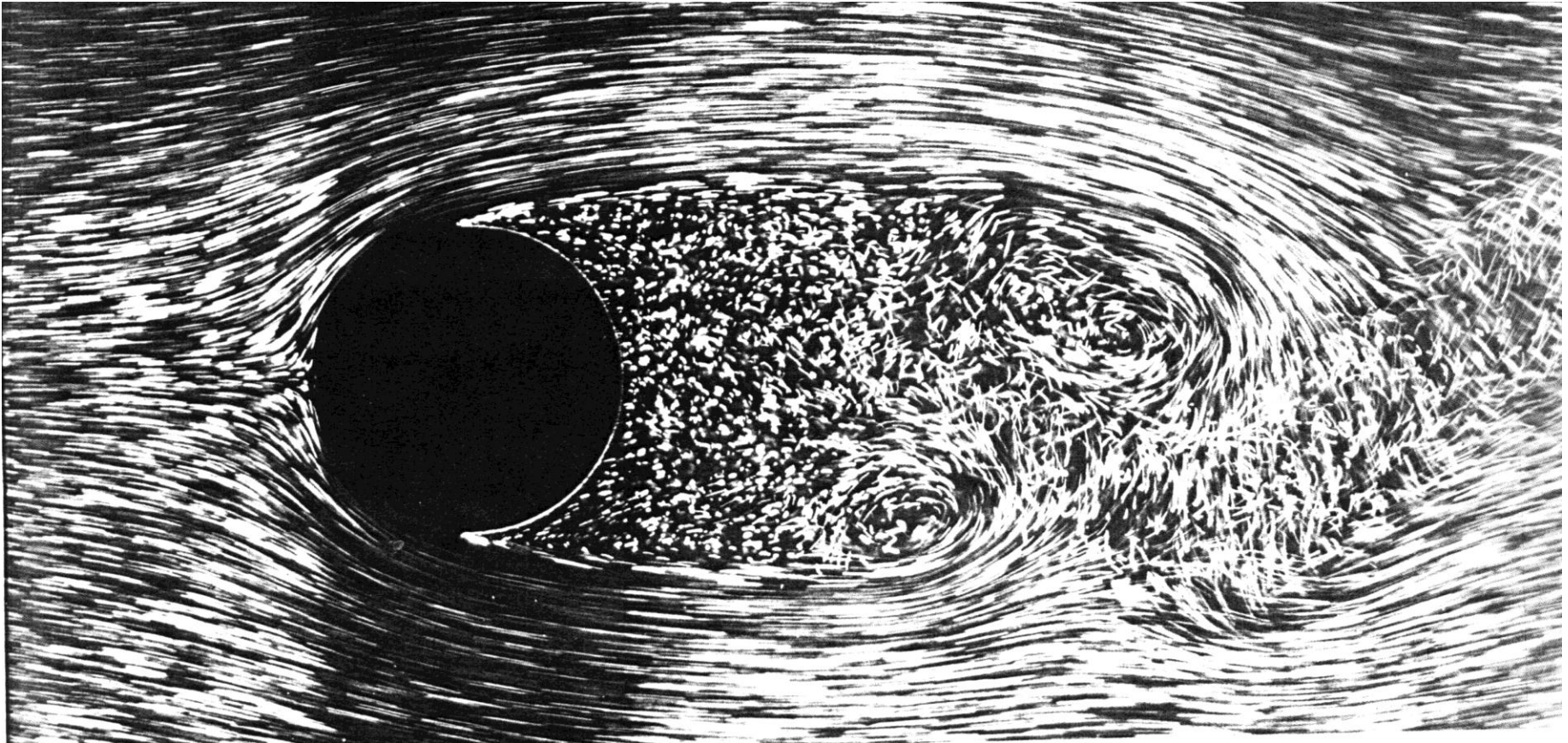
⇒ for sphere: (r_{sp} = radius of sphere)

$$F_{\text{drag, visc, sphere}} = 6 \pi \eta r_{\text{sp}} v$$

Stokes' Law

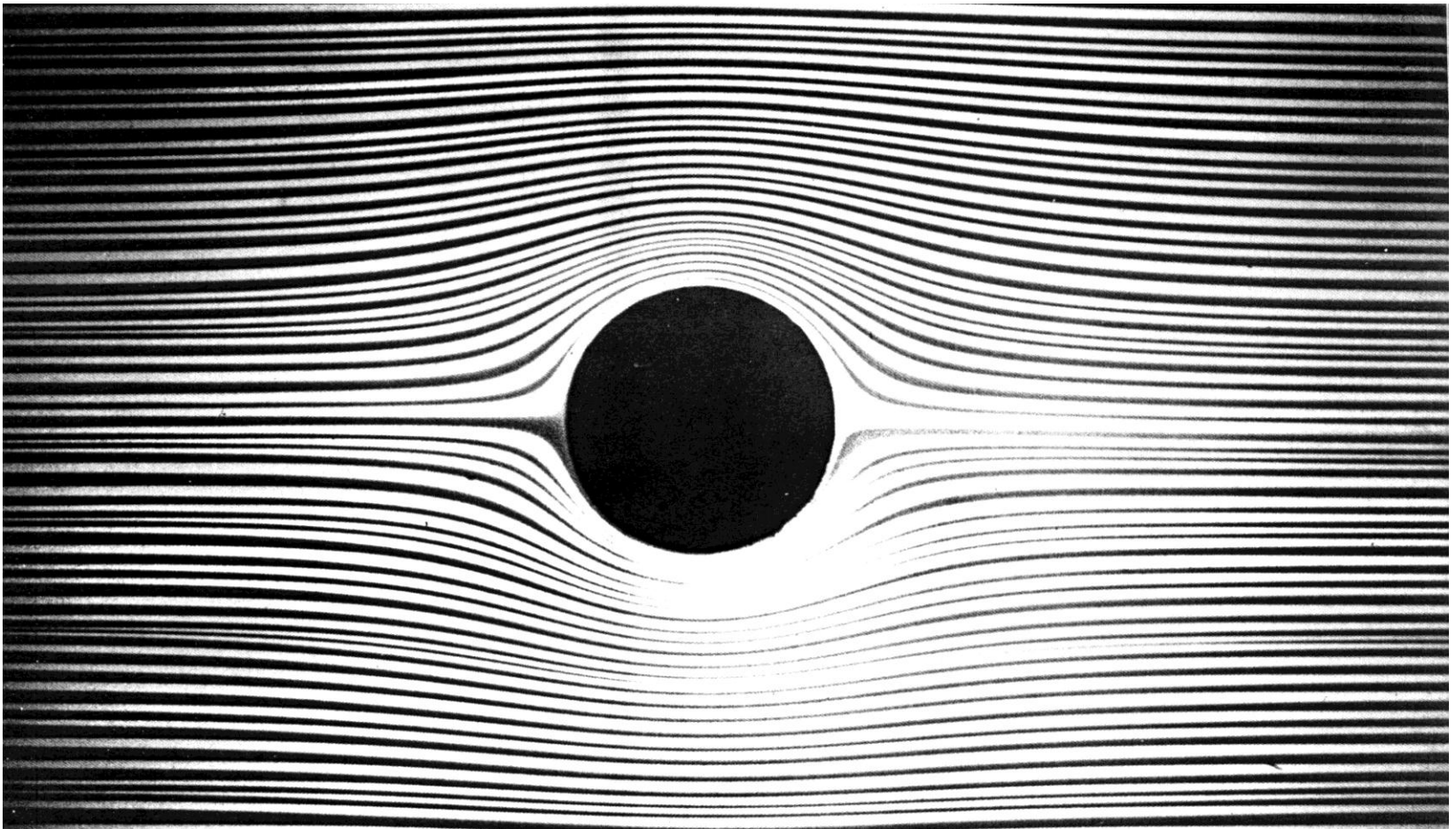
Fluid flow pattern around a moving cylinder

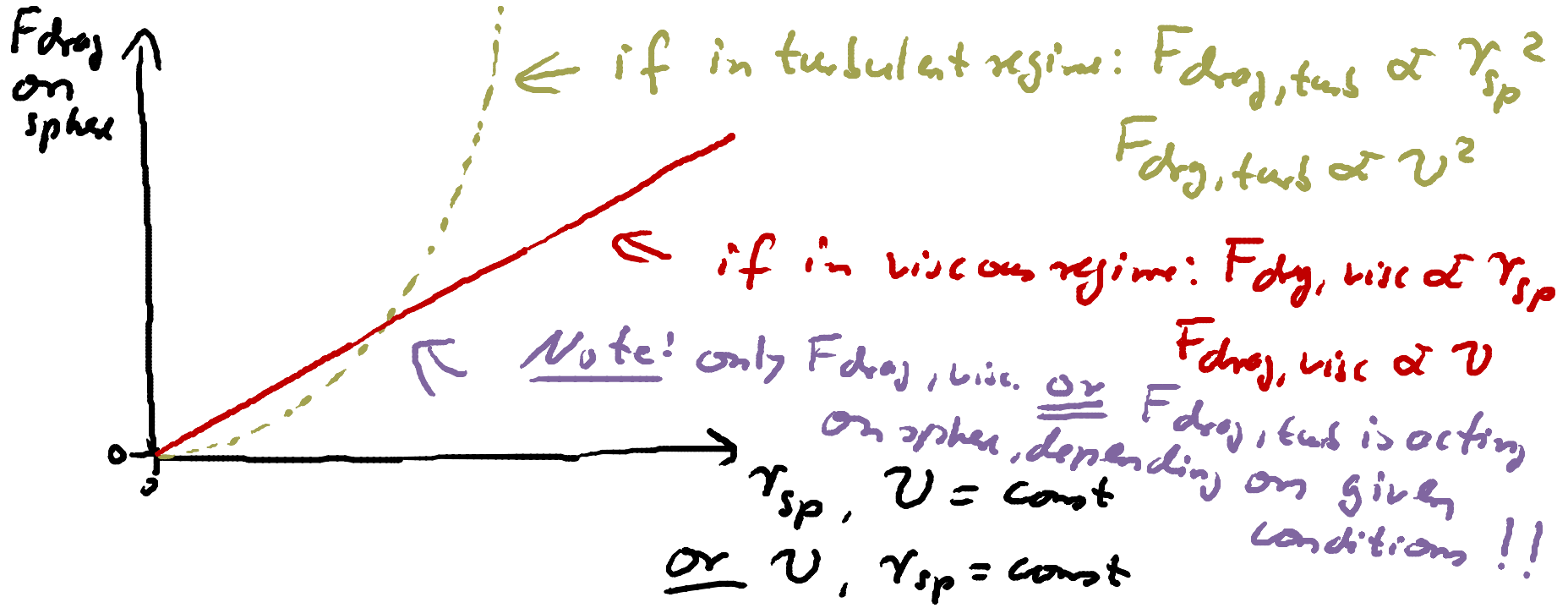
Turbulent flow: High velocities / larger diameters / "thin" fluids:



Fluid flow pattern around a moving cylinder

**Laminar Flow: Low velocities / small diameters
/ "thick" fluids**





What determines whether we are in the viscous regime or turbulent regime?

-> compare forces in regimes:

$$\frac{F_{\text{drag, turb}}}{F_{\text{drag, visc}}} \text{ on sphere} = \frac{1}{24} \frac{\rho_f r_{sp} U}{\eta} \left. \begin{array}{l} \text{if } \gg 1 \Rightarrow \text{turbulent} \\ \text{if } \ll 1 \Rightarrow \text{viscous} \end{array} \right\}$$

Reynolds' number (dimensionless)

⇒ Reynold's Number:

$$Re = \frac{\rho_{\text{fluid}} r v}{\eta}$$

r : "typical" dimension of the object

- for sphere: ($r = r_{\text{sphere}}$) moving through fluid:
 - $Re \gg 24 \rightarrow$ turbulent \rightarrow use $F_{\text{drag, turb}}$
 - $Re \ll 24 \rightarrow$ viscous/laminar \rightarrow use $F_{\text{drag, visc.}}$
- for flow through pipes: ($r =$ radius of pipe)
 - $Re > 3000 \rightarrow$ turbulent
 - $Re < \underbrace{2000} \rightarrow$ viscous

determined experimentally

→ Terminal speed v_t of a sphere:

- at $v = v_t$ when $a \rightarrow 0$

$$\Rightarrow \sum \vec{F} = 0 \quad \text{at } v = v_t$$

$$\Rightarrow |F_{\text{drag}}| = |W| - |F_{\text{buoy}}|$$

⇒ In viscous regime:

$$F_{\text{drag, visc}} (v = v_t) = 6 \pi \eta r_{\text{sp}} \underline{\underline{v_t}}$$

$$W = mg = V_{\text{sp}} \rho_{\text{sp}} g = \frac{4}{3} \pi r_{\text{sp}}^3 \rho_{\text{sp}} g$$

$$F_{\text{buoy}} = W_{\text{fluid disp}} = \frac{4}{3} \pi r_{\text{sp}}^3 \rho_{\text{fluid}} g$$

$$v_{t, \text{visc}} = \frac{2}{9} \frac{(\rho_{\text{sp}} - \rho_{\text{fluid}})}{\eta} g r_{\text{sp}}^2 \propto \underline{\underline{r_{\text{sp}}^2}}$$

